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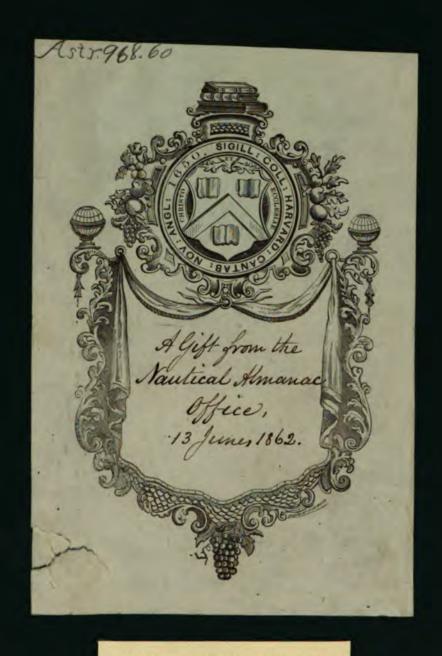
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# TABLES

OF

# MELPOMENE

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# TABLES

OF

# MELPOMENE,

BY

Ernsk-E. SCHUBERT., 1813-1873

COMPUTED FOR THE

## AMERICAN EPHEMERIS AND NAUTICAL ALMANAC,

UNDER THE SUPERINTENDENCE OF

COMMANDER CHARLES HENRY DAVIS, U. S. N.

Published by Inthority of the Secretary of the Navy.

D'BUREAU OF ORDNANCE AND HYDROGRAPHY,

WASHINGTON.

1860.

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1862. June 13 Object from the Nautical Almanac Office.

CAMBRIDGE:
ECTROTYPED AND PRINTED BY WELCH, BIGELOW, & CO.,

# REPORT

TO

## COMMANDER C. H. DAVIS, U. S. N.

# I. ON THE COMPUTATION OF THE GENERAL PERTURBATIONS OF MELPOMENE BY JUPITER.

#### BY ERNEST SCHUBERT.

TOR the computation of these perturbations, Professor Encke's method, published in the Berliner Jahrbuch for 1857, has been used in order to try it by a complete application to a special case. The basis of the work are the following elements:—

MELPOMENE.

1854, Jan. 0, Washington Mean Time; (osculating).

1854, Jan. 0, Washington Mean Time.

The plane of the orbit of Melpomene has been adopted for the fundamental plane, and the major axis for the line of the abscissas. The orbit of Jupiter is referred to this fundamental plane by means of the formulas on page 390 (Jahrbuch for 1857).

 $\log a =$ 

0.7162370

0.3609465

 $\log a =$ 

Now for the computation of  $\frac{m' \kappa^2}{\rho^{08}}$  the periphery was divided into 16 parts, so that M and M' (the mean anomalies of Melpomene and Jupiter) for those 16 points are 0°, 22°.5, 45°, &c. Log  $m' \kappa^2 = 5.5760322$  in units of the seventh decimal-place, and for the Julian year as the unit of time. Each point of the Melpomene orbit is combined with all 16 points of the Jupiter orbit, which gives  $16 \times 16 = 256$  values of  $\frac{m' \kappa^2}{\rho^{08}}$ . On page 354, Professor Encke says that those values can be checked only by double calculation, since it cannot be done by the differences in the series obtained for the different M. But I found that, if we arrange the quantities  $\frac{m' \kappa^2}{\rho^{08}}$  according to another principle, they can be tested by differences, which will be shown by the following:—

			A.	٠,٠		В.							
M =	0°	22°.5	45°	67°.5	90°	etc.			† !		11776.2		
$\frac{m' \kappa^2}{\rho^{CE}}$	11776.2	9701.8	$M = 0^{\circ}$ 5823.7	3385.1	2150.3				3722.0	7454.2 6636.6	11195.8 10851.5		
	7454.2	11195.8	$M = 22^{\circ}.5$ $10838.6$	7038.9	4099.4		1419.6	2117.7 2110.9	3515.1 3583.5	6418.2 6753.7	11154.1 12234.1		
	3722.0	6636-6	$M = 45^{\circ}$ $10851.5$	12032.8	8415.1		:	•			0 & 0		
	2117.7	3515.1	$M = 67^{\circ}.5$ $6418.2$	11154.1	13455.3					22.5 & 0 45 & 22.5 67.5 & 45	0 & 0 22.5 & 22.5 45 & 45		
	1419.6	2110.9	$M = 90^{\circ}$ 3583.5	6753.7	12234.1				etc.	Diff. = 22.5	Diff. = 0		
			etc.										

This sketch needs no further explanation; the principle for the arrangement in B from A is very simple, and it is obvious that it is the vertical series in B which can be tested by differences.

In Table A the values of  $\frac{m' \kappa^2}{\rho^{os}}$  are functions of M', and they are developed in series of the form,

$$\frac{m'\kappa^2}{\rho^{\infty}} = a^{\circ} + a' \cos M' + b' \sin M' + a'' \cos 2 M' + b'' \sin 2 M'.$$

It is evident that now in these series the coefficients are functions of M, and they must be developed in series of the same form, that is, for instance,

$$a^{\circ} = a^{\circ} + \alpha' \cos M + \beta' \sin M + \alpha'' \cos 2M + \beta'' \sin 2M.$$

Each of the latter series must be multiplied with the cos i' M' or sin i' M' belonging to it, and then, finally, by resolving the products of two cosines or sines into sums and differences, we obtain  $\frac{m' \, \kappa^2}{\rho^{cs}}$  developed in series of the general form

$$a_i^{i'}\cos(iM-i'M')+b_i^{i'}\sin(iM-i'M').$$

In order to have throughout —i' M we only have to change the sign of i' and that of the coefficient of the sine.

The formulas for the components of the disturbing force (page 392) are: -

$$\begin{split} \mathbf{X}_1 &= m' \, \mathbf{x}^2 \, \left\{ \left( \frac{1}{\rho^{\text{ol}}} - \frac{1}{r'^{\text{ol}}} \right) \, x'_1 - \frac{x_1}{\rho^{\text{ol}}} \right\} \\ \mathbf{Y}_1 &= m' \, \mathbf{x}^2 \, \left\{ \left( \frac{1}{\rho^{\text{ol}}} - \frac{1}{r'^{\text{ol}}} \right) \, y'_1 - \frac{y_1}{\rho^{\text{ol}}} \right\} \\ \mathbf{Z}_1 &= m' \, \mathbf{x}^2 \, \left\{ \left( \frac{1}{\rho^{\text{ol}}} - \frac{1}{r'^{\text{ol}}} \right) \, z'_1 \right\} \end{split}$$

Therefore, after having developed  $\frac{m' \kappa^2}{\rho^{os}}$  according to the above precepts, we subtract from it

$$\frac{m' \kappa^3}{r'^3} = 2684.3 + 888.2 \cos M'$$
+ 28.1 \cos 2 M'
+ 2.0 \cos 3 M'
+ 0.1 \cos 4 M'

and get thus  $m' x^2 \left(\frac{1}{\rho^{cs}} - \frac{1}{r^{cs}}\right)$ . This periodical series is to be multiplied successively with  $x'_1$ ,  $y'_1$ , and  $z'_1$ ; developed also in periodical series they are:—

$$x'_{1} = -0.37409 + 5.16475 \cos M' + 0.25210 \sin M' + 0.12450 \cos 2 M' + 0.00608 \sin 2 M' + 0.00450 \cos 3 M' + 0.00022 \sin 3 M' + 0.00019 \cos 4 M'$$

$$y'_{1} = +0.02313 - 0.31933 \cos M' + 5.14340 \sin M' - 0.00770 \cos 2 M' + 0.12401 \sin 2 M' - 0.00028 \cos 3 M' + 0.00446 \sin 3 M' + 0.00019 \sin 4 M'$$

$$x'_{1} = -0.03518 + 0.49693 \cos M' + 0.68709 \sin M' + 0.01336 \cos 2 M' + 0.01657 \sin 2 M' + 0.00185 \cos 3 M' + 0.001657 \sin 2 M' + 0.00144 \cos 4 M' + 0.00142 \cos 5 M' + 0.00142 \cos 6 M' + 0.00142 \cos 7 M' + 0.00142 \cos 7 M' + 0.00071 \cos 8 M'$$

After that, the periodical series  $\frac{m'}{\rho^{\infty}}$  must be multiplied with  $-x_1$  and  $y_1$ .

We have 
$$-x_1 = +0.74808 - 2.25537 \cos M$$
  $-y_1 = -2.22785 \sin M$   $-0.24159 \cos 2 M$   $-0.03886 \cos 3 M$   $-0.03861 \sin 3 M$   $-0.00741 \cos 4 M$   $-0.00155 \cos 5 M$   $-0.00155 \sin 5 M$   $-0.00035 \sin 6 M$ 

Finally, after these five multiplications, by forming the sums, we obtain the series for  $X_1$ ,  $Y_1$ ,  $Z_1$ .

I subjoin here now the terms of  $\frac{m'}{\rho^{oa}}$  and of m'  $\kappa^2 \left(\frac{1}{\rho^{oa}} - \frac{1}{r^n}\right)$  retained for multiplication, the terms smaller than 0.5 having been omitted.

	$\frac{m'  \kappa^3}{ ho^{\cos}}$																
i,	i'	cos	sin	i,	i	cos	sin	i,	i'		008	'	sin	i,	i'	COS	sin
0	0	+4348.2	0.0	_	-1	- 7.3	0.0	6	-1	+	5.6	_	5.8	-2	-2	- 1.1	+ 0.5
1 2	0	- 602.6 + 19.8	+ <b>25.</b> 8 -60.9	_	-1 -1	+ 6.3 - 6.0	- 1.6 + 2.8	7	-1 -1	-	2.7 0.0	+	6.6 3.7	-1 0	-2 -2	- 14.0 + 195.3	- 8.8 + 33.7
3	0	+ 1.3	<b>–</b> 5.1		-1	+ 109.0	+ 64.1	"	-1		0.0		0.1	ĭ	-2	-1174.9	+156.8
4	0		- 1.6		-1	-1384.0	+ 90.2	-8	-2		0.0	+	0.5	2	-2	+2618.4	-301.3
-8	-1	0.0	9.77	_	-1	+5208.0	-305.3	-7 c	2	+	0.5	<del>-</del>	1.1	3	-2	+ 350.1	- 13.4
	-1 -1	0.0 + 2.9	- 3.7 + 6.7		-1 -1	+ 185.2 + 48.1	+ 26.4 - 43.1	-6  -5	-2 -2	-	0.8 1.0	+	0.7 0.5	5	-2 -2	+ 77.3 + 16.1	- 27.7 - 8.6
_6	-1	- 5.2	- 5.1		-1	+ 18.5	- 7.9	-4	-2	_	1.2		0.0	6	-2	+ 4.7	- 1.5
<b>–</b> 5	-1	+ 6.6	+ 2.9	5	-1	- 4.4	+ 0.8	-3	-2	+	0.9	+	0.5	7	-2	0.0	- 1.7

$\frac{m'  \kappa^2}{\rho^{\text{os}}}$												
i,	i'	cos	sin	i, i'	cos	ein	i, i'	COS	sin	i, i'	cos	sin
8	-2	0.0	+ 0.5	-2 -4 -1 -4	+ 0.8	+ 1.1	6 -5 7 -5	+ 96.3 + 38.0	- 21.5 - 11.8	-5 -7 -4 -7	+ 5.3 - 7.4	+ 2.6 0.0
-8 -7	-3 -3	+ 0.5 - 0.9	+ 1.2 - 2.9	0 -4 1 -4	+ 3.0 - 31.4	+ 3.7 - 5.3	8 –5	+ 4.5	- 1.2	-3 -7 -2 -7	+ <b>6.8</b> - <b>5.3</b>	- 3.0 + 5.3
-6 -5	-3 -3	+ 2.0 - 2.8	+ 2.1	2 -4 3 -4	+ 158.1 - 447.7	- 19.3 +120.2	-8 -6 -7 -6	+ 12.7 + 4.4	- 1.2 - 5.8	-1 -7 0 -7	+ 2.4	- 6.7 + 7.4
-4 -3	-3 -3	+ 2.8 - 2.9	0.0 + 1.1	4 -4. 5 -4	+ 506.8 + 181.6	-117.6 - 30.1	-6 -6 -5 -6	+ 2.7 + 1.2	0.0   - 1.0	1 -7 2 -7	- 3.1 + 4.3	- 6.5 + 5.1
-2 -1	-3 -3	+ 1.8 0.0	- <b>2.4</b> + <b>4.8</b>	6 -4 7 -4	+ <b>52.8</b> + <b>14.7</b>	- 15.4 - 4.9	-4 -6 -3 -6	- 1.0 + 0.9	0.0	3 -7 4 -7	- 2.3 - 6.7	- 2.7 + 4.7
0 1	-3 -3	- 27.6 + 202.1	- 12.0 + 1.6	8 –4	+ 2.2	- 1.6	-2 -6 -1 -6	- 1.1 0.0	- 0.8 + 1.0	5 -7 6 -7	+ 33.9 - 45.4	- 11.6 + 23.5
3	-3 -3	- 778.5 +1199.2	+153.7 -205.2	-8 -5 -7 -5	+ 4.5 + 2.8	- 1.2 - 4.0	0 -6	0.0 - 1.2	- 1.0 + 0.8	7 -7 8 -7	+ 23.5 + 6.9	- 2.9 - 10.9
5	-3 -3	+ 282.1 + 73.9	- 30.9 - 21.2	-6 -5 -5 -5	+ 2.6	+ 1.5	2 -6 3 -6	+ 5.7	+ 4.0	-8 -8 7 0	+ 3.6	0.0
6 7 8	-3 -3 -3	+ 15.1 + 5.8 + 0.5	<ul><li>5.3</li><li>4.7</li><li>1.2</li></ul>	-4 -5 -3 -5 -2 -5	+ 2.9 - 2.8 + 1.9	0.0 + 1.1 - 2.1	4 -6 5 -6 6 -6	+ 68.9 - 116.8 + 75.3	- 20.7 + 48.6 - 25.2	-7 -8 -6 -8 -5 -8	- 6.9 + 13.0 - 3.6	- 8.9 + 3.8 - 2.4
_8	-4	+ 2.2	- 1.6	-1 -5 0 -5	- 1.3 - 0.8	+ 2.8 - 3.2	7 -6 8 -6	+ 46.2 + 12.7	- 18.2 - 1.2	-4 -8 4 -8	+ 1.9 + 1.9	0.0
-7 -6	-4 -4	0.0	+ 0.8	1 -5 2 -5	+ 5.7	+ 4.3	-8 -7	+ 6.9	- 10.9	5 -8 6 -8	- 3.6 + 13.0	+ 2.4 - 3.8
-5 -4	-4 -4	- 1.4 + 1.5	+ 0.6	3 -5 4 -5	+ 111.6 - 240.3	- <b>23.4</b> + 80.8	-7 -7 -6 -7	+ 24.3 - 6.4	+ 8.4 - 9.8	7 -8 8 -8	- 6.9 + 3.6	+ 8.9 0.0
<del>-3</del>	-4	- 1.6	- 0.6	5 -5	+ 204.6	- 59.9	 <del></del>	 	<u> </u>	<u> </u>	<u> </u>	· ======
						$m' x^2 \left(\frac{1}{\rho}\right)$	$\left(\frac{1}{\cos} - \frac{1}{r^{-1}}\right)$					
i',	i	cos	sin	i', i	cos	sin	i', i.	cos	sin	i', i	COS	sin ·
0	0 0	+1663.9 -1772.6	0.0 - 90.2	6 -1 7 -1	- 1.2 - 3.1	- 0.8 + 6.5	-4 -3 -3 -3	- 1.6 - 2.9	- 0.6 + 1.1	1 -4 2 -4	+ 18.5 + 77.3	+ 7.9 + 27.7
3	0	+ 167.2 - 29.6	- 33.7 + 12.0	-7 -2	- 5.3	+ 5.3	-2 -3 -1 -3	+ 0.9 + 6.3	+ 0.5	3 -4	+ 282.1 + 506.8	+ 30.9 +117.6
5	0	+ 2.9	- 3.7 + 3.2	-6 -2 -5 -2	- 1.1 + 1.9	- 0.8 - 2.1	0 -3	+ 1.3 + 48.1	+ 5.1 + 43.1	5 -4 6 -4	- 240.3 + 68.9	- 80.8 + 20.7
6	0	0.0	+ 1.0	-4 -2 -3 -2	+ 0.8 + 1.8	+ 1.1	2 -3 3 -3	+ 350.1 +1199.2	+ 13.4 +205.2	7 -4 8 -4	- 6.7 + 1.9	- 4.7 0.0
-7 -6	1 1	+ 2.4	- 6.7 + 1.0	-2 -2 -1 -2 0 -2	- 1.1 - 6.0 + 19.8	+ 0.5 + 2.8 + 60.9	4 -3 5 -3 6 -3	- 447.7 + 111.6 - 22.5	-120.2 + 23.4 - 4.0	-8 -5 -7 -5	- 3.6 + 5.3	- 2.4 + 2.6
-5 -4	-1 -1	- 1.3 - 1.1	+ 2.8 - 1.8	1 -2 2 -2	+ 185.2 +2618.4	- 26.4 +301.3	7 –3	- 2.3	+ 2.7	-6 -5 -5 -5	+ 1.2 - 2.5	- 1.0 - 1.5
-3 -2	-1 -1	0.0 - 14.0	+ 4.8 - 8.8	3 -2 4 -2	- 778.5 + 158.1	-153.7 + 19.3	-8 -4 -7 -4	+ 1.9 - 7.4	0.0	-4 -5 -3 -5	- 1.4 - 2.8	+ 0.6 - 1.2
-1 9	-1 -1	+ 109.0 - 602.6	+ 64.1 - 25.8	5 -2 6 -2	- 30.7 + 5.7	+ 1.1 0.0	-6 -4 -5 -4	- 1.0 + 2.9	0.0 0.0	-2 -5 -1 -5	+ 1.0 + 6.6	- 0.5 + <b>2.</b> 9
2	-1 -1	+5208.0	+305.3 -156.8	7 -2	+ 4.3	- 5.1	-4 -4 -3 -4	+ 1.5 + 2.8	0.0	0 -5 1 -5	0.0 - 4.4	0.0
3 4 5	-1 -1 -1	+ 202.1 - 31.4 + 5.7	- 1.6 + 5.3 - 4.3	-7 -3 -6 -3 -5 -3	+ <b>6.8</b> + <b>0.9</b> - <b>2.8</b>	0.0	-2 -4 -1 -4	- 1.2 - 7.3	0.0 0.0 + 1.6	2 -5 3 -5 4 -5	+ 16.1 + 73.9 + 181.6	+ 8.6 + 21.2 + 30.1
	_1	T 0.1	- 4.3	_v -₃	<b>- 2.</b> 8	+ 1.1	0 -4	0-0	+ 1.6	4 o	+ 181.6	+ 30.1

$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	
6 - 5   - 116.8   - 48.6   3 - 6   + 15.1   + 5.3   0 - 7   0.0   0.0   - 4 - 8   + 2.2   - 7 - 5   + 33.9   + 11.6   4 - 6   + 52.8   + 15.4   1 - 7   - 2.7   - 6.6   - 3 - 8   + 0.5   + 8 - 5   - 3.6   - 2.4   5 - 6   + 96.3   + 21.5   2 - 7   0.0   + 1.7   - 2 - 8   0.0   + - 6 - 6   + 13.0   + 3.8   7 - 6   - 45.4   - 23.5   4 - 7   + 14.7   + 4.9   0 - 8   0.0   - 6 - 6   - 6   - 4 - 7   - 4   - 7   + 14.7   + 4.9   0 - 8   0.0   - 6   - 6   - 6   - 4   - 7   + 14.7   + 4.9   0 - 8   0.0   - 6   - 6   - 6   + 2.7   0.0     - 7   - 6.9   - 8.9   7 - 7   + 23.5   + 2.9   3 - 8   + 0.5   - 4   - 6   + 13.0   - 12.2   - 7   - 7   + 24.3   + 8.4   8 - 7   - 6.9   - 8.9   4   - 8   + 2.2   - 8   - 0.0   - 4   - 6   + 13.3   - 1.2   - 7   - 7   + 24.3   + 8.4   8   - 7   - 6.9   - 8.9   4   - 8   + 2.2   - 3   - 6   + 2.0   + 2.1   - 6   - 7   + 4.4   - 5.8   - 7   - 6.9   - 8.9   4   - 8   + 2.2   - 4   - 3   - 6   - 5.2   - 5.1   - 4   - 7   0.0   + 0.8   - 7   - 8   - 6   - 8   + 12.7   - 1.2   8   - 8   + 12.7   - 1   - 6   - 5.2   - 5.1   - 4   - 7   0.0   + 0.8   - 7   - 8   + 6.9   - 10.9   7   - 8   + 6.9   - 7   - 8   - 8   + 3.6   - 8   + 3.6   - 8   + 3.6   - 8   + 3.6   - 8   + 3.6   - 8   + 3.6   - 8   + 3.6   - 8   + 3.6   - 8   + 3.6   - 8   - 8   + 3.6   + 3.6	sin
8 -5   -3.6   -2.4   5 -6   +96.3   +21.5   2 -7   0.0   +1.7   -2 -8   0.0   +8   -6   +13.0   +3.8   7 -6   -45.4   -23.5   4 -7   +14.7   +4.9   0 -8   0.0   -7 -6   -6.4   -9.8   8 -6   +13.0   +3.8   5 -7   +38.0   +11.8   1 -8   0.0   +6 -6   -6   +2.7   0.0     -6 -6   +2.7   0.0     -7 -6   -6.9   -7   +24.3   +8.4   8 -7   -7   +23.5   +2.9   3 -8   +0.5   -4   -6   +13.3   -1.2   -7 -7   +24.3   +8.4   8 -7   -6.9   -8.9   4 -8   +2.2   +8   -0.0   -4 -6   +13.3   -1.2   -7 -7   +24.3   +8.4   8 -7   -6.9   -8.9   4 -8   +2.2   +8   -2.5   -2 -6   -0.8   +0.7   -5 -7   +2.8   -4.0   -8 -8   +3.6   0.0   6 -8   +12.7   +1   -6   -5.2   -5.1   -4 -7   0.0   +0.8   -7 -8   +6.9   -10.9   7 -8   +6.9   +1.5   -1.1   -6   +5.6   +5.8   -2 -7   +0.5   -1.1   -1.2   8 -8   +3.6	1.2 1.6
-8 -6   + 13.0   + 3.8   7 -6   - 45.4   -23.5   4 -7   + 14.7   + 4.9   0 -8   0.0   - 6 -6   -6   -6   -7   -6   -6   -7   -7	1.2
-7 -6   -6.4   -9.8   8 -6   + 13.0   + 3.8   5 -7   + 38.0   + 11.8   1 -8   0.0   + 6.6 -6   + 2.7   0.0   0   -5.6   -6.9   -8.9   7 -7   + 23.5   + 2.9   3 -8   + 0.5   -4.6   + 1.3   -1.2   -7 -7   + 24.3   + 8.4   8 -7   -6.9   -8.9   4 -8   + 2.2   + 4.5   -2.6   -0.8   + 0.7   -5.7   + 2.8   -4.0   -8 -8   + 3.6   0.0   6 -8   + 12.7   -1.2   8 -8   + 4.5   + 4.5   + 4.5   -1.6   -5.2   -5.1   -4.7   0.0   + 0.8   -7 -8   + 6.9   -10.9   7 -8   + 6.9   + 4.6   + 12.7   -1.2   8 -8   + 3.6   + 3.6   + 4.5   + 4.	3.7
-5 -6   + 2.6   + 1.5   -8 -7   - 6.9   - 8.9   7 -7   + 23.5   + 2.9   3 -8   + 0.5   - 4 -6   + 1.3   - 1.2   -7 -7   + 24.3   + 8.4   8 -7   - 6.9   - 8.9   4 -8   + 2.2   + 2.3   -6   + 2.0   + 2.1   -6 -7   + 4.4   - 5.8     -2 -6   - 0.8   + 0.7   -5 -7   + 2.8   - 4.0   -8 -8   + 3.6   0.0   6 -8   + 12.7   - 1.2   6 -8   + 12.7   - 1.2   8 -8   + 3.6     - 1.0     - 1.2     - 1.2   8 - 8   + 3.6     - 1.2     - 1.2     - 1.2   8 - 8   + 3.6     - 1.2   - 1.2     - 1.2     - 1.2     - 1.2     - 1.2     - 1.2     - 1.2     - 1.2     - 1.2     - 1.2     - 1.2     - 1.2     - 1.2   - 1.2     - 1.2     - 1.2     - 1.2     - 1.2     - 1.2     - 1.2     - 1.2     - 1.2     - 1.2     - 1.2     - 1.2     - 1.2   - 1.2     - 1.2     - 1.2     - 1.2     - 1.2     - 1.2     - 1.2     - 1.2     - 1.2     - 1.2     - 1.2     - 1.2     - 1.2   - 1.2     - 1.2     - 1.2     - 1.2     - 1.2     - 1.2     - 1.2	
-3 -6   + 2.0   + 2.1   -6 -7   + 4.4   - 5.8   -2 -6   -0.8   + 0.7   -5 -7   + 2.8   -4.0   -8 -8   + 3.6   0.0   6 -8   + 12.7   + 4.5   + 4.5   + 4.5   -1 -6   -5.2   -5.1   -4 -7   0.0   + 0.8   -7 -8   + 6.9   -10.9   7 -8   + 6.9   + 4.5   + 6.9   + 4.5   + 6.9   + 4.5	0.5 1.2
-2 -6   - 0.8   + 0.7   -5 -7   + 2.8   - 4.0   -8 -8   + 3.6   0.0   6 -8   + 12.7   + 1.1   -1.1   -6   - 5.2   - 5.1   -4 -7   0.0   + 0.8   -7 -8   + 6.9   -10.9   7 -8   + 6.9   + 4.0   + 1.0   -6   -6   -7   -8   + 6.9   + 1.2   -7   -8   + 6.9   + 1.2   -7   -8   + 6.9   + 1.2   -7   -8   + 6.9   + 1.2   -7   -8   + 6.9   + 1.2   -7   -8   + 6.9   + 1.2   -7   -8   + 6.9   + 1.2   -7   -8   + 6.9   + 1.2   -7   -8   + 6.9   + 1.2   -7   -8   + 6.9   + 1.2   -7   -8   + 6.9   + 1.2   -7   -8   + 6.9   + 1.2   -7   -8   + 6.9   + 1.2   -7   -8   + 6.9   -7   -8   + 6.9   -7   -8   + 6.9   + 1.2   -7   -8   + 6.9   + 1.2   -7   -8   + 6.9   -7   -8   + 6.9   + 1.2   -7   -8   + 6.9   + 1.2   -7   -8   + 6.9   -7   -8   + 6.9   -7   -8   + 6.9   + 7   -7   -8   + 6.9   + 7   -7   -7   -7   -7   -7   -7   -	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1.2
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	10.9 0.0
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$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	sin
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	329.5 85.8
$ \begin{vmatrix} 4 & 0 & + & 11.6 & - & 7.4 & + & 7.5 & + & 49.4 & + & 7.8 & + & 7.2 & 7 & -2 & - & 1.5 & + & 7.7 & + & 24.8 & + & 11.7 \\ 5 & 0 & + & 1.2 & - & 3.8 & - & 13.1 & - & 31.6 & & & & & & & & & & & & & & & & & & &$	23.3
$ \begin{vmatrix} 5 & 0 & + & 1.2 & - & 3.8 & - & 13.1 & - & 31.6 \\ 6 & 0 & + & 1.8 & 0.0 & + & 27.5 & + & 27.0 \\ 7 & 0 & - & 1.1 & - & 1.1 & - & 34.1 & - & 14.4 \\ 8 & 0 & + & 1.0 & 0.0 & + & 19.0 & 0.0 \\ -5 & -1 & + & 17.4 & + & 4.8 & - & 3.7 & + & 1.3 \\ -4 & -1 & - & 19.3 & + & 1.9 & + & 7.6 & - & 3.4 \\ -3 & -1 & + & 21.1 & + & 4.8 & + & 2.7 & + & 0.2 \\ -2 & -1 & + & 6.9 & + & 79.6 & + & 72.3 & - & 30.3 & + & 33.6 & + & 6.8 \\ -1 & -1 & -1 & 298.8 & - & 56.1 & - & 5.9 & + & 290.8 & - & 156.4 \\ 1 & -1 & -1 & 1310.8 & + & 148.2 & + & 146.4 & + & 239.5 & - & 712.7 & - & 136.9 & 6 & -3 & + & 17.8 & - & 4.8 & + & 1.9 & + & 2.3 & + & 19.4 \\ 1 & -1 & -1 & 1310.8 & + & 148.2 & + & 146.4 & + & 239.5 & - & 712.7 & - & 136.9 & 6 & -3 & + & 17.8 & - & 4.8 & + & 1.9 & + & 2.3 & + & 19.4 & + \\ 1 & -1 & -1 & -1 & -1 & -1 & -1 & -1 $	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	
$ \begin{vmatrix} -4 & -1 & -1 & 9.3 & + & 1.9 & + & 7.6 & - & 3.4 \\ -3 & -1 & + & 21.1 & + & 4.8 & + & 2.7 & + & 0.2 \\ -2 & -1 & + & 6.9 & + & 79.6 & + & 72.3 & - & 30.3 & + & 33.6 & + & 6.8 \\ -1 & -1 & -1 & -2 & 98.8 & - & 56.1 & - & 5.9 & + & 290.8 & -156.4 & + & 148.1 & 4 & -3 & + & 264.1 & - & 91.3 & - & 46.1 & - & 51.2 & + & 165.7 & + \\ -1 & -1 & -1 & 1310.8 & + & 148.2 & + & 146.4 & + & 239.5 & - & 712.7 & - & 136.9 & 6 & -3 & + & 17.8 & - & 4.8 & + & 1.9 & + & 2.3 & + & 19.4 & + \\ \hline \end{tabular} $	•
$ \begin{vmatrix} -3 & -1 & + & 21.1 & + & 4.8 & + & 2.7 & + & 0.2 \\ -2 & -1 & + & 6.9 & + & 79.6 & + & 72.3 & - & 30.3 & + & 33.6 & + & 6.8 & 3 & -3 & + & 715.6 & - & 40.8 & - & 93.8 & - & 902.6 & - & 120.1 & - \\ -1 & -1 & - & 298.8 & - & 56.1 & - & 5.9 & + & 290.8 & - & 156.4 & + & 148.1 & 4 & -3 & + & 264.1 & - & 91.3 & - & 46.1 & - & 51.2 & + & 165.7 & + \\ 0 & -1 & + & 2521.5 & - & 9.2 & - & 274.4 & - & 2319.6 & + & 946.0 & -1066.3 & 5 & -3 & + & 87.3 & - & 26.9 & - & 21.3 & + & 18.1 & + & 55.0 & + \\ 1 & -1 & -1 & 1310.8 & + & 148.2 & + & 146.4 & + & 239.5 & - & 712.7 & - & 136.9 & 6 & -3 & + & 17.8 & - & 4.8 & + & 1.9 & + & 2.3 & + & 19.4 & + \end{vmatrix} $	32.6
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	935.1
0 -1 + 2521.5 - 9.2 - 274.4 - 2319.6 + 946.0 -1066.3   5 -3 + 87.3 - 26.9 - 21.3 + 18.1 + 55.0 + 1 -1 - 1310.8 + 148.2 + 146.4 + 239.5 - 712.7 - 136.9   6 -3 + 17.8 - 4.8 + 1.9 + 2.3 + 19.4 +	238.2 109.8
	49.7 13.1
	10.1
3 -1 + 170.0 - 14.4 - 22.2 + 189.0 + 93.1 + 126.7 8 -3 - 4.9 + 4.3 - 1.6 - 5.4 4 -1 + 60.0 - 18.5 + 4.5 + 46.9 + 30.0 + 21.6	
$ \begin{vmatrix} 5 - 1 \\ 6 - 1 \end{vmatrix} + \begin{vmatrix} 7.9 \\ 15.4 \\ 1 \end{vmatrix} - \begin{vmatrix} 11.4 \\ 2 \end{vmatrix} + \begin{vmatrix} 5.3 \\ 2 \end{vmatrix} + \begin{vmatrix} 2 - 4 \\ 13.6 \\ 2 \end{vmatrix} + \begin{vmatrix} 13.6 \\ 2 \end{vmatrix} + \begin{vmatrix} 8.6 \\ 2 \end{vmatrix} + \begin{vmatrix} 0.4 \\ 2 \end{vmatrix} + \begin{vmatrix} 13.4 \\ 2 \end{vmatrix} + \begin{vmatrix} 13.5 \\ 2 \end{vmatrix} + \begin{vmatrix} $	1.5 0.5
7-1+6.9+8.3+1.6-6.8 $0-4-48.1-24.1-10.2+48.4-9.5+$	5.2
$egin{array}{ c c c c c c c c c c c c c c c c c c c$	58.1
$\begin{vmatrix} -4 & -2 \end{vmatrix} - \begin{vmatrix} 13.7 \end{vmatrix} + \begin{vmatrix} 1.2 \end{vmatrix} - \begin{vmatrix} 0.4 \end{vmatrix} + \begin{vmatrix} 25.9 \end{vmatrix} - \begin{vmatrix} 3 & -4 \end{vmatrix} + 2445.8 - \begin{vmatrix} 526.9 \end{vmatrix} - \begin{vmatrix} 576.6 \end{vmatrix} - \begin{vmatrix} 2365.7 \end{vmatrix} + \begin{vmatrix} 290.1 \end{vmatrix} - \begin{vmatrix} 290.1 \end{vmatrix} - \begin{vmatrix} 3 & -4 \end{vmatrix} + 2445.8 - \begin{vmatrix} 3 & -4 \end{vmatrix} + $	274.1
$\begin{vmatrix} -2 & -2 \end{vmatrix} - \begin{vmatrix} 4.1 \end{vmatrix} + \begin{vmatrix} 9.2 \end{vmatrix} + \begin{vmatrix} 22.3 \end{vmatrix} + \begin{vmatrix} 12.4 \end{vmatrix}$ $\begin{vmatrix} 5 & -4 \end{vmatrix} + \begin{vmatrix} 204.0 \end{vmatrix} - \begin{vmatrix} 65.5 \end{vmatrix} - \begin{vmatrix} 43.2 \end{vmatrix} - \begin{vmatrix} 113.2 \end{vmatrix} + \begin{vmatrix} 75.9 \end{vmatrix} + \begin{vmatrix} 113.2 \end{vmatrix}$	<b>43</b> 9.8
$ \begin{vmatrix} -1 & -2 \end{vmatrix} + 129.5 \begin{vmatrix} + 109.7 \end{vmatrix} + 86.1 \begin{vmatrix} -135.9 \end{vmatrix} + 63.1 \begin{vmatrix} -15.3 \end{vmatrix} 6 - 4 \begin{vmatrix} + 39.5 \end{vmatrix} - 14.6 \begin{vmatrix} -13.4 \end{vmatrix} - 13.4 \begin{vmatrix} -21.1 \end{vmatrix} + 31.9 \begin{vmatrix} + 30.6 \end{vmatrix} - 2 \begin{vmatrix} -3339.0 \end{vmatrix} + 294.1 \begin{vmatrix} + 393.6 \end{vmatrix} + 3296.3 \begin{vmatrix} -428.2 \end{vmatrix} + 589.8 \begin{vmatrix} 7 & -4 \end{vmatrix} + 31.2 \begin{vmatrix} -17.1 \end{vmatrix} - 8.3 \begin{vmatrix} + 1.9 \end{vmatrix} + 1.9 $	439.8 162.0 24.5
1 -2 +10242.4 -1049.0 -1302.1 -10042.0 -1317.9 -1799.0 8 -4 - 13.2 + 6.9 - 2.7 - 16.7 2 -2 + 337.0 + 64.6 + 21.0 - 820.1 - 303.0 - 271.8	439.8 162.0 24.5

	Retained Terms of the Forces.																											
		i'		X	C1			7	Ľı				Zı		. ا	i'	L		K1			7	71			7	Z <sub>1</sub>	
	٠,	•		cos		sin		COS		sin		COS		sin	Ľ	•		сов		sin		COS		sin	Г	COS		sin
_	1	-5		2.3	٠.	4.6		5.3		0.9		33.3	1		9	-6	-	21.0	+	3.9	-	3.9	-	20.8				
	0 1	-5 -5		2.5 46.7		2.0 0.6		8.7 11.0	1	1.4 44.7		14.4 8.7			1	-7	-	6.0	_	13.2	+	4.5	+	<b>6.</b> 9	+	32.3	_	1.5
		-5 -5				44.9				<b>252.9 790.9</b>			1	52.1 168.1	2 3	-				10.3 1.2	1	4.7 12.9		12.5 42.8	•	2.5 5.0	ı	1.0 8.0
	_	_		1037.1		288.1							1	191.4	_			133.3		42.0				120.4		13.2	1 '	27.0
				385.4 119.0		77.0 37.1	_	96.6 38.9		407.2 98.4		18.8 31.6			5 6	-7 -7	•	223.6 149.6	i	•		113.6 79.5		229.7 171.2		15.5 17.1	1 -	50.5 30.6
	7	-5	+	40.8	_	29.4		3.0	-	37.0					7	<b>-7</b>	+	148.6	-	45.4	-	39.2	-	83.3		0.5	1	20.7
81	_	-5 -5	1	16.9 12.4		9.9 3.4	<u>-</u>	19.2 3.3		29.0 12.3					8 9	-7 -7				7.7 12.0		6.3 11.9		45.1 9.7				
		_				<b>C</b> O		10.4		10.0					١.	٥	١.	= 0		18 5		10 5		F 1				
_		-6 -6		11.2 1.7	1	6.2 7.3		19.4 24.2		19.9 11.4	_	30.3	-	2.1	0	-8 -8	•	-		17.5 19.0		_		5.1 1.2	+	24.0	+	1.6
	-	-6 -6		0.3 0.4		9.0 6.0		26.7 25.9		0.5 16.4		25.7 8.3		1.6 2.4	1 2	–8 –8				16.4 12.6				9.1 12.1		<b>37.</b> 9 <b>16.</b> 8		1.9 2.3
		-6		37.7		10.0		15.1		64.1		9.8	1		3	–¢ –8	1	8.7		7.3		6.3	1	9.4		1.9		0.8
		_	•	175.4 494.6		55.6 177.8		44.8 181.2		205.8 459.3		25.6 38.5		43.0 98.1	4 5	-8 -8		9.8 <b>62.</b> 0		9.3 <b>26.</b> 9		9.4 <b>2</b> 8.9		10.2 66.9		0.7 5.6		3.1 13.7
	5	-6	+	411.7	_	136.9	-	159.7	-	422.5	+	49.2	-	80.5	6	-8	-	93.5	+	50.5	+	<b>58.</b> 8	+	104.6	-	3.6	+	21.0
		-6 -6	•	228.2 89.2		55.2 22.3		50.9 54.2		192.7 93.4		5.7 10.5		47.5 8.1	7 8	-8 -8		42.2 24.9		4.2 38.7				72.7 10.6	+	5.3	-	9.6
		-6		22.5		8.9		0.8		50.3							Ľ											

For the computation of

$$r^{\circ} R^{\circ} = x_1 \mathbf{X}_1 + y_1 \mathbf{Y}_1$$

and

$$c^{\circ} T^{\circ} = \mathbf{X}_1 \frac{d x_1}{d t} + \mathbf{Y}_1 \frac{d y_1}{d t}$$

we have the above series for  $x_1$  and  $y_1$  with reversed signs, and

These multiplications furnish us now finally the material for the formation of the differential equation for  $r^{\circ} \delta r$ , namely, of

$$\frac{d^3\left(r^{o}\,\delta\,r\right)}{d\,t^{a}} + \frac{\kappa^{a}\left(1+m\right)}{r^{ca}}\left(r^{o}\,\delta\,r\right) = r^{o}\,R^{o} + 2\,fc^{o}\,T^{o}\,d\,t = \Sigma.$$

	Terms of $\Sigma$ retained for integration.														
i,	i'	cos	sin	i,	i'	cos	sin	i,	i'	COS	sin	i,	i'	cos	sin
0	0	+ 9109.8	0.0	-1	-2	- 214.7	- 225.4	4	-4	+8063.0	-1850.3 - 525.3	6	-6	+1013.5	-350.0
2	0	- 7631.9 - 13.2	+ 561.6 - 877.8	0	-2 -2	+ 3113.6 -49502.2	+ 435.3	5 6	-4 -4	+3015.7	- 251.7	8	-6 -6	+ 677.6 + 362.8	-202.9 -129.7
3	0	- 31.4	- 142.2	2	-2	+51251.5	-6036.5	7	-4	+ 195.6	- 60.2				
4	0	+ 27.6	- 5.0	3	-2	+ 8109.5	- 413.2			1		1	-7	+ 28.7	+ 53.2
5	0	- 35.0	- 18.2	4	-2	+ 1518.4	- 473.2	1	-5	+ 77.2	- 40.9	2	-7	+ 157.4	- 70.3
6	0	+ 30.0	- 2.2	5	-2	+ 431.0	- 90.6	2	-5	- 638.2	- 18.8	3	-7	+ 130.5	+ 2.7
7	0	- 29.5	+ 21.7					3	-5	+1875.3	- 439.1	4	-7	- 307.2	+ 62.4
8	0	+ 14.1	- 44.6	0	-3	- 208.1	- 119.9	4	-5	-3827.3	+1280.4	5	-7	+ 609.7	-243.4
9	0	+ 3.0	+ 20.6	1	-3	+ 5649.5	+ 26.7	5	<b>–5</b>	+2916.8	- 851.0	6	-7	- 783.2	+388.8
Į.		ļ i		2	-3	-15678.7	+3104.7	6	<b>-5</b>	+1588.1	<b>- 379.9</b>	7	-7	+ 289.9	-139.6
-2	-1	+ 10.1	- 80.2	3	-3	+20761.9	-3605.4	7	-5	+ 501.0	- 127.7	8	-7	+ 365.4	-123.3
-1	-1	+ 578.1	+ 686.0	4	-3	+ 5454.1	- 628.4	8	5	+ 192.7	- 75.1			1	
0	-1	- 3520.7	- 11.5	5	-3	+ 1309.6	- 321.7	l				2	-8	+ 101.2	+120.2
1	-1	+16549.2	-1084.2	6	-3	+ 330.1	- 126.3	0	-6	- 29.7	- 74.4	3	-8	+ 105.6	+ 96.9
2	-1	- 2803.0	+ 760.2					1	-6	+ 92.7	+ 123.8	4	-8	- 28.5	- 31.8
3	-1	- 261.1	- 495.8	0	-4	+ 67.5	+ 56.3	2	-6	+ 370.1	+ 256.6	5	-8	- 85.7	+ 51.5
4	-1	- 99.9	- 116.9	1	-4	+ 399.3	+ 32.9	3	-6	- 440.1	+ 30.6	6	-8	+ 272.2	-123.8
5	-1	+ 34.7	- 45.4	2	-4	+ 3281.9	- 388.5	. 4	-6	+1089.6	- 344.7	7	-8	- 311.7	+153.9
				3	-4	- 7965.4	+2071.6	5	-6	-1794.8	+ 723.2	8	-8	+ 119.9	+ 17.6

For the computation of the coefficients of integration we have, —

$\log \mu$	3.008587	$\log p_0$	9.87395n		
$\log \frac{365.25}{206266}$	7.248165	" p <sub>1</sub>	0.35322	log	$q_1 0.34788$
$\log \mu'$	2.475858	" p <sub>2</sub>	9.38308	"	$q_2$ 9.37951
" μ —	-0.256752	" p <sub>3</sub>	8.58950	. "	q <sub>3</sub> 8.58670
" μ' <del>-</del>	- 9.724028	" p <sub>4</sub>	7.86982	44	q. 7.86747
μ	1.806142	" p <sub>5</sub>	7.19033	"	$q_5$ 7.19033
$\mu'$	0.529691	" <b>p</b> <sub>6</sub>	6.54407	"	q <sub>6</sub> 6.54407

p and q are the coefficients in the series for  $x_1$  and  $y_1$ .

$\log \frac{1}{ab} 9.288603$	μ 1.806142	μ' 0.529691
$\log \frac{1}{\mu} 9.743248$	2 μ 3.612284	$2 \mu' 1.059382$
_	3 µ 5.418426	$3 \mu' 1.589073$
$\log \frac{1}{a b \mu} 9.031851$	$4 \mu 7.224568$	$4 \mu' 2.118764$
	$5 \mu 9.030710$	$5 \mu' 2.648455$
	$6 \mu 10.836852$	$6 \mu' 3.178146$
	7 μ 12.642996	$7 \mu' 3.707837$
	$8 \mu 14.449136$	$8 \mu' 4.237528$
	9 µ 16.255278	$9 \mu' 4.767219$
•	$10 \mu 18.061420$	
	11 μ 19.867562	

Log of the " Entwickelungs-Factoren."

$$i + 4 \text{ and } i - 4 \begin{cases} +\frac{3}{1}, & +\frac{1}{3} & +\frac{4}{3}, & -\frac{9}{4} & +\frac{15}{1}, & -\frac{1}{3} \\ 4.68480n & 7.33105 & 7.30661n \end{cases}$$

$$i + 8 \text{ and } i - 3 \begin{cases} +\frac{2}{1}, & +\frac{1}{3} & +\frac{3}{3}, & 0 & +\frac{4}{3}, & -1 & +\frac{5}{3}, & -\frac{2}{3} & \cdots \\ 6.02698n & 7.92534 & 7.90573n & 6.40380n \end{cases}$$

$$i + 2 \text{ and } i - 2 \begin{cases} +\frac{2}{3}, & 0 & +\frac{3}{3}, & -1 & +\frac{4}{3}, & -\frac{3}{3} & +\frac{5}{3}, & -\frac{3}{3} & \cdots \\ 8.54206 & 8.52827n & 7.01565n & 5.66881n \end{cases}$$

$$i + 1 \text{ and } i - 1 \begin{cases} +\frac{1}{3}, & 0 & +\frac{2}{3}, & -1 & +\frac{4}{3}, & -\frac{3}{3} & +\frac{4}{3}, & -\frac{3}{3} & \cdots \\ 9.20940 & 9.19653n & 7.65594n & 6.28942n \end{cases}$$

$$i \begin{cases} +\frac{1}{3}, & -1 & +\frac{2}{3}, & -\frac{3}{3} & +\frac{4}{3}, & -\frac{3}{3} & -\frac{4}{3} & -\frac{3}{3} & \cdots \\ 9.98970n & 8.35223n & 6.94297n & 5.62793n \end{cases}$$

The numbers above the logarithms are those which constitute  $\pm z$  in  $i \pm z$ .

	Specimen of the Tables of Divisors.  For the Class $i' = 0$ .														
	TO HIS CHART I U.														
	-4 -8 -9 -1 0 +1 +2 +8 +4 +5 +6 +7 +8 +9														
		9-14119 <sub>m</sub>	9-26613 <sub>n</sub>	9-44221 <sub>m</sub>	9.74825 <sub>m</sub>	œ	9-74325	9-44221	9-26618	9-14119	9-04428	8-96510	8-89615	8-84016	8-78900
-5	9-04428 <sub>m</sub>	8-18547	8-31041	8-48649	8-78753	8-08856 <sub>m</sub>	8-78753 <sub>m</sub>	8-48649 <sub>n</sub>	8-31041 <sub>m</sub>						
-4	9-14119 <sub>m</sub>	ì	8-40732	8-58340	8-88444	8-28238 <sub>m</sub>	8-88444	8-58340 <sub>n</sub>	8 · 40782 <sub>n</sub>	8 · 28238 <sub>n</sub>		]		ĺ	
-8															
-2	9-44221 <sub>R</sub>	1			9-18646	8-88442 <sub>n</sub>	9-18566 <sub>n</sub>	8-88442 <sub>n</sub>	8-70834 <sub>m</sub>	8 • 58840 <sub>n</sub>	8-48649 <sub>n</sub>	8-40781 <sub>n</sub>			
-1	9-74325 <sub>m</sub>					9-48650 <sub>m</sub>	9-48650 <sub>m</sub>	9-18546 <sub>m</sub>	9-0098R <sub>m</sub>	8-88444 <sub>m</sub>	8-7875 <b>3</b> <sub>n</sub>	8-70685 <sub>n</sub>	8-64140 <sub>m</sub>		
0	<b>o</b> o						9-48650 <sub>m</sub>	8-88442 <sub>n</sub>	8-53226 <sub>m</sub>	8-28288 <sub>n</sub>	8-08856 <sub>n</sub>	7-98020 <sub>m</sub>	7-79680 <sub>m</sub>	7-68082 <sub>n</sub>	
+1	9-74325							9-18546	9-00988	8-88444	8-78753	8-70635	8-64140	8-58841	8-43235
+2	9-44221								8-70634	8-58840	8-48649	8-40731	8-34036	8-28287	8-23121
+8	9-26618									8-40782	8-31041	8-28128	8-16428	-8-10629	8-05513
+4	9-14119	ļ						[. '			8-18547	8-10629	8-03984	7-98125	7-98019
+5	9-04428			İ				ŀ				8 <b>-0093</b> 8	7-94248	7-88444	7-83328
+6	8-96510												7-86325	7-80526	7-75410
+7	8-89815						}			İ				7-78831	7-68715
+8	8-84016						}			l			l		7-62916

When for this class i' = 0, one of the divisors in  $\frac{1}{(i-\kappa)\,\mu \cdot (i-\kappa')\,\mu}$ , becomes zero we have to put down the negative square of that divisor which retains a real value. This table of the divisor for i' = 0 and for the coefficients of integration  $f_i^0(i+\kappa)$  is changed into the table of the divisors for  $f_i'(i+\kappa)$  by squaring all the numbers and by adding to the logarithms of the squares  $\log(c+c')\,\mu$ . Excepted herefrom are the terms for which c or c' becomes zero. Those terms are to be multiplied by  $\frac{1}{c'\mu}$  or  $\frac{1}{c\mu}$ .

	Specimen of the Tables of the Coefficients of Integration. $\mathbf{i'} = 0.$												
	f-4	f-8	f-2	f-1	f0	f+1	f + 2	f+8	f+4	f+5	f+6	f+7	Σ
i = 0 i = 1 i = 2 i = 3 i = 4 i = 5 i = 6	+0-00008		-0-00084	-0-00906	+0-80113° -0-02582 +0-00082 +0-00081 +0-00008	-0-02582 +0-07717* +0-03052 +0-00427 +0-00073 +0-00015	+0.00082 +0.03052 -0.09931* -0.00371 -0.00073 -0.00015	1	+0-00008 +0-00078 -0-00073 -0-00091 -0-02059* -0-00030 -0-00007	+0-00015 -0-00015 -0-00019 -0-00030 -0-01282*	-0-00004 -0-00004 -0-00007 -0-00012 -0-00877*		+0.25290 +0.07846 -0.07356 -0.03920 -0.02179 -0.01848 -0.00900
i = 7												-0-00689*	-0-00639

In such a table it is only necessary to compute the values on one side of the diagonal line of asterisks, since the values appear on both sides arranged in the same manner as  $[a\ b]$ ,  $[a\ c]$ ,  $[b\ c]$ , with respect to  $[a\ a]$ ,  $[b\ b]$  in the method of least squares. By means of the horizontal sums z the coefficients are checked because of

$$\mathcal{Z}f_{i}^{i'}(i+*,i') = -\frac{(p_0+p_1+p_2....)}{ab} \left\{ \frac{q_1}{(i+1,i')(i-1,i')} + \frac{2q_2}{(i+2,i')(i-2,i')} + \frac{8q_3}{(i+3,i')(i-3,i')} \right.$$

	r° ð r											
i,	i'	cos	sin	i, i'	cos	sin	i, i'	COS	sin	i, i'	COS	sin
0	0	+ 41.67t	0.0	0 -	+ 9933.9	- 754.7	5 -4	- 61.9	+11.5	-1 -7	+ 1.3	- 3.6
1	0	-125.63t	-3697.52t	1 -9	-12287.5	+1166.2	6 -4	- 15.0	+ 3.9	0 -7	+ 7.9	- 21.8
2	0	- 13.46t	- 397.69t	2 -9	-21290.5	+2442.7	7 -4	- 1.8	+ 0.5	1 -7	+ 64.1	-210.9
3	0	- 2.61t	- 64.08	3 -	- 2306.4	+ 229.2		٠ .		2 -7	- 31.3	+ 22.5
4	0	0.0	- 12.234	4 -9		+ 50.1	-1 -5	+ 2.2	- 0.7	3 -7	+148.5	+ 87.3
5	0	0.0	- 2.51t	5 -9	- 46.1	+ 6.0	0 -5	+ 14.2	- 4.0	4 -7	+ 51.3	+ 3.4
				1			1 -5	+127.2	- 9.3	5 -7	- 19.2	+ 10.6
0	0	+ 2936.7	0.0	-3 -3		- 0.6	2 -5	-138.4	-29.3	6 -7	+ 17.3	- 8.0
1	0	- 989.2	+ 19.8	-2 -3		- 3.4	3 -5	-433.7	+80.6	7 -7	- 3.7	- 1.9
2	0	- 210.4	+ 105.3	-1 -3		- 23.1	4 -5	+184.0	-67.4	8 –7	- 3.3	+ 1.1
3	0	- 25.8	+ 11.2	0 -8		- 192.4	5 -5	77.9	+21.7		· .	1
4	0	- 6.2	+ 1.2	1 -8		+1118.1	6 –5	- 25.7	+ 5.8	0 -8	+ 1.7	+ 2.1
				2 -3		-3229.5	7 –5	- 5.8	+ 1.5	1 -8	+ 13.0	+ 15.7
-3	-1	- 15.5	- 3.7	3 -3		+ 30.7	8 –5	- 1.4	0.0	2 -8	+ 14.3	+ 22.4
-2	-1	- 111.9	- 15.2	4 -3	1	- 13.5	<u> </u>	ļ		3 -8	+ 32.1	+ 24.5
-1	-1	- 969.8	- 293.3	5 -3		- 0.4	-1 -6	+ 0.2	+ 1.2	4 -8	+ 13.9	+ 12.8
0	-1	- 4613.1	+ 328.3	6 -	- 9.6	+ 2.4	0 -6	+ 6.3	+17.9	5 -8	+ 5.6	- 1.1
1	-1	+10401.0	- 584.0	١.	1		1 -6	- 27.4	+15.8	6 -8	- 6.3	+ 3.1
2	-1	+ 2177.7	- 221.7	-2 -4		- 0.4	2 -6	+ 28.2	+51.6	7 -8	+ 4.5	- 2.3
3	-1	+ 291.9	+ 3.1	-1 -4	+ 4.6	- 2.3	3 -6	+279.0	+42.3	8 –8	- 1.2	0.0
4	-1	+ 52.3	- 0.4	0 →		- 33.7	4 -6	- 55.1	+30.5			
1 _				1 1 -		+ 96.8	5 -6	+ 59.2	-21.5	6 -9	+ 1.5	- 0.9
-3	-2	+ 8.3	+ 1.5	2 -	1	- 145.9	6 -6	- 17.3	+ 6.0	7 -9	- 2.2	+ 1.0
-2	-2	+ 142.5	- 2.2	3 -		- 288.0	7 -6	<b>- 7.9</b>	+ 2.4	8 -9	+ 0.4	- 0.8
	_2	+ 980.0	+ 17.4	4 -	- 264.9	+ 66.3	8 -6	<b>- 2.</b> 8	+ 1.0	9 -9	- 0.1	0.0

For the formation of the differential equations for  $\xi_1$  and  $\eta_1$  it is necessary to multiply  $r^{\circ} \delta r$  with  $\frac{3 \kappa^2}{\kappa^{\circ}} x_1$  and  $\frac{3 \kappa^2}{r^{\circ}} y_1$ .

Having performed these multiplications we obtain for integration

$$\frac{d^{2} \xi_{1}}{d t^{2}} + \frac{\kappa^{2} (1+m)}{r^{03}} \xi_{1} = X_{1} + \frac{3 \kappa^{2} (1+m) x_{1}}{r^{03}} (r^{0} \delta r) = \xi_{1} \Sigma,$$

$$\frac{d^{2}\eta^{1}}{dt^{2}} + \frac{\kappa^{2}(1+m)}{r^{\cos}} \eta_{1} = Y_{1} + \frac{3\kappa^{2}(1+m)y_{1}}{r^{\cos}} (r^{\circ} \delta r) = {}^{\eta_{1}}\Sigma,$$

and simply

$$\frac{d^2\zeta_1}{d\ell^2} + \frac{\kappa^2(1+m)}{r^{cs}}\zeta_1 = \mathbf{Z}_1.$$

	-									
į	į,	ξ <sub>1</sub>	Σ	ηι	Σ	i, i'	Ę	$^{1}\mathcal{Z}$	η,	Σ
,		COS	sin	COS	sin		cos	sin	cos	sin
0	0	- 293.0t	0.0	- 8731.9t	0.0	4 -1	+ 9901.6	- 687.9	+ 639.9	+ 9298.1
1	ō	- 157.8t	+ 878.71	- 6465.1t	+ 28.9t	5 -1	+ 4485.2	- 293.2	+ 293.5	+ 4324.0
2	0	- 300.4t	- 7176.5t	+ 5387.1t	- 241.4t	6 -1	+ 1848.4	- 128.2	+ 108.6	+ 1792.8
3	0	- 204.0€	- 5548.1t	+ 4985.9t	- 187.2t	7 -1	+ 707.7	- 35.2	+ 42.0	+ 685.0
4	0	- 103.34	- 2019.2t	+ 2747.8	- 98.1t					
5	0	- 44.5¢	- 1300.9t	+ 1255.34	- 42.8t	-5 -2	+ 642.1	+ 12.6	+ 10.6	- 722.2
6	0	- 17.7t	- 525.2t	+ 523.1t	- 16.7t	-4 -2	+ 1486.2	+ 29.1	+ 24.1	- 1432.4
7	0	- 6.5t	- 205.24	+ 214.34	- 5.8t	-3 -2	+ 2815.4	+ 106.1	+ 100.8	- 2580.8
8	0	- 2.5t	- 86.7t	+ 72.6t	- 2.2t	-2 -2	+ 2684.3	+ 452.4	+ 471.5	- 1797.5
9	ō	- 1.0¢	- 29.0¢	+ 9.4t	- 0.3t	-1 -2	- 7484.1	+ 1745.8	+ 1767.9	+10518.1
10	ŏ	- 0.1 <i>t</i>	- 3.9t	+ 1.6t	- 0.0	0 -2	-54730.2	+ 6308.1	+ 6527.9	+64290.9
	- 1	Снеск.		1	BCK.	1 -2	-33213.1	+ 4804.2	+ 6058.7	+63561.3
1 00 1	D <sub>0</sub> +1		$\sum b_m^t q_{m^c} + 0.2$		= -1.3	2 -2	-43437.6	+ 5071.7	- 911.5	- 7514.1
II	J - 4 -	at I m	- Magna	1	_ ,	3 -2	-67573.3	+ 7582.9	- 6459-1	-56034.2
0	0	- 1018.5	0.0	+ 266.3	0.0	4 -2	-43662.0	+ 4902-5	- 4521.2	-40231.6
1	0	+15182.5	- 28.1	+ 162.6	+15375.4	5 -2	-21547.8	+ 2409.7	- 2290.0	-20489.0
2	0	+ 5564.4	+ 173.9	- 34.7	+ 5736.0	6 -2	- 9236.7	+ 1028.4	- 1022.1	- 8963.1
3	0	+ 1767.9	+ 254.2	- 196.5	+ 1794.1	7 -2	- 3643.3	+ 418.6	- 375.7	- 3553.1
4	0	+ 493.1	+ 187.1	- 172.2	+ 546.1	8 -2	- 1396.3	+ 152.9	- 165.9	- 1351.0
5	0	+ 117.3	+ 92.0	- 105.0	+ 88.9			1	1	
6	0	+ 27.6	+ 40.7	- 12.6	+ 52.6	-4 -3	- 651.5	- 85.0	- 81.9	+ 655.5
7	0	+ 12.2	+ 15.1	- 50.0	÷ 14.3	-3 -3	- 1374.1	- 208.3	- 196.8	+ 1267.2
						<b>-2 -3</b>	- 1941.2	- 493.8	- 469.4	+ 1623.6
-5	-1	- 406.2	- 85.9	- 90.4	+ 427.5	-1 -3	+ 389.6	- 1075.9	- 986.1	- 1536.3
-4	-1	- 982.6	- 212.8	- 197.2	+ 914.4	0 -3	+15466.8	- 2231.2	- 1968.7	-19070.7
-3	-1	- 1719.4	- 439.9	- 409.9	+ 1568.1	1 -3	+32924.0	- 7039.1	- 6188.3	-44406.5
-2	-1	- 1636.9	- 655.5	- 551.2	+ 1006.6	2 -3	+11266.3	- 1666.8	- 3073-1	-16238.7
-1	-1	+ 4032.3	- 612.7	- 215.2	- 6026.3	3 -3	+39386.4	- 6595.6	+ 5534.2	+32608.6
0	-1	+24638.8	- 2220.4	- 1199.6	-30750.9	4 -3	+24184.2	- 4154.3	+ 3749.3	+22344.9
1	-1	+ 2392.2	- 642.0	- 633.8	-16574.1	5 -3	+11285.6	- 1951.6	+ 1832.9	+10799.1
2	-1	+22618.3	- 1611.4	+ 943.3	+16076-1	6 -3	+ 4654.2	- 807.3	+ 782.0	+ 4512.8
3	-1	+18183.6	- 1301.6	+ 1150.8	+16159.8	7 -3	+ 1770.4	- 314.5	+ 294.3	+ 1739.2
ــــــــــــــــــــــــــــــــــــــ	÷	13230							1	

i,	· i'	ξι	2	η	Σ	i, i'	ξį	Σ	71	Σ
		COS	sin	CO8	sin		cos	sin	COS	sin
8	-3	+ 643.7	- 106.8	+ 106.7	+ 636.1	2 -6	+ 584.2	+ 270.1	+ 47.8	- 556.3
ĺ			•		1	3 -6	+ 437.0	+ 203.4	- 151.2	- 126.5
-2	-4	+ 310.6	- 68.2	- 56.7	288.9	4 -6	+ 358.0	+ 366.4	- 36.9	+ 995.9
-1	-4	+ 810.7	- 101.6	- 103.4	- 799.2	5 –6	+ 709.5	<b>+ 42.1</b>	- 309.6	- 87.7
0	-4	+ 2202.0	- 221.4	- 169.3	- 2134.8	6 -6	+ 450.4	- 3.1	- 84.7	+ 71.9
1	-4	+ 6730.5	- 729.0	- 615.5	- 6538.2	7 –6	+ 162.7	+ 5.0	- 73.3	+ 0.4
2	-4	+ 1955.1	- 235.7	- 317.0	- 2674.6				1	
3	-4	+ 7290.6	- 885.8	- 204.7	+ 1960.0	-2 -7	+ 54.5	- 161.6	- 161.9	- 67.0
4	-4	+ 6102.3	- 860.7	+ 698.4	+ 4901.3	-1 -7	+ 151.6	- 346.6	- 304.2	- 128.3
5	-4	+ 2681.5	- 386.5	+ 300.1	+ 2412.3	0 -7	+ 239.2	- 450.1	- 367.1	- 210.4
6	-4	+ 906.7	- 113.1	+ 92.0	+ 861.4	1 -7	+ 259.1	- 101.8	+ 234.0	- 144.9
7	-4	+ 293.8	- 37.9	+ 14.6	+ 267.7	2 -7	+ 602.1	- 301.2	+ 692.7	- 249.8
i						3 -7	+ 235.5	- 165.7	+ 292.0	- 25.8
-1	-5	+ 23.6	- 23.9	- 30.9	- 13.7	4 -7	+ 533.2	+ 74.6	- 117.3	+ 228.1
0	-5	- 124.0	- 35.9	- 13.9	+ 166.0	5 -7	+ 140.3	+ 187.4	+ 9.8	+ 518.6
1	-5	- 770.1	- 13.7	+ 9.7	+ 895.9	6 -7	+ 283.7	+ 4.4	- 151.0	- 31.0
2	-5	- 414.6	+ 12.5	+ 81.9	+ 801.6	7 -7	+ 228.1	- 28.0	- 54.4	+ 9.6
3	-5	- 1078.9	+ 128.4	+ 243.3	+ 400.4					1
4	-5	- 210.8	- 143.9	- 378.3	- 1848.4	-1 -8	+ 49.6	+ 35.3	+ 32.3	- 47.1
5	<b>-5</b>	- 18.1	- 108.7	- 24.7	- 603.6	0 –8	+ 85.2	+ 114.7	+ 104.7	- 75.5
6	-5	- 169.1	- 27.5	- 32.8	- 308.5	1 -8	+ 99.9	+ 107.1	+ 71.3	- 74.1
7	<b>-5</b>	- 155.7	- 8.3	- 20.1	- 207.0	2 -8	+ 166.9	+ 158.9	+ 46.6	- 73.9
8	-5	124.0	+ 25.8	- 33.9	- 128.7	3 -8	+ 121.3	+ 131.4	- 50.9	+ 24.9
ł				į.		4 -8	+ 123.3	+ 129.5	- 86.5	+ 104.0
-1	-6	+ 71.7	+ 112.7	+ 134.3	- 55.7	5 -8	+ 154.8	+ 65.2	- 107.3	+ 30.4
0	-6	+ 164.4	+ 183.6	+ 112.6	- 154.6	6 -8	- 27.9	+ 89.5	+ 13.8	+ 155.1
1	-6	+ 453.6	+ 265.6	+ 173.0	- 434.8	7 -8	+ 57.3	+ 18.4	- 40.2	- 55.8

The integration of the preceding three differential equations gives finally the perturbations of the rectangular co-ordinates.

i, i'	ફ		1	71	č	1
·	cos	sin	` COS	sin	cos	sin
0 0 1 0 2 0 3 0 4 0 5 0	- 84.94t - 4.74t + 25.65t + 8.30t + 2.50t + 0.68t	0.0 +4279.97 <i>t</i> +1241.89 <i>t</i> + 325.86 <i>t</i> + 86.21 <i>t</i> + 22.98 <i>t</i>	-1022.41t -4154.40t -1226.46t - 322.92t - 85.92t - 22.70t	0.0 - 11.92t + 24.98t + 8.27t + 2.37t 0.0	+ 148.67t - 448.23t - 48.01t - 7.72t - 1.47t - 0.31t	0.0 + 493.85t + 53.12t + 8.56t + 1.63t + 0.34t
6 0 7 0	+ 0.16 <i>t</i> 0.0	+ 6.19t + 1.31t	- 6.02t - 1.37t	0.0	- 0.07t 0.0	+ 0.08 <i>t</i> 0.0
0 0 1 0 2 0 3 0 4 0 5 0 6 0	- 699.7 +1118.5 + 463.6 + 100.7 + 23.3 + 5.8 + 0.8	0.0 - 5.6 - 31.7 - 15.4 - 5.2 - 1.5 - 0.4	+ 75.5 - 9.4 + 28.9 + 13.1 + 4.9 + 1.7 + 0.1	0.0 + 901.6 + 433.4 + 97.4 + 21.1 + 6.1 + 0.5	- 202.6 + 120.9 + 38.2 + 5.2 + 0.8 + 0.2	0.0 + 143.4 + 42.2 + 6.6 + 1.0 + 0.2
-5 -1 -4 -1	+ 4.1 + 32.1	+ 1.1 + 3.7	+ 1.0 + 3.5	- <b>4.0</b> - 32.4	0.0 + 0.8	- 0.9

	8	i	17	h	ζ	1
i, i'	COS	sin	CO8	sin	COS	sin
-3 -1 -2 -1 -1 -1 0 -1 1 -1 2 -1 3 -1 4 -1 5 -1 6 -1 7 -1	+ 122.3 + 494.5 + 2206.5 + 7732.7 - 1340.7 - 3739.2 - 1092.5 - 300.6 - 79.0 - 21.9 - 6.3	+ 11.8 + 26.8 - 55.3 - 671.7 - 82.3 + 227.2 + 72.3 + 19.9 + 5.0 + 1.3 0.0	+ 11.8 + 26.3 - 72.4 - 325.3 - 0.9 - 192.7 - 70.3 - 19.6 - 5.4 - 1.1 0.0	- 122.9 - 491.7 - 2188.4 - 7809.7 - 1289.8 - 3658.9 - 1081.8 - 300.2 - 84.8 - 20.7 - 6.1	+ 4.2 + 22.7 + 226.2 + 428.1 - 554.6 - 202.1 - 22.9 - 4.2 - 0.6	- 4.5 - 26.9 - 236.6 - 312.4 + 231.4 - 114.3 - 10.7 - 1.6 - 0.3
-5 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2	- 6.6 - 50.0 - 192.0 • 778.1 - 3613.0 -19149.5 - 8330.7 +10930.4 + 4932.9 + 1507.9 + 428.2 + 122.5 + 30.7	- 0.2 + 1.9 + 7.5 + 36.1 + 213.1 + 2127.3 + 1305.0 - 1159.0 - 540.5 - 166.7 - 47.6 - 13.7	- 0.2 + 2.0 + 7.8 + 36.1 + 218.7 + 2083.7 + 754.2 + 1065.5 + 540.7 + 166.1 + 47.9 + 12.7 + 3.0	+ 7.2 + 52.5 + 192.5 + 779.4 + 3600.3 +19003.2 + 9254.2 +10367.5 + 4849.2 + 1497.3 + 432.3 + 112.6 + 29.9	- 1.7 - 9.2 - 72.0 - 428.6 + 525.7 + 244.1 + 3.7 + 1.5 + 0.3	+ 2.1 + 12.0 + 85.4 + 600.3 - 787.6 - 146.5 - 46.1 - 7.4 - 1.4
8 4 7 7 7 7 7 7 7 7 7 7 7 7 8	+ 8.0  - 1.9 + 65.9 + 245.3 + 1128.7 + 5724.9 + 9598.9 - 5031.4 - 3779.0 - 1034.5 - 268.1 - 80.4 - 17.7 - 4.0	- 0.8 + 3.0 + 3.6 + 13.5 + 45.6 + 4.2 - 2097.8 - 17.9 + 539.8 + 161.6 + 43.2 + 13.6 + 3.1 + 0.7	+ 0.9 + 2.8 + 3.5 + 13.2 + 42.7 - 15.3 - 1894.6 + 509.0 - 523.1 - 156.4 - 42.6 - 9.6 - 3.0 - 0.6	+ 7.7  + 4.8  - 66.1  - 263.7  - 1120.9  - 5630.2  - 9736.8  - 2272.5  - 3638.3  - 1022.7  - 269.3  - 56.7  - 17.2  - 3.9	+ 0.6 + 3.3 + 21.1 + 187.9 + 145.1 - 842.5 - 69.4 - 18.6 - 3.7 - 0.7	- 0.7 - 3.6 - 22.1 - 208.4 - 246.1 + 1273.3 + 141.1 + 16.8 + 3.0 + 0.5
14 14 19 14 14 14 14 14 14 14 14 14 14 14 14 14	- 1.1 + 1.4 - 3.2 - 8.9 + 1.4 + 1826.7 + 748.2 - 833.4 - 294.8 - 72.0 - 14.5 - 3.4	+ 1.4 + 1.2 - 12.1 - 182.2 - 120.8 + 99.3 + 40.7 + 10.1 + 1.8 + 0.3	+ 0.9 + 1.2 - 22.6 - 135.1 - 111.6 - 1.6 - 33.9 - 8.1 - 1.8	+ 1.1 - 1.3 + 2.7 + 9.3 - 4.0 - 1854.9 - 32.3 - 402.4 - 250.5 - 66.4 - 16.4 - 2.9	+ 4.3 + 27.9 + 59.7 - 131.7 - 56.4 - 2.5 - 2.4 - 0.5	- 0.3 - 2.5 - 21.9 - 91.2 + 217.7 + 90.2 + 14.8 + 0.9
-2 -5	- 1.6			+ 1.7		

. ,		i	1	71	ž.	ol .		
i, i'	COS	sin	cos	sin	COS	sin '		
-1 -5	- 10.1	+ 1.9	+ 2.1	+ 10.4	- 2.1	+ 0.2		
0 -5	- 47.7	+ 7.9	+ 4.1	+ 46.9	+ 1.8	+ 1.3		
1 -5	- 222.1	- 13.4	- 15.2	+ 218.3	- 11.5	+ 10.6		
2 -5	- 148.9	+ 21.4	+ 52.2	+ 188.6	+ 13.8	- 9.1		
3 -5	+ 204.2	- 30.9	- 40.0	+ 7.4	+ 20.9	- 39.4		
4 -5	+ 20.8	+ 7.2	+ 20.2	+ 113.3	- 5.5	+ 86		
5 –5	+ 2.5	+ 2.9	+ 1.1	+ 20.6	+ 0.6	+ 2.5		
6 –5	+ 3.1	- 0.5	+ 0.5	+ 6.1	- 0.5	1		
7 –5	+ 1.7			+ 2.4				
8 –5	+ 0.9			+ 0.9				
-2 -6	+ 0.7	+ 0.3	+ 0.2	- 0.7				
-1 -6	+ 1.3	- 2.8	- 4.2	- 1.9	+ 1.2			
0 -6	+ 14.0	- 2.3	+ 2.1	- 14.4	- 4.0	- 0.3		
1 –6	+ 191.1	+ 141.0	+ 126.8	- 187.8	- 14	- 2.7		
2 -6	+ 166.8	+ 64.2	- 62.6	- 66.6	+ 2.7	- 2.5		
3 -6	- 153.2	- 78.5	+ .95.3	- 77.5	- 14.6	+ 22.4		
46	- 37.1	- 32.5	+ 11.8	- 87.9	+ 1.6	- 5.5		
56	- 25.6	- 3.1	+ 11.6	- 1.8	- 1.7	+ 2.6		
6 –6	- 9.0	- 0.3	+ 1.9	- 2.2		+ 0.9		
76	- 2.2		+ 0.9					
-3 <b>-7</b>	- 0.6	+ 0.5	- 0.2	+ 0.4	•			
-2 -7	- 2.0	+ 4.3	+ 4.3	+ 2.1				
-1 -7	- 9.4	+ 16.8	+ 15.9	+ 9.2	- 1.9			
0 -7	- 41.5	+ 57.1	+ 54.6	+ 41.9	- 5.3	- 0.5		
1 -7	- 237.0	+ 146-4	+ 103.9	+ 234.6	- 83.3	- 5.1		
2 -7	+ 162-0	- 86.7	+ 110.3	- 238.0	+ 29.9	- 4.7		
3 -7	+ 290.3	- 153.9	+ 137.5	+ 272.2	- 8.9	+ 17.8		
4 -7	20.6	- 30.8	+ 37.4	0.0	- 2.5	+ 4.9		
5 –7	- 2.3	- 11.4	+ 4.1	- 17.7	+ 0.3	- 1.6		
6 -7	- , 5.4	- 1.0	+ 4.1	+ 0.5	- 0.4	+ 0.7		
7 –7	- 2.4	- 0.3	+ 1.3	- 0.3				
-1 -8	- 1.6	1.4	- 1.4	+ 1.7				
0 -8	- 5.8	- 8.3	8.4	+ 6.1	- 0.5			
1 -8	- 16.8	- 21.4	- 22.0	+ 18.8	+ 15.5	- 1.0		
2 -8	+ 46.1	+ 43.3	+ 39.6	- 43.5	+ 1.4	- 0.7		
3 -8	+ 44.0	+ 50.4	- 46.7	+ 39.6	- 4.0	+ 0.9		
4 –8	- 12.4	- 11.7	+ 9.6	- 14.1	- 0.4	- 0.4		
<b>5</b> –8	- 7.7	- 3.0	+ 5.4	- 2.0	- 0.3	+ 0.7		
6 –8	+ 0.6	- 2.2	- 0.1	- 4.0		- 0.5		
7 -8	- 0.9	+ 0.3	+ 0.6	+ 0.8	<u> </u>	<u> </u>		
Normal Places referred to the Mean Equinox 1854.0.								

Berlin M. T.	а	δ	Berlin M. T.	α	δ
1852, July 1.0	271 35 16.53	- 8 35 16.00	1855, April 26.0	223 23 31.65	- 0 58 16.38
1852, October 1.0	274 56 46.92	-18 24 28.78	1856, October 22.0	39 13 48.02	- 5 12 59.07
1853, January 1.0	322 28 46.75	-16 2 17.53	1858, March 20.0	182 4 41.86	+ 7 34 3.35
1854, January 28.0	128 3 16.18	+12 2 48.34	1859, July 8.0	278 7 52.10	- 9 19 9.96

The perturbations computed with the above coefficients for the times of the normals are: -

ક્ષ	71	ζ,	ξ	η	ζ
+11421	-15176	-2756	+14787	-10133	<b>- 6</b> 858
+ 4084	<b>-19862</b>	<b>-2823</b>	+ 9001	-16524	- 8192
+ 1750	-33592	-2105	+10510	-30074	-11002
+39074	- 4084	+3665	+38902	+ 6322	+ 1899
+ 2042	<b>- 2185</b>	+ 532	+ 2592	- 1580	- 98
+ 1754	-14556	- 380	+ 5556	-12885	<b>- 4268</b>
+ 5642	<b>- 2660</b>	+2672	+ 6360	- 1575	+ 1788
+ 8584	-10494	<b>-4500</b>	+10653	- 6160	- 7252

For  $\xi_1$ ,  $\eta_1$ ,  $\zeta_1$ , the plane of the orbit of Melpomene is the fundamental plane, but  $\xi$ ,  $\eta$ ,  $\zeta$  are referred to the equator. The transformation is effected by means of the formulas on pages 391 and 392.

We derive from  $\pi' = 16^{\circ} 16' 53''.3$ ,  $\Omega' = 19^{\circ} 16' 43''.7$ , and  $i' = 15^{\circ} 28' 17''.2$  for 1854.0:

The computation of the normal places from the osculating elements for 1854.0 with the perturbations  $\xi$ ,  $\eta$ ,  $\zeta$ , gives the following equations of condition for the determination of the corrections of the elements:—

$\begin{array}{cccccccccccccccccccccccccccccccccccc$								
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	+1.72507	-3.46371	+1.76341	-0.01327	+0.11791	- 9.60585	+ 157.29	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	+1.05428	-2.12179	+0.96271	-0.00356	+0.03244	- 5.53250	+ 26.24	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	+0.98888	-1.13494	+0.69111	-0.02955	+0.01693	- 3.91254	- 184.68	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	+1.54040	+3.09070	+1.69341	-0.05026	-0.05610	+ 0.38965	- 508.67	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	+1.05335	-1.21848	+1.51267	-0.04736	+0.35622	+ 5.19856	+ 75.05	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	+3.21295	+1.63979	+2.06075	-0.07675	+0.47456	+33.30130	-1902.90	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	+1.01318	+0.73413	+1.50797	-0.08393	+0.19514	+15.62610	- 219.44	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	+1.85143	-3.64800	+1.80356	-0.01777	+0.07135	+37.14650	- 606.95	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		8 M	δφ	δπ	ðΩ	ði 10	00 δ μ	= 0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	-0.08528	+0.22198	-0.13034	+0.17877	+1.44227	+ 0.73639	- 87.12	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	-0.12241	+0.18470	-0.09555	+0.17529	+0.48963	+ 0.52905	- 26.89	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	+0.12166	-0.18671	+0.08963	+0.12534	-0.11444	- 0.53821	- 35.08	
+0.92431   -0.01619   +0.57207   +0.16001   -1.80113   + 9.04078   - 511.75   -0.27122   -0.25501   -0.39779   -0.21930   +0.73969   - 4.07944   + 93.35	-0.11837	-0.24087	-0.14720	-0.27302	-0.64995	- 0.13495	+ 82.14	
-0.27122 $-0.25501$ $-0.39779$ $-0.21930$ $+0.73969$ $-4.07944$ $+93.35$	-0.25846	+0.20020	-0.38766	-0.08737	+1.41267	- 1.07558	- 23.25	
	+0.92431	-0.01619	+0.57207	+0.16001	-1.80113	+ 9.04078	- 511.75	
-0.04169 +0.15224 -0.08194 +0.20950 +1.35572 - 0.58380 <b>-</b> 67.39 J	-0.27122	-0.25501	-0.39779	-0.21930	+0.73969	- 4.07944	+ 93.35	
	-0.04169	+0.15224	-0.08194	+0.20950	+1.35572	- 0.58380	- 67.39	

From which, by the method of least squares, is obtained: -

$$\delta M = + 12' 16''.46$$
  $\delta \varphi = + 1' 33''.89$   $\delta \pi = - 9' 0''.57$   $\delta Q = + 2' 41''.49$   $\delta i = + 0' 12''.08$   $\delta \mu = + 0''.15125$ 

and thus finally the pure elliptical elements: -

1854, Jan. 0, Washington Mean Time.

$$M = 80^{\circ} 8 5 \ddot{3}.31$$
 $\pi = 15 5 30.95$ 
 $\Omega = 150 3 49.70$ 
 $\Omega = 10 9 16.85$ 
 $\Omega = 12 84 20.18$ 
 $\Omega = 1020''.11977$ 
 $\Omega = 0.3609032$ 
 $M = 15 5 30.95$ 
 $M = 16 7 48.6$ 
 $\Omega' = 16 7 48.6$ 
 $\Omega' = 17 16 5.9$ 
 $\Omega' = 17 16 5.9$ 
 $\Omega' = 18 16 5.9$ 
 $\Omega' = 18 16 5.9$ 
 $\Omega' = 18 16 5.9$ 
 $\Omega' = 18 16 5.9$ 
 $\Omega' = 18 16 5.9$ 
 $\Omega' = 18 16 5.9$ 
 $\Omega' = 18 16 5.9$ 
 $\Omega' = 18 16 5.9$ 

With these elements, and the above perturbations, I have constructed tables which represent the normals as follows:—

Δα COS δ	<b>⊿</b> 8	△ a cos 8	<b>⊿ ð</b>
+1.8	1.5	<b>5.2</b>	+1.2
-3.6	-4.3	+3.8	0.3
2.0	-1.3	5.5	-4.9
1.3	<b>2.3</b>	0.6	+1.4

This result is certainly satisfactory, since the perturbations by Saturn have been neglected.

For curiosity's sake I have computed an approximation of the secular variations of the elements from the terms multiplied by t. They are:—

$$\Delta \pi = + 32.01$$
 $\Delta \Omega = -35.01$ 
 $\Delta i = -0.33$ 
 $\Delta \varphi = +0.68$ 
in one year.

### II. ON THE CONSTRUCTION OF THE TABLES OF MELPOMENE.

BEFORE entering into the details of the construction of the tables, I would take the liberty of making some general remarks on the treatment of asteroids at the present time.

After two oppositions it is possible to determine the elements of an asteroid near enough the truth for computing the perturbations, and I think those by Jupiter are sufficient for our present purposes. Three oppositions, then, admit the more accurate determination of the elements, and after about eight oppositions they can be finally corrected for the computation of the general perturbations of the first order by Jupiter. Preliminary tables constructed upon them will give, for the next fifty years, the ephemeris near enough to find the planet, and for forming normal places. After that, a computer can do something definite; then he may compute the perturbations of the second order by using those known of the first order, or he may find it necessary to recompute the first order with the elements upon which the preliminary tables are based. And only then it will be necessary to calculate the perturbations by Saturn also. Our duty in our time with respect to the asteroids is, to avoid all superfluous work on them, and to get out as soon as possible such preliminary tables. Those asteroids which are of special interest, as, for instance, Leucothea and Euphrosyne for the determination of the mass of Jupiter, must of course be treated in a different manner. For those it will be best to carry on the special perturbations by Saturn, Jupiter, Mars, Earth, and Venus for a number of years.

A number of small terms and equations have been omitted, since six decimal places were found to be sufficient in the tables. If we denote the Arguments in the following manner,

I = - M'	XVI = -M - 3M'	XXXI = 5 M - 4 M
$\mathbf{II} = \mathbf{M} - \mathbf{M}'$	XVII = 4 M - 8 M'	XXXII = 3 M - 8 M'
III = M - 3 M'	XVIII = 5 M - 2 M'	XXXIII = -4M - M'
IV = M - 2 M'	XIX = 3 M - 7 M'	XXXIV = 7 M - 2 M'
V = 2 M - 3 M'	XX = 5 M - 3 M'	XXXV = 5 M - 6 M'
VI = 8 M - 2 M'	XXI = -2 M - 3 M'	XXXVI = 6 M - M'
VII = 2 M - M'	XXII = M - 7 M'	XXXVII = 4M - 5M'
VIII = - M - 2 M'	XXIII = M - 5 M'	XXXVIII = 4M - 7M'
$\mathbf{IX} = -  \mathbf{M} -  \mathbf{M}'$	XXIV = 3 M - 5 M'	XXXIX = M - 8 M'
X = M - 4M'	XXV = -8 M - 2 M'	XL = 7M - 3M'
XI = M	XXVI = M - 6 M'	XLI = - M - 5 M'
XII = 3 M - M'	XXVII = 2 M - 7 M'	XLII = - M - 7 M'
XIII = 3 M - 4 M'	XXVIII = 2 M - 5 M'	XLIII = - M - 4 M'
XIV = -2 M - M'	XXIX = -3 M - M'	XLIV = 5 M - 8 M'
XV = 4M - M'	XXX = 5 M - M'	XLV = 5 M - 7 M'

the perturbations are: -

·	ţ	l	,	i1	ζ	i
	cos	sin	COS	sin	908	sin
0 M M 2 M 3 M 4 M 5 M 6 M	- 84.94t - 4.74t + 25.65t + 8.30t + 2.50t + 0.68t + 0.16t	+4279.97t +1241.89t + 325.86t + 86.21t + 22.98t + 6.19t	-1022.41t -4154.40t -1226.46t - 322.92t - 85.92t - 22.70t - 6.02t	- 11.92t + 24.98t + 8.27t + 2.37t	+ 148.67t - 448.23t - 48.01t - 7.72t - 1.47t - 0.31t - 0.07t	+ 493.85t + 53.12t + 8.56t + 1.63t + 0.34t + 0.08t
7 M	1 0-20	+ 1.31t	- 1.37t		5.5.10	, 0.000
I 21 31 41 51 61 71 81	+ 7732.7 -19149.5 + 5724.9 + 1.4 - 47.7 + 14.0 - 41.5 - 5.8	- 671.7 + 2127.3 + 4.2 - 12.1 + 7.9 - 2.3 + 57.1 - 8.3	- 325.3 + 2063.7 - 15.3 - 22.6 + 4.1 + 2.1 + 54.6 - 8.4	- 7809.7 +19003.2 - 5630.2 - 4.0 + 46.9 - 14.4 + 41.9 + 6.1	+ 428.1 - 428.6 + 187.9 + 27.9 + 1.8 - 4.0 - 5.3 - 0.5	- 312.4 + 600.3 - 208.4 - 21.9 + 1.3 - 0.3 - 0.5
11 211 311 411 511 611 711	- 1340.7 +10930.4 3779.0 - 294.8 + 2.5 9.0 2.4	- 82.3 - 1159.0 + 539.8 + 40.7 + 2.9 - 0.3 - 0.3	- 0.9 + 1065.5 - 523.1 - 33.9 + 1.1 + 1.9 + 1.3	- 1289.8 +10367.5 - 3638.3 - 250.5 + 20.6 - 2.2 - 0.3	- 554.6 + 244.1 - 69.4 - 2.5 + 0.6	+ 231.6 - 146.5 + 141.1 + 14.8 + 2.5 + 0.9
3 III III	+ 9598.9 + 166.8	2097.8 + 64.2	- 1894.6 - 62.6	9736.8 66.6	+ 145.1 + 2.7	- 261.1 - 2.5
IV 2 IV 3 IV 4 IV	- 8330.7 + 748.2 - 153.2 - 12.4	+ 1305.0 - 120.8 - 78.5 - 11.7	+ 754.2 - 111.6 + 95.3 + 9.6	+ 9254.2 32.3 77.5 14.1	+ 525.7 - 131.7 - 14.6 - 0.4	- 787.6 + 217.7 + 22.4 - 0.4
V 2 V	- 5031.4 - 37.1	- 17.9 - 32.5	+ 509.0 + 11.8	- <b>2272.</b> 5 - 87.9	- 842.5 + 1.6	+ 1273.3 - 5.5
VI 2 VI	+ 4932.9 - 14.5	- 540.5 + 1.8	+ 540.7 - 1.8	+ 4849.2 - 16.4	+ 3.7	- 46.1
3 VII 2 VII	- 3739.2 + 1507.9 - 80.4	+ 227.2 166.7 + 13.6	- 192.7 + 166.1 - 9.6	- 3658.9 + 1497.3 - 56.7	- 202.1 + 1.5 - 0.7	- 114.3 - 7.4 + 0.5
VIII 2 VIII	- 3513.0 - 3.2	+ 213.1 + 1.4	+ 218.7 + 0.9	+ 3500.3 + 2.7	- 72.0	+ 85.4
IX 2 IX 3 IX 4 IX	+ 2208.5 - 778.1 + 65.9 - 1.1	- 55.3 + 36.1 + 3.6	- 72.4 + 36.1 + 3.5	- 2188.4 + 779.4 - 66.1 + 1.1	+ 226.2 - 9.2 + 0.6	- 236.6 + 12.0 - 0.7
X 2 X	+ 1826.7 + 46.1	- 182.2 + 43.3	- 135.1 + 39.6	- 1854.9 - 43.5	+ 59.7 + 1.4	- 91.2 - 0.7

			<del></del>					
	<b>.</b>	1		71	,	ζ <sub>1</sub>		
	CO8	sin	cos	sin	COS	sin		
0 XI	- 699.7	•	+ 75.5	•	- 202.6			
XI	+ 1118.5	- 5.6	- 9.4	+ 901.6	+ 129.9	+ 143.4		
2 XI	+ 463.6	- 31.7	+ 28.9	+ 433.4	+ 38.2	+ 42.2		
3 XI	+ 100.7	- 15.4	+ 13.1	+ 97.4	+ 5.2	+ 6.6		
4 XI	+ 23.3	- 5.2	+ 4.9	+ 21.1	+ 0.8	+ 1.0		
5 XI	+ 5.8	- 1.5	+ 1.7	+ 6.1	l			
ХII	- 1092.5	+ 72.3	- 70.3	- 1081.8	- 22.9	- 10.7		
2 XII	+ 122.5	- 13.7	+ 12.7	+ 112.6				
XIII	- 833.4	+ 99.3	- 1.6	- 402.4	- 56.4	+ 90.2		
2 XIII		- 2.2		<b>- 4.0</b> '				
xıv	+ 494.5	+ 26.8	+ 26.3	- 491.7	+ 22.7	- 26.9		
2 XIV	- 50.0	+ 1.9	+ 2.0	+ 52.5				
xv	- 300.6	+ 19.9	- 19.6	- 300.2	- 4.2	- 1.6		
2 X Ÿ	+ 8.0	- 0.8	+ 0.9	+ 7.7				
XVI	+ 1128.7	+ 45.6	+ 42.7	- 1120.9	+ 21.1	- 22.1		
XVII	- 1034.5	+ 161.6	- 156.4	- 1022.7	- 18.6	+ 16.8		
XVIII	+ 428.2	- 47.6	+ 47.9	+ 432.3		- 1.4		
XIX	+ 290.3	- 153.9	+ 137.5	+ 272.2	- 8.9	+ 17.8		
XX	- 268.1	+ 43.2	- 42.6	- 269.3	- 3.7	+ 3.0		
XXI	+ 245.3	+ 13.5	+ 13.2	- 263.7	+ 3.3	- 3.6		
XXII	- 237.0	+ 146.4	+ 103.9	+ 234.6	- 83.3	- 5.1		
XXIII	- 222.1	- 13.4	- 15.2	+ 218.3	- 11.5	+ 10.6		
XXIV	+ 204.2	- 30.9	- 40.0	+ 7.4	+ 20.9	- 39.4		
XXV	- 192.0	+ 7-5	+ 7.8	+ 192.5	- 1.7	+ 2.1		
XXVI	+ 191.1	+ 141.0	+ 126.8	- 187.8	- 1.4	- 2.7		
XXVII	+ 162.0	- 86.7	+ 110.3	- 238.0	+ 29.9	- 4.7		
XXVIII	- 148.9	+ 21.4	+ 52.2	+ 188.6	+ 13.8	- 9.1		
XXIX	+ 122.3	+ 11.8	+ 11.8	- 122.9	+ 4.2	- 4.5		
XXX	- 79.0	+ 5.0	- 5.4	- 84.8	1			
XXXI	- 72.0	+ 10.1	- 8.1	- 66.4	- 2.4	+ 0.9		
XXXII	+ 44.0	+ 50.4	- 46.7	+ 39.6	- 4.0	+ 0.9		
XXXIII	+ 32.1	+ 3.7	+ 3.5	- 32.4	+ 0.8	- 0.9		
VVVV	+ 30.7	- 3.5	+ 3.0	+ 29.9	1	, 06		
XXXV	- 25.6 - 91.0	- 3.1	+ 11.6	- 1.8	- 1.7	+ 2.6		
XXXVI XXXVII	- 21.9 + 20.8	+ 1.3 + 7.2	- 1.1	- 20.7	- 5.5			
XXXVIII	- 20.6		+ 20.2	+ 113.3	1	+ 8.6		
XXXIX	- 20.6 - 16.8	- 30.8 - 91.4	+ 37.4	0.0	- 2.5 + 15.5	+ 4.9		
XL	- 10.6 - 17.7	- 21.4 + 2.1	- 22.0	+ 18.8	+ 15.5	- 1.0		
XLI	- 10.1	+ 3.1 + 1.9	- 3.0	- 17.2	- 2.1	+ 0.2		
XLII	- 9.4	+ 16.8	+ 2.1	+ 10.4 + 9.2	- 2.1 - 1.9	+ 0.2		
XLIII	- 8.9	+ 1.2	+ 15.9 + 1.2		+ 4.3	2.5		
XLIV	- <b>7.7</b>	- 3.0	+ 1.2 + 5.4	+ 9.3 - 2.0	T 400	. – 2.0		
XLV	- 2.3	- 11.4	+ 4.1	- 17.7	0.0	- 1.6		

Tables for the equation of the centre and the radius vector have been superseded by solving Kepler's problem in the manner I have shown in Vol. III. No. 53 of the *Astronomical Journal*, viz.:— If we suppose one of the radii vectores to turn uniformly about one of the foci, describing therefore the mean anomaly,

the other radius vector will then, in not very eccentric ellipses, describe nearly the true anomaly. This auxiliary anomaly, denoting with v', we have, simply,

$$\cot \frac{1}{2} v' = \frac{1-e}{1+e} \cot \frac{1}{2} M.$$

The logarithm of the constant factor  $\frac{1-e}{1+e}$  is for Melpomene = 9.8078595, and log p=0.3398226 for the computation of the radius vector by means of  $r=\frac{p}{1+e\cos v}$ .

The correction c, to be added to v' in order to get the true anomaly v, is given in Table II., with M as the argument. For the construction of this table I had c developed in the following series:—

$$c = -$$
 526.495 sin  $M$   $c = +$  68.825 sin 5  $M$   $c = +$  0.373 sin 9  $M$   $+$  2282.957 sin 2  $M$   $+$  18.848 sin 6  $M$   $+$  0.103 sin 10  $M$   $+$  819.532 sin 3  $M$   $+$  5.096 sin 7  $M$   $+$  0.058 sin 11  $M$   $+$  1.395 sin 8  $M$ 

#### Example for computing a Place from the Tables.

1861, Feb. 5<sup>d</sup> 5<sup>h</sup> 58<sup>m</sup> 15<sup>e</sup> Washington M. T. = Feb. 5<sup>d</sup> 12<sup>h</sup> Berlin M. T.

We write down on a scrap of paper the constants to be used. From Table V. the logarithms of

log e 9.337800	$\log \frac{1-\epsilon}{1+\epsilon}$ 9.807860	$\log p$ 0.339823	$\cos (x_1 x)$ 9.982068	$\cos (y_1 x) \\ 9.427362n$	$\cos (z_1 x) \\ 8.943100$
cos (x <sub>1</sub> y) 9.449004	cos (yı y) 9.96665 <b>6</b>	$\cos(z_1 y) \\ 9.400622n$	$\cos (x_1 z)$ $8.144356n$	cos (yı z) 9.424948	. cos (z <sub>1</sub> z) 9.984015

and from Table VI.,

A'	B!	C'	log sin a	log sin b	$\log \sin c$
105° 84′ 42″.6	16° 53′ 23″.8	357° 0′ 0″.6	9.998323	9.985806	9.425543

M = mean anomaly, and t = time since 1854.0 are taken from Table I.

		2	<b>Y</b>	ŧ		
1861,	<b>84</b> °	42	<b>59</b> .56	+7.00068	cot ½ M 47° 29° 38″.8	9.962142
Feb.	8	47	3.72	0.08488	$\frac{1-e}{1+e}\cot \frac{1}{2}M = \cot \frac{1}{2}v' \qquad 59 \ 80 \ 30.4$	9.770002
5 days	1	25	0.60	0.01369	v 119 1 0.8	
5 hours		3	32.53	0.00057	From Table II. $c$ — 26 10.1	
58 minutes			41.09		v 118 34 50.7	
15 seconds			0.17		cos v	9.679789n
	94	59	17.67	+7.09982	$e \cos v \qquad -0.104133$	9.017589n
					$1 + \cos v \qquad 0.895867$	9.952243
					<i>r</i>	0.387580

Formation of the Arguments from Table III.\*

	I.	П.	m.	IV.	₹.	<b>V</b> I.	VII.	VIII.	IX.
1861,	237.828	322.545	78.202	200.37	162.92	9.81	47.26	30.94	153.11
Feb.	357.425	6.209	1.058	3.63	9.85	21.20	14.99	346.07	348.64
5 days	359.584	1.001	0.171	0.59	1.59	3.42	2.42	357.75	358.17
6 hours	359.979	0.050	0.008	0.03	0.08	0.17	0.12	359.89	359.91
	234-816	329.805	79.439	204.62	174.44	34.60	64.79	14.65	139.83
							02.00	21.00	200.00
		XI.	XII.	XIII.	XIV.	XV.	XVL	XVII.	XVIII.
1861,	316.03	84.72	131.98	125.46	68.40	216.7	268.8	332.4	179.2
Feb.	358.48	8.78	23.78	16.05	339.85	32.6	343.5	27.4	38.8
5 days	359.76	1.42	3.84	2.59	356.75	5.3	357.3	4.4	6.3
6 hours	359.99	0.07	0.19	0.13	359.84	0.3	359.9	0.2	0.3
o mouto	314.26	94.99	159.79	144.23	44.84	<del>254.9</del>	249.5	4.4	224.6
	314.40	34.33	103.73	144.60	34.03	A04.3	A45.0	3.4	224-0
	XIX.	XX.	XXI.	XXII.	XXIII.	XXIV.	XXV.	XXVI.	XXVII.
1001	118.9	57.1	184.1	309.5	193.9	3.3	221.5	71.7	34.2
1861, Feb.	118.9 8.3	36.2	154.1 334.7	350.8	193.9 <b>355.</b> 9	ა.ა 13 <b>.</b> 5	328.5	353.3	359.5
5 days	0.3 1.3	30.2 5.8	355.9	358.5	359.3	2.2	354.9	358.9	359.9
6 hours	0.1	0.3	359.8	359.9	0.0	0.1	359.8	0.0	0.0
O nome	128.6	99.4	154.5	298.7	189.1	19.1	184.7	63.9	33.6
	120.0	99.4	104.0	230.7	109-1	19.1	104.7	03-9	33.0
	xxvIII.	XXIX.	XXX.	XXXI.	XXXII.	XXXIII.	· xxxiv.	xxxv.	XXXVI.
1861,	278.6	343.7	301.4	294.9	356.8	259.0	348.7	50.6	26.1
Feb.	4.7	331.1	41.3	33.6	5.7	322.3	56.3	28.5	50.1
5 days	0.8	355.3	6.7	5.4	0.9	353.9	9.1	4.6	8.1
6 hours	0.0	359.8	0.3	0.3	0.1	359.7	0.5	0.2	0.4
	284.1	309.9	349.7	334.2	3.5	214.9	54.6	83.9	84.7
•									
	•								
	XXXVII.	XXXVIII.	XXXIX.	XL.	XLI.	XLII.	XLIII.	XLIV.	XLV.
1861,	88.0	203.7	187	226	24	140	147	166	<b>2</b> 88
Feb.	22.3	17.1	348	54	338	333	341	23	26
5 days	3.6	2.8	358	9	· 357	356	357	4	4
6 hours	0.2	0.1	0	0	0	0	0	0	0
	114.1	223.7	173	289	359	109	125	193	318

With these Arguments the perturbations are computed from Table IV.

<sup>\*</sup> These Arguments being expressed in degrees and decimals, 360.0, 720.0, or 1080 0, must be subtracted when one of the sums is greater than one of those numbers.

	ર્દા		<b>1</b>		ζ <sub>1</sub>		
	+	-	+	-	+	_	
Terms with t	2608.5		264.9		502.0		$\cos(x_1 x) \xi_1 + 4820.0$
I	1008.2		2527.7		95.0		$\cos(y_1 x) \eta_1 - 265.9$
11	491.3			397.8		50.1	$\cos(z_1 x) \zeta_1 + 49.0$
m		43.5		988.5		21.9	$\xi + 4603.1$
IA	753.4			460.7		8.8	
v	497.6			<b>6</b> 8.8	.96.4		$\cos(x_1 y) \xi_1 + 1412.5$
VI	375.1		318.2	1	ł	2.3	$\cos(y_1 y) \eta_1 + 920.2$
VII		240.2		232.2	·	19.6	$\cos(z_1 y) \zeta_1140.4$
VIII		334.7	109.8		ì	4.8	$\eta + 2192.3$
IX		185.2		217.4		33.9	•
X	136.1		127.3		10.8		$\cos (x_1 z) \xi_1 - 70.0$
XI		119.6	79.7			12.0	$\cos \cdot (y_1 z) \eta_1 + 264.3$
KII	115.2			37.1	1.8		$\cos (z_1 z) \zeta_1 + 537.9$
XIII	73.6			23.1	9.9		ζ + 732.2 Reduction to the appar-
XIV	37.1		20.0	27.5		0.3	ent equinox
XV	5.1	40.0	29.8		0.3		sin (A' + v) 224 9 33.3 9.843018.
XVI		43.8	104.2		1.4	. ~	\$ . 00 00
XVII		101.9		23.5	0.1	1.7	x 0.228921, g 0.9765
XVIII		27.2	12.7	<b>33.</b> 8	1.9		sin (B' + v) 135 28 14.5 9.845888 G 338 24
XX		30.1	12.7	<b>~</b> 0	0.3		$r \sin b$ 0.373386 $\sin (G + \alpha')$ 111 9 9.9697
XXI	8.7			<b>25.</b> 8	0.3	0.5	2 0 3590
XXII		21.7		12.3		0.5	
XXIII	22.1	24.2		15.6	•	3.6	mi (0 + 0) 110 04 01.5 9.900195
XXIV			1	2.0	1.0		r sin c 9.813123
XXV	18.3 19.1			3.5 2.5	0.7 0.1		9.768318
XXVI	19.1 21.2				0.1	0.3	$\cos (G+\alpha) \qquad 9.5573_n$
XXVII	21.2 8.7			11.3 3.9	2.2	0.0	$y + 1.656815$ $\Delta \delta' - 3.42 \ 0.5338_n$
XXVIII	0.7	5.7		17.0	1.2		$\eta$ + 2192
XXIX	7.0		10.2	17.0	0.6		Y -0.614699
XXX	7.0	7.9	0.9		0.0		$\Delta \cos \delta' \sin \alpha' + 1.044308 = 0.018828$
XXXI		6.9	2.0			0.3	x -1.694031
XXXII	4.6			4.4		0.4	ξ + 4603
XXXIII	3.0	2.8	1.6	2.3		0.2	X +0.723955
XXXIV	1.5		2.6				dcos d' cos a'0.965473 9.984740,
XXXV		0.6		0.1			sin a' 9.865861
XXXVI		0.1		2.1			$\tan \alpha' 132 \ 45 \ 13.3 \ 0.034088_{n}$ $\alpha = 132 \ 45 \ 35.5$
XXXVII		0.2	9.5		1.0		
XXXVIII	3.6			2.7		0.1	z +0.586568
XXXIX	1.5	1	2.4			1.5	ζ + 732
XL		0.9	1.5				Z -0.266747
XLI		1.0	0.2			0.2	A sin d' +0.320553 9.505900
XLII	1.9		0.3				A cos d' 0.152967
XLIII	0.6		0.7			0.4	cos d' 9.969240
XLIV	0.8			0.5			$\tan \delta' + 12 \cdot 42 \cdot 5.8 \cdot 9.352933 \qquad \delta = +12 \cdot 42 \qquad 3.4$
XLV	0.6		1.5		0.1		
	6221.4	1198.2	3607.7	2614.1	720.8	162.7	A 0.163727
ξι, ηι, ζι			+ 993.6	~~1.1	+ 558.1	- 0.001	a' and b' are referred to the mean
	3.700980		2.997212		2.746712		equinox 1861.0.
		·		<u> </u>			Indumor 2001ini

My computations for 1861, with the osculating elements for 1854.0 and the special perturbations by Jupiter and Saturn, give for the same time:—

$$a = 132^{\circ} 45^{\circ} 33^{\circ}.3$$

$$\delta = +12 42 2.0$$

$$da = 22$$

$$d\delta = 1.4$$

By this close agreement between the two different computations, the correctness of the tables is satisfactorily proved.

For the computation of an exact opposition ephemeris, it will be necessary only to compute the perturbations from 16 to 16 days from the tables, and then to interpolate them twice in the middle, in order to get them from 4 to 4 days, with which interval such ephemerides are commonly calculated. For an approximate ephemeris for the whole year, the terms multiplied with the time and the first four equations will be sufficient, and also a direct computation of the perturbations only from 40 to 40 days, with afterwards two interpolations in the middle, if the ephemeris is to be computed from 10 to 10 days.

TABLE I.

FOR THE MEAN ANOMALY.

The times are referred to the meridian of Washington.

Years.	M	t	Years.	M	t
1852 B	233 <sup>°</sup> 17 <sup>'</sup> 25.88	- 1.99863	1877	300 42 39.50	+23.00068
1853	336 43 9.59	- 0.99932	1878	44 8 23.22	24.00000
1854	80 8 <b>53.31</b>	0.00000	1879	147 34 6.93	24.99932
1855	183 34 37.03	+ 0.99932	1880 <i>B</i>	251 16 50.77	26.00137
1856 B	287 17 20.86	2.00137	1881	354 42 34.48	27.00068
1857	30 43 4.58	3.00068	1882	98 8 18.20	28.00000
1858	134 8 48.29	4.00000	1883	201 34 1.92	28.99932
1859	237 34 32.01	4.99932	1884 B	305 16 45.75	30.00137
1869 B	341 17 15.85	6.00137	1885	48 42 29.47	31.00068
1861	84 42 59.56	7.00068	1886	152 8 13.18	32.00000
1862	188 8 <b>43.2</b> 8	8.00000	1887	255 33 56.90	32.99932
1863	<b>291 34 26.99</b>	8.99932	1888 <i>B</i>	359 16 40.74	34.00137
1864 B	35 17 10.83	10.00137	1889	102 42 24.45 .	35.00068
1865	138 42 54.55	11.00068	1890	236 8 8.17	36-00000
1866	242 8 38.26	12.00000	1891	309 33 51.88	36.99932
1867	345 34 21.98	12.99932	1892 B	53 16 35.72	38.00137
1868 B	89 17 5.81	14.00137	1893	156 42 19.44	39.00068
1869	192 42 49.53	15.00068	1894	260 8 3.15	40.00000
1870	296 9 33.25	16.00000	1895	3 33 46.87	40.99932
1871	39 34 16.96	16.99932	1896 B	107 16 30.70	42.00137
1872 B	143 17 0.80	18.00137	1897	210 42 14.42	43.00068
1873	246 42 44.51	19.00063	1898	314 7 58.14	44.00000
1874	350 8 28.23	20.00000	1899	57 33 41.85	44.99932
1875	93 34 11.95	20.99932	1900 B	161 16 25.69	+46.00137
1876 B	197 16 55.78	+22.00137			
Months.	M	t	Days.	M	t
January	o° o′ 0.00	+0.00000	1	o 17 0.12	+0.00274
February	8 47 3.72	0.08488	2	0 34 0.24	0.00548
March	16 43 7.08	0.16154	3	0 51 0.36	0.00821
April	<b>25 30 10.78</b>	0.24642	4	1 8 0.48	0.01095
May	34 0 14.38	0.32856	5	1 25 0.60	0.01369
June	42 47 18.10	0.41344	6	1 42 0.72	0.01643
July	51 17 21.68	0.49558	7	1 59 0.84	0.01917
August	60 4 25.40 .	0.58046	8	2 16 0.96	0.02190
September	68 51 29.12	0.66534	9	2 33 1.08	0.02464
October	77 21 32.72	0.74748	10	2 50 1.20	0.02738
November	86 8 36.44	0.83236	20	5 40 2.40	0.05476
Docember .	94 38 40.04	+7.91450	30	8 30 3.60	+0.08214

In Bissextile Years one day must be subtracted from the date in the first two months.

TABLE I.—Concluded.

### FOR THE MEAN ANOMALY.

The times are referred to the meridian of Washington.

Hours.	М	t	Hours.	М	t
	0 42.51	.0.00011	10	9 12.57	. 0 001 40
1		+0.00011	. 13		+0.00149
2	1 25.01	0.00023	14	9 55.07	0.00160
3	2 7.52	0.00034	15	10 37.58	0.00172
4	2 50.02	0.00046	16	11 20.08	0.00183
5 '	3 32.53	0.00057	17	12 2.59	0.00195
6	4 15.03	0.00069	18	12 45.09	0.00206
7	4 57.54	0.00080	19	13 27.60	0.00218
8	5 40.04	0.00092	20	14 10.10	0.00229
9	6 22.55	0.00103	21	14 52.61	0.00241
10	7 5.05	0.00114	22	15 35.11	0.00252
11	7 47.56	0.00126	23	16 17.62	0.00264
12	8 30.06	+0.00137	24	17 0.12	+0.00275
		M			<i>M</i>
	For Minutes.	For Seconds.	•	For Minutes.	For Seconds
1	0.71	0.01	31	21.96	0.36
2	1.42	0.02	32	22.67	0.37
3	2.13	0.03	33 ·	23.38	0.39
4	2.83	0.05	34	24.09	0.40
5	3.54	0.06	35	24.80	0.41
6	4.25	0.07	36	<b>25.5</b> 0	0.42
7	4.96	0.08	37	26.21	0.44
8	5.67	0.09	38	26.92	0.45
9	6.38	0.11	39	<b>27.</b> 63	0.46
10	7.08	0.12	40	28.34	0.47
11	7.79	0.13	41	29.05	0.48
12	8.50	0.14	42	29.76	0.50
13	9.21	0.15	43	30.47	0.51
14	9.91	0.16	44	31.17	0.52
15	10.62	0.17	45	31.88	0.53
16	11.33	0.19	<b>46</b>	32.59	0.54
17	11.55 12.04	0.19	47	33.29	0.55
18	12.75	0.20		34.00	0.57
19	13.46	0.21	48 49	•	0.58
20	· ·			.34.71 25.40	
	14.17	0.23	50	35.42	0.59
21	14.88	0.25	51	36.12	0.60
22	15.58	0.26	52	36.83	0.61
23 24	16.29	0.27	53	37.54	0.62
	17.00	0.28	54	38.25	0.64
<b>25</b>	17.71	0.29	55	38.96	0.65
26 27	18.42	0.31	56	39.67	0.66
<b>27</b>	19.13	0.32	<b>57</b>	40.38	0.67
28	19.84	0.33	58	41.09	0.68
29	20.54	0.34	59	41.80	0.70
30	21.25	0.35	60	42.51	0.71

TABLE II.

FOR THE CORRECTION c TO BE ADDED TO THE AUXILIARY ANOMALY v.

Argument = M. For M > 180° the Argument is 360° - M, and the sign of c to be reversed.

Angument — M. Tot M > 100 and Angument is 000 — M, and all of the object.											
Arg.	c	Diff.	Arg.	c	Diff.	Arg.	с	Diff.	Arg.	c	Diff
°	0 0.00	٠	00.5	+40 58.26	n	450	+39 29.45		~° =	. 6 45 15	
0.0		+68-81	22.5	41 26.80	+28-54	45.0 .5	+39 29.45 39 0.24	-29-21	67.5	+ 8 45.17	-45-84
1.0	+ 1 8.81 2 17.58	68-77	23.0 .5	41 53.88	27-06	46.0	38 30.16	80-08	68.0 .5	7 59.33	45-76
	3 26.26	68-68		42 19.51	25-63		37 59.23	30-98	69.0	7 13.57	45-67
.5	4 34.79	68-68	24.0	42 19-51	24-15	.5 47.0		81-75		6 27.90	45-55
2.0 .5	5 43.14	68-85	.5	43 6.35	22-69		37 27.48	89-55	70.0	5 42.35	45-42
1		68-13	25.0	1	21-21	.5	36 54.93	88-89		4 56.93	45-28
3.0	6 51.27 7 59.10	67-83	.5 ec o	43 27.56 43 47.30	19-74	48.0	36 21.61	84-07	.5 71.0	4 11.65	45-12
.5	9 6.61	67-51	26.0	44 5.57	18-27	.5 49.0	35 47.54	84-79		3 26.53 2 41.58	44-95
4.0	10 13.75	67-14	.5	44 22.37	16-90		35 12.75	85-50	.5 72.0	1 56.82	44-76
-5	10 13.75	66-72	27.0	44 23-37	14.00	-5	34 37.25	96.10	1 /2.0	1 50-62	44-57
5.0	+11 20.47	00-13	.5	+44 37.69	15-82	50.0	+34 1.07	36-18	.5	+ 1 12.25	44.01
.5	12 26.74	+66-27	28.0	44 51.56	+13-87	.5	33 24.25	-36-82	73.0	+ 0 27.90	-44-85
6.0	13 32.50	65-76	.5	45 3.96	12-40	51.0	32 46-80	87-45	.5	- 0 16.23	44-18
.5	14 37.71	65-21	29.0	45 14.90	10-94	.5	32 8.74	88-06	74.0	1 0.13	43-90
7.0	15 42.33	64-62	.5	45 24.40	9-50	52.0	31 30.10	88-64	.5	1 43.78	43-65
.5	16 46.31	63-98	30.0	45 32.46	8-06	.5	30 50.90	39-20	75.0	2 27.17	43-39
8.0	17 49.61	63-80	.5	45 39.07	6-61	53.0	30 11.17	89-73	.5	3 10.29	43-12
.5	18 52.20	62-59	31.0	45 44.27	5-20	.5	29 30.93	40-24	76.0	3 53.12	42-83
9.0	19 54.04	61-84	.5	45 48.04	8-77	54.0	28 50.19	40-74	.5	4 35.67	42.55
.5	20 55.08	61-04	32.0	45 50.40	2-36	.5	28 8.99	41-20	77.0	5 17.91	42-24
	20 00.00	60-20	0.0.0	40 00/40	+ 0-98	<b>"</b>	20 0.33	41-63		011.51	41-98
10.0	+21 55.28		.5	+45 51.38	1 0-20	55.0	+27 27.36	47.00	.5	- 5 59.84	11.00
.5	22 54.61	+59-33	33.0	45 50.97	- 0-41	.5	26 45.30	-42-06	78.0	6 41.45	-41-61
11.0	23 53.03	58-42	.5	45 49.19	1.78	56.0	26 2.84	42-46	.5	7 22.73	41-28
.5	24 50.51	57-48	34.0	45 46.05	8-14	.5	25 20.01	42-88	79.0	8 3.66	40-98
12.0	25 47.02	56-51	.5	45 41.57	4-48	57.0	24 36-82	43-19	.5	8 44.24	40-56
.5	26 42.51	<b>55-4</b> 9	35.0	45 35.76	5-81	.5	23 53-31	48-51	80.0	9 24.46	40-22
13.0	27 36-96	54-45	-5	45 28.65	7-11	58.0	23 9.48	43-68	.5	10 4.31	39-85
.5	28 30.33	58-37	36.0	45 20.23	8-42	.5	22 25.37	44-11	81.0	10 43.79	<b>39-4</b> 8
14.0	29 22.60	52-27	.5	45 10.53	9-70	59.0	21 40.99	44-38	.5	11 22.88	39-09
.5	30 13.73	51-18	37.0	44 59.58	10-95	.5	20 56-37	44-62	82.0	12 1.57	89-69
		49-97			12-19			44-85			38-30
15.0	+31 3.70		.5	+44 47-39	1	<b>60.</b> 0	+20 11.52	Ī	.5	-12 39.87	1 1
.5	31 52.48	+48-78	39.0	44 33.97	-18-42	-5	19 26.47	-45-05	83.0	13 17.76	-37-89
16.0	32 40.04	47-56	.5	44 19.35	14-62	61.0	18 41.24	45-28	.5	13 55.23	87-47
.5	33 26.36	46-89	39.0	44 3.55	15-80	-5	17 55.84	45-40	84.0	14 32.29	87-06
17.0	34 11.42	45-06	.5	43 46.58	16-97	62.0	17 10.30	46-54	.5	15 8.92	36-63
.5	34 55.19	48-77	40.0	43 28.48	18-10	.5	16 24.63	45-67	85.0	15 45.11	36-19
18.0	35 37.66	49-47	-5	43 9.25	19-28	63.0	15 38.86	45-77	.5	16 20.86	35-75
.5	36 18.80	41-14	41.0	42 48 93	20-82	.5	14 53.01	45-85	86.0	16 56.17	25-21
19.0	36 58.60	89-80	.5	42 27.52	21-41	64.0	14 7.08	45-98	.5	17 31.03	34-86
.5	37 37.03	38-48	42.0	42 5.07	22-45	-5	13 21.11	45-97	87.0	18 5.43	84-40
		87-05	1		23-49			46-01		1	23-94
20.0	+38 14.08	+35-67	.5	+41 41.58	-24-50	65.0	+12 35.10	-46-08	-5	-18 39.37	-33-48
.5	38 49.75	34-26	43.0	41 17.08		.5	11 49.07		88.0	19 12.85	88-00
21.0	39 24.01	82-84	.5	40 51.60	25-48 26-45	66.0	11 3.05	46-02 46-00	.5	19 45.85	32-53
.5	39 56.85	81-42	44.0	40 25.15		.5	10 17-05	45-97	89.0	20 18.38	82-04
22.0	40 29.27	+29-99	-5	39 57.76	27-39 -28-31	67.0	9 31.08	-45-91	.5	20 50.42	-31-56
.5	+40 58.26	23-88	45.0	+39 29.45	20.91	.5	+ 8 45.17	40.91	90.0	-21 21.98	91.00

TABLE II.—Concluded.

## FOR THE CORRECTION c TO BE ADDED TO THE AUXILIARY ANOMALY v'.

Argument = M. For  $M > 180^{\circ}$  the Argument is  $360^{\circ} - M$ , and the sign of c to be reversed.

Arg.	c	Diff.	Arg.	c	Diff.	Arg.	с	Diff.	Arg.	c	Diff
000	01 01 02	н	1105	-36 9.15	"	125 0	24 10 07		1505	-20 16.21	"
90.0	-21 21.98 21 53.05	-81-07	112.5 113.0	-36 9.15 36 16.91	- 7.76	135.0 .5	-34 18.97 34 6.94	+12-03	157.5 158.0	19 51.85	+24-36
.5 91.0	22 23.63	80-58	.5	36 24.18	7.27	136.0	33 54.55	12-89		19 27.32	24-58
.5	22 53.72	80-09	114.0	36 30.94	6-76	.5	33 41.80	12-75	.5 159.0	19 2.61	94-71
92.0	23 23.31	29.59	.5	36 37.20	6-26	137.0	33 28.70	13-10	-5	18 37.73	24.88
.5	23 52.40	29-09	115.0	36 42.97	5-77	.5	33 15.25	18-45	160.0	18 12.68	25-05
93.0	24 20.98	28•58	.5	36 48.25	5-28	138.0	33 1.46	13.79	.5	17 47.47	26-21
.5	24 49.05	28.07	116.0	36 53.03	4-78	-5	32 47.32	14-14	161.0	17 22.10	25-87
94.0	25 16.62	27-57	.5	36 57.33	4-30	139.0	32 32.85	14-47	.5	16 56-58	25-52
.5	25 43.67	27-05	117.0	37 1.14	8-81	-5	32 18.04	14-81	162.0	16 30-90	25.68
		26-54			8-82			15-14			25-82
95.0	-26 10.21	-26-03	.5	-37 4.46	- 2.85	140.0	-32 2.90	+15-46	.5	-16 5.08	+25.97
.5	26 36.24	25.51	118.0	37 7.31	2-36	.5	31 47.44	15-79	163.0	15 39.11	26-11
96.0	27 1.75	24.99	.5	37 9.67	1.89	141.0	31 31.65	16-10	.5	15 13.00	26-24
.5	27 26.74	24-46	119.0	37 11.55	1.42	.5	31 15.55	16-42	164.0	14 46.76	26-38
97.0	27 51.20	23.91	.5	37 12.97	0.94	142.0	30 59.13	16-72	-5	14 20.38	26-50
.5	28 15.14	23-42	120.0	<b>37 13.</b> 91	0-47	.5	30 42.41	17-04	165.0	13 53.88	26-68
98.0	28 38.56	22-89	.5	37 14.38	- 0.01	143.0	30 25.37	17-88	-5	13 27.25	26-74
.5	29 1.45	22-37	121.0	37 14.39	+ 0.46	.5	30 8.04	17-63	166.0	13 0.51	26-86
99.0	29 23.82	21-84	.5 100 0	37 13.93	0-92	144.0	29 50.41	17-98	.5	12 33.65	26-97
.5	20 45.66	01 93	122.0	37 13.01	,	.5	29 32.48	18-22	167.0	12 6.68	~~~
100.0	30 6.98	21-82	.5	-37 11.64	1-37	145.0	-29 14.26	16-22	.5	-11 39.61	27-07
.5	30 27.77	20-79	123.0	37 9.81	+ 1-83	.5	28 55.75	+18-51	168.0	11 12.43	+27-18
101.0	30 48.03	20.26	.5	37 7.53	2-28	146.0	28 36.96	18-79	.5	10 45.15	27-28
.5	31 7.76	19-73	124.0	37 4.81	2-72	.5	28 17.89	19-07	169.0	10 17.78	27-87
102.0	31 26.97	19-21	.5	37 1.64	8-17	147.0	27 58.54	19-85	.5	9 50.32	27-46
.5	31 45.64	18-67	125.0	36 58.04	8-60	.5	27 38.93	19-61	170.0	9 22.77	27-55
103.0	<b>32 3.7</b> 9	18-15	.5	36 54.00	4-04	148.0	27 19.05	19-88	.5	8 55.14	27-68
.5	32 21.41	17-62	126.0	36 49.53	4-47	.5	<b>26</b> 58.91	20.14	171.0	8 27.43	27.71
104.0	<b>32 38.5</b> 0	17-09	-5	36 44.63	4-90	149.0	26 38.51	20-40 20-65	.5	7 59.64	27.79
.5	32 55.06	16-56	127.0	36 39.31	5-82	.5	26 17.86	20.00	172.0	7 31.79	27-85
	00 11 10	16-04	_		5-74		~ ~ ~ ~ ~ ~	20-90	l .		27-92
105.0	-33 11.10	-15-51	.5	-36 33.57	+ 6-16	150.0	-25 56.96	+21-15	.5	- 7 3.87	+27-96
.5	33 26.61	14-98	128.0	36 27.41	6-58	.5	25 35.81	21-40	173.0	6 35.89	28-04
106.0	33 41.59	14-46	.5	36 20.83	6-99	151.0	25 14.41	21-68	174.0	6 7.85	28-09
.5 107.0	33 56.05 34 9.99	13-94	129.0	36 13.84 36 6.44	7-40	.5 152.0	24 52.78 24 30.92	21-96	174.0	5 39.76	28-14
.5	34 9.99 34 23.40	13-41	.5 130.0	35 58.63	7-81	152.0	24 30.92 24 8.83	22-09	.5 175.0	5 11.62 4 43.44	28-18
108.0	34 36.30	12-90	130.0	35 50.41	8-22 <sup>-</sup>	153.0	23 46.51	22-82	.5	4 43.44	28-23
.5	34 48.68	12-38	131.0	35 41.80	8-61	.5	23 23.98	92-53	176.0	3 46.94	28-27
109.0	35 0.54	11-86	.5	35 32.79	9-01	154.0	23 1.23	22-75	.5	3 18.65	28-29
.5	35 11.88	11-84	132.0	35 23.39	9-40	.5	22 38.27	22-96	177.0	2 50.32	28-33
	12.30	10-88	1	33 33.00	9-79	~		28-17		2 302	29-35
110.0	-35 22.71		.5	-35 13.60		155.0	-22 15.10		-5	- 2 21.97	1 1
-5	35 33.02	-10-81	133.0	35 3.43	+10-17	.5	21 51.72	+23-38	178.0	1 53.60	+26-87
111.0	35 42.82	9.80	.5	34 52.87	10-56	156.0	21 28.14	28-58	.5	1 25.21	28-39
.5	35 52.10	9-28 8-78	134.0	34 41.94	10-93	.5	21 4.36	23.78	179.0	0 56.81	28-40 28-40
112.0	36 0.88	- 8-27	-5	34 30.64	+11-67	157.0	20 40.38	+24-17	.5	- 0 28.41	+28-41
.5	-36 9.15	3.21	135.0	-34 18.97	11.01	.5	-20 16.21	1.24-17	180.0	0 0.00	1 20041

TABLE III. FOR THE ARGUMENTS.

The For the different Found. The states we to the meridian of Visioning out.									
Years.	I.	II.	III.	IV.	<b>v</b> .	VI.	VII.	VIII.	IX.
1852 B	150.924	24.214	326.061	175.14	199.35	281.72	<b>257.5</b> 0	68.56	277.63
1853	120.598	97.317	338.513	217.92	315.23	171.35	74.04	264.48	143.88
1854	90.273	170.420	350.966	260.69	71.11	60.99	250.57	100.40	10.12
1855	50.273 59.947	243.524	3.418	303.47	187.00	310.63	67.10	296.32	236.37
1856 B	29.539	316.828	15.905	346.37	303.19	200.94	244.12	131.79	102.25
1857	359.213	29.931	28.357	29.14	59.07	90.58	60.65	327.71	328.50
	328.888	103.035	40.810	71.92	174.96	340.22	237.18	163,63	194.74
1858 1859	298.562	176.138	53.263	114.70	290.84	229.85	53.71	359,55	67.99
1860 B	268.154	249.442	65.749	157.59	47.04	120.17	230.73	195,02	286.87
1861	237.828	322.545	78.202	200.37	162.92	9.81	47.26	30.94	153.11
-	207.503	35.648	90.654	243.15	278.80	259.44	223.79	226.86	19.36
1862		108.752	103.108	285.93	34.68	149.08	40.33	62.78	245.60
1863	177.178		115.594	328.82	150.88	39.40	217.34	258.25	111.48
1864 B	146.769	182.056		1	266.76	289.03	33.87	94.17	337.73
1865	116.444	255.159	128.047	11.60	22.64		210.41	290.09	203.97
1866	86.119	329.263 41.366	140.500 152.953	54.38 97.16	138.53	178.67 68.30	210.41 26.94	126.01	70.22
1867	55.793		•	1	254.72	318.62	203.95	321.48	296.10
1868 B	25.385	114.670	165.440	140.05	10.62	208.26	203.55	157.41	162.35
1869	355.060	197.774	177.893	182.83	1	97.90	197.02	353.33	28.59
1870	324.734	260.877	190.346	225.61	126.49 242.37		13.55	189.25	254.84
1871	294.409	333.981	202.799	268.39		347.53	190.57	24.72	120.72
1872 B	264.001	47.284	215.286	311.29	358.57	237.85		220.64	346.96
1873	233.676	120.388	227.740	354.06	114.45	127.49	7.10	56.56	213.21
1874	203.350	193.492	240.192	36.84	230.33	17.12	183.63	252.48	79.46
1875	173.025	266-595	252.646	79.62	346.22	266.76	0.17	87.95	305.34
1876 B	142.617	330.899	265.134	122.52	102.42 218.30	157.08	177.18 353.71	283.87	171.58
1877	112.292	53.003	277.586	165.29	334.18	46.72 296.35	170.25	119.80	37.84
1878	81.967	126.107	290.040	208.07	90.06	185.99	346.78	315.71	264.07
1879	51.642	199.210	302.494	250.85 293.74	206.26	76.30	163.80	151.19	129.95
1880 B	21.234	272.514	314.981	336.53	322.14	325.95	340.33	347.11	356.20
1881	350.908	345.618 58.721	327.434 339.887	19.30	78.02	215.58	156.86	183.03	222.44
1882	320.583	1	1	1	193.91	105.22	333.39	18.95	88.69
1883	290.258	131.825	352.340	62.08	310.11	355.54	150.41	214.42	314.57
1884 B	259.849	205.129	4.827	104.98	1	245.17	326.94	50.34	180.82
1885	229.524	278.232	17.280	147.76	65.99 181.87	134.81	320.94 143.47	246.26	47.06
1886	199.198	351.335 64.439	29.732 42.185	190.53 233.31	297.75	24.44	320.00	82.18	273.31
1887	168.873				53.95	274.76	137.02	277.65	139.19
1888 B	138.465	137.743	54.672 67.125	276.21 318.98	169.83	164.40	313.55	113.58	5.43
1889	108.139	210.846		1.76	285.71	54.03	130.09	309.49	231.68
1890	77.814	283.950	79.578	1.76 44.54	41.59	303.67	306.62	145.41	97.92
1891	47.489	357.053	92.031	1	l	193.99	123.63	340.88	323.80
1892 B	17.080	70.357	104.517	87.44	157.79	83.63	300.17	176.81	190.05
1893	346.755	143.460 216.564	116.970	130.23 172.99	273.68 29.56	333.26	116.70	12.73	56.30
1894	316.430	1	129.423	215.77	29.56 145.44	222.90	293.23	208.65	282.54
1895	286-104	289.667 2.971	141.876 154.363	215.77 258.67	261.64	113.22	293.23 110.25	44.12	148.42
1896 B	255.696 225.371	76.075	166-816	301.49	17.52	2.85	286.78	240.04	14.67
1897				301.49	133.30	2.55 252.49	103.31	75.96	240.91
1898	195.045	149.178 222.232	179.268 191.721	27.00	249.28	142.12	279.84	271.88	107.16
1899	164.720	295.585	204.208	69.90	5.48	32.44	96.86	107.35	333.04
1900 B	134.311	400.000	1 2011-200	1 03.30	1 0.40	0.6.22	1 20.00	1 2.77.00	1,00,007

### FOR THE ARGUMENTS.

		As For the different lears. The names are referred to the including of washington.							
Years.	<b>X</b> .	XI.	XII.	XIII.	XIV.	XV.	XVI.	XVII.	XVIII.
1852 B	116.98	233-29	130.80	223.57	44.34	<b>4.1</b>	219.5	305.9	28.3
1853	99.11	336.72	50.76	52.55	167.16	27.5	25.1	268.7	124.8
1854	81.24	80.15	330.72	241.53	289.98	50.9	190.7	231.4	221.3
1855	63.37	183.58	<b>250.6</b> 8	70.52	52.79	74.3	356.3	194.1	317.8
1856 B	45.44	287.29	171.41	260.02	174.96	96.7	161.3	157.8	55.5
1857	27.57	30.72	91.37	89.01	297.78	192.1	326.9	120.5	152.0
1858	9.70	134.15	11.33	277.99	60.59	145,5	132.5	83-3	248.5
1859	351.82	237.58	<b>291.2</b> 9	106.98	183.41	168.9	298.1	46.0	345.0
1860 B	<b>3</b> 33.90	341.29	212.02	296.48	305.58	193.3	103.2	9.6	82.7
1861	316.03	84.72	131.98	125.46	68.40	216.7	268.8	332.4	179.2
1862	298.16	188.15	51.94	314.45	191.21	240.1	74.4	295.1	275.7
1863	280.29	291.57	331.90	143.43	314.03	263.5	240.0	257.8	12.2
1864 B	262.36	35.29	252.63	332.93	76.20	287.9	45.0	221.5	110.0
1865	244.49	138.72	172.59	161.92	199,01	311.3	210.6	184.2	206.5
1866	226.62	242.14	92.55	350.91	<b>321.</b> 83	334.7	16.2	146.9	303.0
1867	208.75	345.57	12.51	179.89	84.65	358.1	181.8	109.7	39.5
1868 B	190.82	89.29	293,24	9.39	206.81	22.5 -	346.9	73.3	137.2
1869	172,95	192.71	213.20	198.38	329.63	45.9	152.5	36.0	233.7
1870	155.08	296.14	133.16	27.37	92.45	69.3	318.1	358.8	330.2
1871	137.21	39.57	53.12	216.35	215.27	92.7	123.7	321.5	66.7
1872 B	119.29	143.28	333.85	45.85	337.43	117.1	288.7	285.1	164.4
1873	101.42	246.71	253.81	234.84	100.25	140.5	94.3	247.9	260.9
1874	83.54	350.14	173.77	63.83	223.07	163.9	259.9	210.6	357.4
1875	65.67	93.57	93.74	252.81	345.89	187.3	65.5	173.4	93.9
1876 B	47.75	197.28	14.46	82.32	106.05	211.7	230.6	137.0	191.6
1877	29.88	300.71	294.42	271.30	230.67	235.1	36.2	99.7	268.1
1878	12.01	44.14	214.39	100.29	<b>3</b> 53 <b>.6</b> 9	258.5	201.8	<b>62.</b> 5	24.6
1879	354.13	147.57	134.35	289.27	116.50	281.9	7.4	25.2	121.1
1880 B	336.21	251.28	55.08	118.78	238.67	306.3	172.4	348.8	218.9
1881	318.34	354.71	335.04	307.76	1.49	329.7	338.0	311.6	315.4
1882	300.47	98.14	255.00	136.75	124.31	353.1	143.6	274.3	51.9
1883	<b>282.6</b> 0	201.57	174.96	325.73	247.12	16.5	309.2	237.0	148.4
1884 B	264.68	<b>305.2</b> 8	<b>95.6</b> 9	155.23	9.29	41.0	114.3	200.7	246.1
1885	<b>246.8</b> 0	48.71	15. <b>6</b> 5	344.22	132.11	64.4	<b>27</b> 9.9	163.4	342.6
1886	228.93	152.14	295.61	173.20	254.92	87.7	85.5	126.1	79.1
1887	211.06	255.57 🔻	215.57	2.19	17.74	111.1	251.1	88.9	175.6
1888 B	193.14	<b>3</b> 59 <b>.2</b> 8	136.30	191.69	139.91	135.6	56.1	52.5	273.3
1889	175.26	102.71	56.26	20.68	<b>262.7</b> 3	159-0	221.7	15.2	9.8
1890	157.39	206.14	336.22	209.66	25.54	182.4	27.3	338.0	106.3
1891	139.52	309.56	256.18	38.65	148.36	205.7	192.9	300.7	202.8
1892 B	121.60	53.28	176.91	228.15	270.53	230.2	358.0	264.3	300.5
1893	103.73	156.71	96.87	57.14	33.34	253.6	163.6	227.1	37.0
1894	85.85	260.13	16.83	246.12	156.16	277.0	329.2	189.8	133.5
1895	67.98	3.56	296.79	75.11	278.98	300-4	134.7	152.6	230.0
1896 B	50.06	107.28	217.52	264.61	41.15	324.8	299.8	116.2	327.8
1897	32.19	210.70	137.48	93.59	163-96	348.2	105.4	78.9	64.3
1898	14.31	314.13	57.44	262.56	296.78	11.6	271.0	41.7	160-8
1899	356.44	57.56	337.40	111.56	<b>49.6</b> 0	35.0	76.6	4.4	257.2
1900 B	338.52	161.27	<b>2</b> 58.13	301.07	171.76	59.4	241.7	328.0	355.0

# FOR THE ARGUMENTS.

		FOR the dilicions roads. The wince are received to the nactual or washington,							
Years.	XIX.	XX.	XXI.	XXII.	XXIII.	XXIV.	XXV.	XXVI.	ххии.
1852 B	316.3	179.2	346.2	<b>209.</b> 8	<b>267.</b> 9	14.5	322.0	<b>58.</b> 8	83.0
1853	54.3	245.4	.48.4	100.9	219.7	173.1	311.0	340.3	77.6
1854	152.4	311.6	110.5	352.1	171.5	<b>331.</b> 8	300.0	261.8	72.2
1855	250.4	17.7	172.7	243.2	123.3	<b>130.</b> 5	289,2	183.3	66.8
1856 B	348.6	85.1	234.0	134.1	<b>75.</b> 0	<b>28</b> 9.6	277.2	104.5	61.3
1857	86.6	151.2	296.2	25.2	<b>26.</b> 8	88,2	266.3	<b>26.</b> 0	55.9
1858	184.7	217.4	358.4	276.4	<b>33</b> 8.6	<b>246.</b> 9	255.3	307.5	50.5
1859	282.7	283.6	60.5	<b>167.</b> 5	290.4	45,5	244.4	228.9	45.1
1860 B	20.9	<b>35</b> 0.9	121.9	58.4	242.1	204.6	232,4	150.2	39.7
1861	118.9	57.1	184.1	<b>309.</b> 5	193.9	<b>3.</b> 3	<b>221.</b> 5	71.7	34.2
1862	217.0	123.2	246.2	200.7	145.7	162.0	<b>2</b> 10.6	353.2	28.8
1863	315.0	189.4	308.4	91.8	97.5	320.6	199.6	274.6	23.4
1864 B	53,2	256.7	<b>36</b> 9. <b>7</b>	342.7	49.1	` 119.7	187.7	195,9	18.0
1865	151.3	322.9	71.9	233.8	0.9	278.4	176.7	117.4	12.5
1866	249.3	29.1	134.1	125.0	312.7	77.0	1 <b>6</b> 5.8	38.9	7.1
1867	347,3	95.2	196.2	16.1	264.5	235.7	154.9	320.3	1.7
1868 B	85,5	162.6	257.6	267.0	216.2	34.8	142.9	241.6	356.3
1869	183,6	228.7	319.7	158.1	168.0	193.4	132.0	163.1	350.8
1870	281.6	294.9	21.9	49.3	119.8	<b>3</b> 52.1	121.0	84.5	345,4
1871	19.6	1.1	84.1	300.4	71.6	150.8	110.1	6.0	340.0
1872 B	117.9	<b>6</b> 8.4	145.4	191,3	23.3	309.9	98.2	287.3	334.6
1873	215,9	134.6	207.6	82.4	335.1	108.5	87.2	208.8	329,2
1874	313,9	200.8	<b>269.</b> 8	333,6	<b>286.</b> 9	267.2	76.3	130.2	323,7
1875	51.9	266.9	<b>331.</b> 9	224,7	238.7	65.8	65.3	51.7	318.3
1876 B	150.2	334.3	33.3	115.6	190.4	224.9	53.4	333.0	312.9
1877	248,2	40.4	95.5	6.8	142.2	23.6	42.5	254.5	307.5
1878	346.2	106.6	157.6	<b>257.</b> 9	94.0	182.3	31.5	175.9	302.0
1879	84.2	172.8	219.8	143.0	45.8	<b>34</b> 0.9	20.6	97.4	296.6
1880 B	182.5	240.1	<b>2</b> 81.1	39.9	<b>3</b> 57.5	140.0	8.6	18.7	291.2
1881	280.5	306.3	<b>34</b> 3.3	291.1	309.3	298.7	<b>3</b> 57.7	300.2	285.8
1882	18.5	12.4	<b>4</b> 5.5	182.2	261.1	97.3	<b>346.</b> 8	221.6	280.4
1883	116.5	78.6	107.6	73.4	212.9	<b>256.</b> 0	<b>335.</b> 8	143.1	274.9
1884 B	214.8	145.9	169.0	324.2	164.5	55.1	. 323.9	64.4	269.5
1885	312.8	212.1	<b>2</b> 31.2	215.4	116.3	213.7	<b>312.</b> 9	345.9	264.1
1886	<b>50.</b> 8	278.3	293.3	106.5	68.1	12.4	302.0	267.3	258.7
1887	148.8	344.4	<b>355.</b> 5	357.7	19.9	171.1	<b>291.</b> 0	188.8	253.2
1888 B	247.1	51.8	<b>56.</b> 8	<b>24</b> 8.5	<b>331.</b> 6	330.2	<b>27</b> 9.1	110.1	247.8
1889	345.1	118.0	119.0	139.7	283.4	128.8	<b>26</b> 8.2	31.5	242.4
1890	83.1	184.1	181.2	<b>30.</b> 8	<b>235.2</b>	<b>287.</b> 5	<b>2</b> 5 <b>7.</b> 2	313.0	237.0
1891	181.1	<b>2</b> 50.3	243.3	282.0	187.0	86.1	<b>24</b> 6.3	<b>234.</b> 5	231.5
1892 B	<b>27</b> 9.4	317.6	304.7	172.8	138.7	245.2	<b>234.</b> 3	155.8	226.1
1893	17.4	<b>23.</b> 8	6.9	64.0	90.5	43.9	223.4	77.2	220.7
1894	115.4	90.0	69.0	315.1	42.3	202.6	212.5	358.7	215.3
1895	213.4	156.1	131.2	206.3	<b>354</b> .1	1.2	201.5	280.2	209.9
1896 B	311.7	223.5	192.5	97.1	<b>305.</b> 8	<b>16</b> 0.3	189.6	201.4	204.4
1897	49.7	289.6	254.7	348.3	257.6	319.0	178.6	<b>122.</b> 9	199.0
1898	147.7	<b>35</b> 5.8	<b>316.</b> 9	239.4	209.4	117.6	167.7	44.4	193.6
1899	245.7	62.0	19.0	<b>13</b> 0.6	161.2	276.3	<b>156.</b> 8	325.9	188.2
1900 B	344.0	129.3	80.4	21.5	112.8	75.4	144.8	247.1	182.7

## FOR THE ARGUMENTS.

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Years.	XXVIII.	XXIX.	XXX.	XXXI.	XXXII.	XXXIII.	XXXIV.	XXXV.	XXXVI.
1852 B	141.2	171.1	237.4	330.1	107.3	<b>297.</b> 8	134.9	272.0	110.7
1853	196.4	190.4	4.2	6.0	174.9	213.7	78.2	247.2	340.9
1854	251.7	209.7	131.0	41.8	242.6	129.7	21.6	222.4	211.2
1855	306.9	229.2	257.8	77.7	310.3	45.6	324.9	197.6	81.4
1856 B	2.3	247.7	26.0	114.6	18.2	320.4	270.1	173.7	313.3
1857	57.5	267.1	152.8	150.4	85.9	236.3	213.5	148.9	183.5
1858	112.7	286.4	279.6	186,3	153.5	152.3	156.8	124.1	53.8
1859	168.0	305.8	46.4	222.1	221.2	68.3	100.2	99.3	284.0
1860 B	223.4	324.3	174.6	259.1	289.1	343.0	45,3	75.4	155.9
1861	278.6	343.7	301.4	294.9	356.8	259.0	348.7	50.6	26.1
1862	333.8	3,1	68.2	330.7	64.5	174.9	292.0	25.7	256.4
1863	29.0	22,5	195.0	6.6	132.1	90.9	235.4	0.9	126.6
1864 B	84.4	40.9	323.2	43.5	200.0	5.6	180.5	337.0	358.5
1865	139.6	60.3	90.0	79.4	267.7	281.6	123.9	312.2	228.7
1866	194.9	79.7	216.8	115.2	335,4	197.5	67.2	287.4	99.0
1867	250.1	99.1	343.7	151.0	43.1	113.5	10.6	262.6	329.2
1868 B	305.5	117.5	111.8	188.0	110.9	28.2	315.8	238.7	201.1
1869	0.7	136.9	238,6	223.8	178.6	304.2	259.1	213.9	71.3
1870	56.0	156.3	5.4	259.7	246.3	220.2	202.5	189.1	301.6
1871	111.2	175.7	132,3	295.5	314.0	136.1	145.8	164.3	171.8
1872 B	166.6	194.1	260.4	332.4	21.9	50.9	91.0	140.4	43.7
1873	221.8	213.5	27,2	8.3	89.5	<b>326.</b> 8	34.3	115.6	274.0
1874	277.0	232.9	154,1	44.1	157.2	242.8	337.7	90.8	144.2
1875	332,3	252.3	280,9	80.0	224,9	158.7	281.0	66.0	14.4
1876 B	27.6	270.8	49.0	116.9	292.8	73.5	226.2	42.1	246.3
1877	82.9	290.2	175.8	152.7	0.5	349.4	169.6	17.3	116.6
1878	138.1	309.5	302.7	188.6	68.2	265.4	112.9	352.5	346.8
1879	193,3	328.9	69.5	224.4	135.8	181.4	56.3	327.7	217.1
1880 B	248.7	347.4	197.6	261.3	203.7	. 96.1	1.4	303.8	88.9
1881	304.0	6.8	324.5	297.2	271.4	12.1	304.8	279.0	319.2
1882	359.2	26.2	91.3	333.0	339.1	288.0	248.1	254.2	189.4
1883	54.4	45.5	218.1	8.9	46.8	204.0	191.5	229.4	59.7
1884 B	109.8	64.0	346.2	<b>45.</b> 8	114.6	118.7	136.7	205.5	291.5
1885	165.0	83.4	113.1	81.6	182.3	34.7	80.0	180.7	161.8
1886	220.3	102.8	239.9	117.5	250.0	310.7	23.4	155.9	32.0
1887	275.5	122.2	366.7	153.3	317.7	226.6	326.7	131.1	262.3
1888 B	330.9	140.6	134.9	190.2	25.6	141.4	271.9	107.2	134.1
1889	26.1	160.0	261.7	226.1	93.2	57.3	215.2	82.4	4.6
1890	81.3	179.4	28.5	261.9	160.9	333.3	158.6	57.6	234.6
1891	136.6	198.8	155.3	297.8	228.6	249.2	101.9	<b>32.</b> 8	104.9
1892 B	192.0	217.3	283.5	334.7	296.5	164.0	47.1	8.9	336.7
1893	247.2	236.6	50.3	10.6	4.2	79.9	350.4	344.1	207.0
1894	302.4	256.0	177.1	46.4	71.8	355.9	293.8	319.2	77.2
1895	357.6	275.4	303.9	82.2	139.5	271.9	237.1	294.4	307.5
1896 B	53.0	293.9	72.1	119.2	207.4	186.6	182.3	270.6	179.3
1897	108.3	313.3	198.9	155.0	275.1	102.6	125.6	245.7	49.6
1898	163.5	332.6	325.7	190.8	342.8	18.5	69.0	220.9	279.8
1899	218.7	352.0	92.5	226.7	50.4	294.5	12.4	196.1	150.1
1900 B	274.1	10.5	220.7	263.6	118.3	209.2	317.5	172.2	22.0
10002	77.3.1	40.0		~50.0	110.0	~~///~	00		74.0

TABLE III.—Continued.

### FOR THE ARGUMENTS.

A. FOR the different roads. The times are referred to the meridian of washington.									
Years.	XXXVII.	XXXVIII.	XXXIX.	XL.	XLI.	XLII.	XLIII.	XLIV.	XLV.
1852 B	<b>247.</b> 8	189.6	° 1	286°	161°	103°	10°	214	<b>63</b> °
1853	149.9	31.1	221	199	266	147	146	128	8
1854	52.0	232.5	82	112	11	192	281	43	313
1855	314.0	73.9	303	25	116	236	56	317	258
1856 B	216.8	275.9	164	300	220	279	191	233	203
1857	118.9	117.4	24	213	325	324	326	147	148
1858	21.0	318.8	245	126	70	8	101	62	93
1859	283.1	160.2	106	39	175	52	237	336	38
1860 B	185.9	2.2	327	313	279	96	371	252	344
1861	88.0	203.7	187	226	24	140	147	166	268
1862	350.1	45.1	48	140	129	184	262	81	233
1863	252.2	246.5	269	53	234	229	57	355	178
1864 B	155.0	88.5	129	327	339	272	192	271	124
			350	240	84	316	327	185	69
1865	57.1	290.0		153	188		102	100	14
1866	319.2 221.3	131.4 332.8	211		293	1 45		14	318
1867			72	67	38		238	1	1 1
1868 B	124.1	174.8	292	341		88	12	290	264 209
1869	26.2	16.3	153	254	143	133	148	204	
1870	288.2	217.7	14	167	248	177	283	119	154
1871	190.3	59.2	235	80	352	221	58	33	99
1872 B	93.1	261.1	95	355	97	265	193	308	44
1873	355.2	102.6	316	268	202	309	328	223	349
1874	257.3	304.0	177	181	307	353	103	138	294
1875	159.4	145.5	<b>3</b> 8	94	52	38	239	52	239
1876 B	62.2	347.4	<b>258</b>	9	156	81	13	327	185
1877	324.3	188.9	119	282	261	125	148	262	130
1878	226.4	30.3	340	195	6	170	284	156	74
1879	128.5	231.8	201	108	111	214	59	71	19
1880 B	31.3	73.8	61	23	215	257	194	346	325
1881	293.4	275.2	282	296	320	302	329	261	270
1882	195.5	116.6	143	209	65	346	104	175	215
1883	97.6	318.1	4	122	170	30	239	90	160
1884 B	0.4	160.1	224	37	274	74	14	5	105
1885	262.5	1.5	85	310	19	118	149	280	50
1886	164.5	202.9	306	223	124	162	285	194	355
1887	66.6	44.4	166	136	229	207	60	109	300
1888 B	329.4	306.4	27	50	333	<b>25</b> 0	195	23	246
1889	231.5	87.8	248	323	78	294	330	299	191
1890	133.6	289.2	109	236	183	339	105	213	135
1891	35.7	130.7	329	149	288	23	240	. 128	80
1892 B	298.5	332.7	190	64	32	66	15	43	26
1893	200.6	174.1	51	337	137	111	150	318	331
1894	102.7	15.5	272	250	242	155	286	232	276
1895	4.8	217.0	132	163	347	199	61	147	221
1896 B	267.6	59.0	353	78	91	243	195	62	166
1897	169.7	260.4	214	351	196	287	331	336	111
1898	71.8	101.8	74	, 264	301	331	106	<b>2</b> 51	56
1899	333.8	303.3	295	177	46	15	241	166	1
1900 B	236.7	145.3	156	92	150	59	16	81	307

## FOR THE ARGUMENTS.

<b>B.</b> V	ariations of t	he Argument	s for the diff	erent Months.	s. The times are referred to the meridian of Washington.						
Months.	L	II.	III.	IV.	٧.	VI.	VII.	VIII.	IX.		
January	0.000	0.000	0.000	0.00	0.00	0.00	0.00	0.00	0.00		
February	357.425	6.209	1.058	3.63	9.85	21.20	14.99	346.07	348.64		
March	355.098	11.817	2.014	6.91	18.74	40.35	28.53	333.48	338.38		
April	352.523	18.026	3.072	10.54	28.59	61.55	43.52	319.55	327.02		
May	350.031	24.035	4.096	14.06	38.12	82.07	58.03	306.07	316.03		
June	347.456	30.244	5.154	17.69	47.97	103.27	73.02	292.14	304.67		
July	344.964	36.253	6.178	21.21	57.50	123.79	87.53	278.66	293.68		
August	342.389	42.462	7.236	24.84	67.35	144.99	102.52	264.73	282.32		
September	339.814	48.671	8.294	28.47	77.19	166-19	117.51	250.80	270.96		
October	337.322	54.680	9.318	31.99	86.72	186.71	132.02	237.32	259.97		
November	334.747	60.889	10.376	35.62	96.57	207.91	147.01	223.39	248.61		
December	332.255	66.898	11.400	39.14	106.10	228.43	161.52	209.91	237.62		
,			·	<u></u>	···	<u> </u>		<u> </u>			
Months.	X.	XI.	XII.	XIII.	XIV.	xv.	XVI.	XVII.	xvIII.		
January	0.00	0.00	0.00	0.00	0.00	0.0	0.0	0.0	0.0		
February	358.48	8.78	<b>23.7</b> 8	16.05	339.85	32.6	343.5	27.4	38.8		
March	357.11	16.72	45.26	30.55	321.65	62.0	328.6	52.2	73.8		
April	355.59	25.50	69.04	46.60	301.50	94.6	312.1	79.6	112.6		
May	354.12	34.00	92.05	62.13	282.00	126.1	296.1	106.1	150.1		
June	352.60	<b>42.7</b> 8	115.83	78.18	261.85	158.7	279.6	133.5	188.9		
July	351.13	51.28	138.84	93.71	242.35	190.2	263.6	160.0	226.4		
August	349.61	60.06	162.62	109.76	222.20	222.8	247.1	187.4	265.2		
September	348.09	68.84	186.39	125.81	202.05	255.3	230.6	214.8	303.9		
October	346.62	77.34	209.40	141.34	182.55	286.8	214.6	241.3	341.4		
November	345.10	86.12	233.18	157.39	162.40	319.4	198.1	269.7	20.2		
December	343.63	94.62	<b>256.1</b> 9	172.92	142.90	350.9	182.1	295.3	57.7		
December	040.00	34.06	200.15	112.52	142.50	300.5	102.1	250.0	, 57.7		
Months.	XIX.	XX.	XXI.	XXII.	XXIII.	XXIV.	XXV.	XXVI.	XXVII.		
January	0.0	0.0	<b>0.</b> 0	0.0	0.0	0.0	0.0	0.0	0.0		
February	8.3	36.2	334.7	350.8	355.9	13.5	328.5	353.3	359.5		
March	15.8	68.9	311.9	342.4	352.2	25.6	300.1	347.3	359.1		
April	24.1	105.1	286.6	333.2	348.1	39.1	268.6	340.6	358.6		
May	32.2	140.1	262.1	324.2	344.1	52.2	238.1	334.2	358.2		
June	40.5	176.3	<b>236.</b> 8	315.0	340.0	65.6	206.6	327.5	357.7		
July	48.6	211.3	212.3	306.1	336.0	78.7	176.1	321.0	357.3		
August	56.9	247.5	187.0	296.8	331.9	92.1	144.6	314.3	356.8		
September	65.2	283.7	161.7	287.6	327.8	105.6	113.1	307.6	356.3		
October	73.3	318.7	137.2	278.6	323.8	118.6	82.6	301.2	355.9		
November	81.6	354.9	111.9	269.4	319.7	132.1	51.1	294.5	355.4		
December	89.7	29.9	87.4	260.5	315.7	145.2	20.6	288.0	355.0		
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In Bissextile Years subtract one day from the date in the first two months.

### FOR THE ARGUMENTS.

B. Variations of the Arguments for the different Months. The times are referred to the meridian of Washington.

Months.	XXVIII.	XXIX.	XXX.	XXXI.	XXXII.	XXXIII.	XXXIV.	xxxv.	XXXVI.
January	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
February	4.7	331.1	41.3	33.6	5.7	322.3	56.3	28.5	50.1
March	8.9	304.9	78.7	64.0	10.9	288.3	107.2	54.2	95.4
April	13.5	276.0	120.0	97.6	16.6	250.6	163.5	82.6	145.5
May	18.0	248.0	160.0	130.2	22.2	214.1	218.0	110.2	194.0
June	22.7	219.1	201.3	163.8	27.9	176.4	274.4	138.6	244.1
July	27.2	191.1	241.3	196.4	33.5	139.9	328.9	166.2	292.6
August	31.8	162.2	282.6	230.0	39.2	102.2	25.2	194.6	342.7
September	36.5	133.3	323.9	263.6	44.9	64.5	81.6	223.1	32.8
October	41.0	105.3	3.9	296.2	50.5	28.0	136.1	250.6	81.3
November	45.6	76-4	45.2	329.8	56.2	350.3	192.4	279.1	131.4
December	50.1	48.4	85.2	2.4	61.8	313.8	246.9	306.6	179.9

Months.	XXXVII.	xxxviii.	XXXIX.	XL.	XLI.	XLII.	XLIII.	XLIV.	XLV.
January	0.0	0.0	°	°	°	°	°	°	°
February	22.3	17.1	348	54	338	333	341	23	26
March	42.4	32.5	338	102	319	309	324	44	50
April	64.6	49.6	326	156	297	282	305	67	76
May	86.2	66.2	314	208	276	256	286	90	101
June	108.4	83.3	303	262	254	229	267	113	127
July	130.0	99.9	291	314	233	203	248	136	152
August	152.2	117.0	<b>27</b> 9	7	212	177	229	159	. 178
September	174.5	134.1	<b>26</b> 8	61	190	150	210	182	204
October	196.0	150.6	256	113	169	124	192	205	229
November	218.3	167.7	244	167	147	97	173	228	255
December	239.8	184.3	233	219	126	71	154	250	280

In Bissextile Years subtract one day from the date in the first two months.

# FOR THE ARGUMENTS.

### C. Variations of the Arguments for the different Days. The times are referred to the meridian of Washington.

Days.	I.	II.	ш.	IV.	v.	VI.	VII.	VIII	IX.
1	359.917	0.200	0.034	0.12	0.32	0.68	0.48	359.55	359.6
2	359.834	0.401	0.068	0.23	. 0.64	1.37	0.97	359.10	359.2
3	359.751	0.601	0.102	0.35	0.95	2.05	1.45	358.65	358.9
4	359.667	0.801	0.137	0.47	1.27	2.74	1.93	358.20	358.5
5	359.584	1.001	0.171	0.59	1.59	3.42	2.42	357.75	358.1
6	359.501	1.202	0.205	0.70	1.90	4.10	2.90	357.30	357.8
7	359.418	1.402	0.239	0.82	2.22	4.79	3.39	<b>356.</b> 85	357.4
8	359.335	1.602	0.273	0.94	2.54	5.47	3.87	356.40	357.0
9	359.252	1.803	0.307	1.06	2.86	6.16	4.35	<b>35</b> 5.95	356.7
10	359.169	2.003	0.341	1.17	3.18	6.84	4.84	355.51	356.3
20	358.338	4.006	0.683	2.34	6.35	13.68	9.67	<b>351.</b> 01	352.6
30	357.508	6.009	1.024	3.52	9.53	20.52	14.51	346-52	849.0

	1								
Days.	x.	XI.	XII.	XIII. '	XIV.	XV.	XVI.	XVII.	xvIII.
1	359.95	0.28	0.77	0.52	359.35	° 1.1	359.5	0.9	1.3
2	359.90	0.57	1.53	1.04	358.70	2.1	<b>3</b> 58.9	1.8	2.5
3	359.85	0.85	2.30	1.55	<b>3</b> 58.05	3.2	358.4	2.7	3.8
4	359.80	1.13	3.07	2.07	357.40	4.2	357.9	3.5	5.0
5	359.76	1.42	3.84	2.59	356.75	5.3	<b>3</b> 57.3	4.4	6.3
6	359.71	1.70	4.60	3.11	356.10	6.3	<b>356.</b> 8	5.3	7.5
7	359.66	1.98	5.37	3.62	<b>355.4</b> 5	7.4	356.3	6.2	8.8
8 .	359.61	2.27	6.14	4.14	354.80	8.4	<b>3</b> 55.7	7.1	10.0
9	359.56	2.55	6.90	4.66	354.15	9.5	355.2	8.0	11.3
10	359.51	2.83	7.67	5.18	<b>353.</b> 50	10.5	354.7	8.8	12.5
20	359.02	5.67	15.34	10.36	347.00	21.0	349.4	17.7	25.0
30	358.53	8.50	23.01	15.53	340.50	31.5	344.0	26.5	37.5

Days.	XIX.	XX.	XXI.	XXII.	XXIII.	XXIV.	xxv.	XXVI.	XXVII.
1	0.3	1.2	359.2	359.7	359.9	0.4	359.0	359.8	0.0
2	0.5	2.3	358.4	359.4	359.7	0.9	358.0	359.6	0.0
3	0.8	3.5	357.6	359.1	359.6	1.3	356.9	359.4	0.0
4	1.1	4.7	356.7	<b>358.</b> 8	359.5	1.7	355.9	359.1	359.9
5	1.3	5.8	355.9	358.5	359.3	2.2	354.9	<b>358.</b> 9	<b>3</b> 59.9
6	1.6	7.0	355.1	358.2	359.2	2.6	353.9	358.7	359.9
7	1.9	8.2	354.3	357.9	359.1	3.0	352.9	358.5	359.9
8	2.2	9.3	353.5	357.6	358.9	3.5	351.9	358.3	<b>3</b> 59.9
9	2.4	10.5	352.7	357.3	<b>358.</b> 8	3.9	350.9	358.1	<b>3</b> 59.9
10	2.7	11.7	351.8	357.0	358.7	4.4	349.8	357.9	<b>359.</b> 9
20	5.4	23.4	343.7	354.0	357.4	8.7	339.7	355.7	359.7
30	8.1	35.0	<b>3</b> 35.5	351.1	356.0	13.0	329.5	353.6	359.6

## FOR THE ARGUMENTS.

C. Variations of the Arguments for the different Days. The times are referred to the meridian of Washington.

Days.	XXVIII.	XXIX.	XXX.	XXXI.	XXXII.	XXXIII.	XXXIV.	xxxv.	xxxvi.
1	0.2	359.1	1.3	1.1	0.2	358.8	1.8	0.9	1.6
2	0.3	358.1	2.7	2.2	0.4	357.6	3.6	1.8	3.2
3	0.5	357.2	4.0	3.3	0.6	356.3	5.5	<b>2.</b> 8	4.9
4	0.6	356.3	5.3	4.3	0.7	355.1	7.3	3.7	6.5
5	0.8	355.3	6.7	5.4	0.9	353.9	9.1	4.6	8.1
6	0.9	354.4	8.0	6.5	1.1	352.7	10.9	5.5	9.7
7	1.1	353.5	9.3	7.6	1.3	351.5	12.7	6.4	11.3
8 .	1.2	352.5	10.7	8.7	1.5	350.3	14.5	· 7.3	12.9
9	1.4	351.6	12.0	9.8	1.7	349.0	16.4	8.3	14.6
• 10	1.5	350.7	13.3	10.9	1.9	347.8	18.2	9.2	16.2
20	3.0	341.3	26.7	21.7	3.7	335.7	36.3	18.4	32.3
30	4.5	332.0	40.0	32.6	5.6	323.5	54.5	27.5	48.5

Days.	XXXVII.	xxxviii.	XXXIX.	XL.	XLI.	XLII.	XLIII.	XLIV.	XLV.
1	0.7	0.6	°°	° °	359	359	359	ı° ı	°
2	1.4	1.1	<b>35</b> 9	3	359	358	359	2	2
3	2.2	1.7	<b>35</b> 9	5	358	357	358	2	3
4	2.9	2.2	359	7	357	357	358	3	3
5	3.6	2.8	<b>358</b>	9	357	356	357	4 .	4
6	4.3	3.3	358	10	356	355	356	5	5
7	5.0	3.9	357	12	355	354	356	5	6
8	5.7	4.4	357	14	354	353	355	6	7
9	6-5	5.0	357	16	354	352	354	7	8
10	7.2	5.5	356	17	353	351	354	8	8
20	14.4	11.0	352	35	346	343	348	15	17
30	21.5	16.6	<b>34</b> 9	52	339	334	342	23	25

# FOR THE ARGUMENTS.

<b>D.</b> \	Variations of the Arguments for the di	fferent Hours. The times are refe	erred to the meridian of Washington.
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Hours.	I.	n.	III.	ıv.	<b>v</b> .	VI.	VII.	VIII.	IX.
1	359.997	0.008	0.001	0.00	0.01	0.03	0.02	359.98	359.99
2	359.993	0.017	0.003	0.01	0.03	0.06	0.02	359.96	359.97
3	359.990	0.025	0.004	0.02	0.04	0.09	0.06	359.94	359.95
4	359.986	0.033	0.006	0.02	0.05	0.11	0.08	359.92	359.94
5	359.983	0.042	0.007	0.03	0.07	0.14	0.10	359.90	359.92
6	359.979	0.050	0.008	0.03	0.08	0.17	0.12	359.89	359.91
7	359.976	0.058	0.010	0.03	0.09	0.20	0.14	359.87	359.89
8	359.972	0.066	0.011	0.04	0.11	0.23	0.16	359.85	359.88
9	359.969	0.075	0.013	0.04	0.12	0.26	0.18	359.83	359.86
10	359.965	0.083	0.014	0.05	0.13	0.29	0.20	359.81	359.85
20	359.930	0.166	0.028	0.10	0.26	0-57	0.40	359.62	<b>3</b> 59. <b>7</b> 0
	1	1	.	ł		ľ			
								· · · · · · · · · · · · · · · · · · ·	

Hours.	X.	XI.	XII.	XIII.	XIV.	XV.	XVI.	XVII.	XVIII
1	0.00	0.01	0.03	0.02	359.97	0.0	0.0	0.0	0.1
2	0.00	0.02	0.06	0.04	359.95	0.1	0.0	0.1	0.1
3	359.99	0.04	0.10	0.07	359.92	0.1	359.9	0-1	0.9
4	359.99	0.05	0.13	0.09	359.89	0.2	<b>359.9</b>	0.2	0.9
5	359.99	0.06	0.16	0.11	359.87	0.2	359.9	0.2	0.
6	359.99	0.07	0.19	0.13	359.84	0.3	359.9	0.2	0.
7	359.99	0.08	0.22	0.15	359.81	0.3	359.9	0.3	0.
8	359.98	0.10	0.26	0.17	359.78	0.4	<b>359.8</b>	0.3	0.
9	359.98	0.11	0.29	0.20	359.76	0.4	359.8	0.3	0.
10	359.98	0.12	0.32	0.22	359.73	0.4	359.8	0.4	0.
20	359.96	0.24	0.64	0.24	359.46	0.9	359.6	0.7	1.

Hours.	XIX.	XX.	XXI.	XXII.	XXIII.	xxiv.	xxv.	XXVI.	xxvII.
1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2	0.0	0.1	359.9	0.0	0.0	0.0	359.9	0.0	0.0
3	0.0	0.2	359.9	0.0	0.0	0.1	359.9	0.0	0.0
. 4	0.0	0.2	359.9	0.0	0.0	0.1	<b>359.</b> 8	0.0	0.0
5	0.1	0.2	359.8	359.9	0.0	0.1	359.8	0.0	0.0
6	0.1	0.3	<b>359.8</b>	359.9	0.0	0.1	359.8	0.0	0.0
7	0.1	0.3	<b>359.8</b>	359.9	0.0	0.1	359.7	0.0	0.0
8	0.1	0.4	<b>359.7</b>	359.9	0.0	0.1	359.7	0.0	0.0
9	0.1	0.4	<b>359.7</b>	359.9	0.0	0.2	359.6	0.0	0.0
10	0.1	0.5	<b>359.7</b>	359.9	0.0	0.2	359.6	0.0	0.0
20	0.2	1.0	359.3	359.8	0.0	0.4	359.2	0.0	0.0

# TABLE III.—Concluded.

## FOR THE ARGUMENTS.

D. Variations of the Arguments for the different Hours. The times are referred to the meridian of Washington.

Hours.	XXVIII.	XXIX.	XXX.	XXXI.	XXXII.	XXXIII.	XXXIV.	xxxv.	XXXVI.
1	0.0	0.0	0.1	0.0	0.0	359.9	0.1	0.0	0.1
2	0.0	359.9	0.1	0.1	0.0	359.9	0.2	0.1	0.1
3	0.0	359.9	0.2	0.1	0.0	359.8	0.2	0.1	0.2
4	0.0	359.8	0.2	0.2	0.0	359.8	0.3	0.2	0.3
5	0.0	359.8	0.3	0.2	0.0	359.7	0.4	0.2	0.3
6	0.0	359.8	0.3	0.3	0.1	359.7	0.5	0.2	0.4
7	0.0	359.7	0.4	0.3	0.1	359.6	0.5	0.3	0.5
8	0.0	359.7	0.5	0.4	0.1	359.6	0.6	0.3	0.5
9	0.0	359.7	0.5	0.4	0.1	359.5	0.7	0.3	0.6
10	0.0	359.6	0.6	0.5	0.1	359.5	0.8	0.4	0.7
20	0.0	359.2	1.1	0.9	0.2	359.0	1.5	0.8	1.3
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Hours.	XXXVII.	XXXVIII.	XXXIX.	XL.	XLI.	XLII.	XLIII.	XLIV.	XLŸ.
1	0.0	0.0	°	°	°	°	°	°	°
2	0.1	0.1	0	0	0	0	0	o	Ö
3	0.1	0.1	0	0	0	0	0	0	0
4	0.1	0.1	0	0	0	0	0	0	0
5	0.2	0.1	0	0	0	0	0	0	0
6	0.2	0.1	0	0	0	0	0	0	0
7	0.2	0.2	0	0	0	0	0	0	0
8 -	0.2	0.2	0	· 1	0	0	0	0	0
9	0.3	0.2	0	1	0.	0	0	0	0
10	0.3	0.2	0	1	0	0	0	0	0
20	0.6	0.5	0	1	359	359	0	1	1
,	1				1	1	1	1	

TABLE IV.

PERTURBATIONS OF THE 'CO-ORDINATES IN UNITS OF THE SIXTH DECIMAL.

2 23.5   14-85   683.69   0-78   33.49   1-14   40   4401.91   3-98   330.15   10-92   27.29   1.28   33.45   3.45	l		<del></del>								<del></del>			
1 + 9.15   14-85   683.97   7-68   34.95   7-168   33.45   7-1	1 - 1	ં કૃ	Diff.	$\eta_1$	Diff.	ζ1	Diff.	Arg.	ξ1	Diff.	η1	Diff.	ζ1	Diff.
1 + 9.15   14-85   683.97   7-68   34.95   7-168   33.45   7-1	n	5 94		_684 99		25 71			±437 89		_960.75		<b>⊥94.60</b>	
2 23.51 14.56 683.09 0-78 33.45 1-14 47 443.73 2-99 340.15 10-29 279.72 2-16 33.74 3 3.783 14.59 683.02 1-66 690.23 1-66 690.24 1-66 1-73 1-74 690.24 1-75 64 456.22 1-66 690.24 1-75 1-74 690.24 1-75 1-74 690.24 1-75 1-74 690.24 1-75 1-74 690.24 1-74 1-74 1-74 1-74 1-74 1-74 1-74 1-7			+14-89		+ 0-85		+1.12			+8-09	_	+10.32		+1.81
3 37.83   14-32   681.88   1-51   32.99   1-16   49   446.27   2-44   329.91   10-17   29.867   1-86   1-66   31.11   1-16   49   446.56   2-99   319.63   10-17   29.84   1-29   1-20			14-86		0.78		1-14	0	l	2-82		10-28		1-29
4   52,00   14-36   630.23   1-66   31.11   1-18   49   448.66   2-36   319.74   10-11   31.10   1-16   668.02   1-16   675.60   2-96   29.91   1-20   50   450.58   2-00   309.63   10-00   32.34   1-20   30.63   1-20   30.63   10-00   32.34   1-20   30.63   10-00   32.34   1-20   30.63   10-00   32.34   1-20   30.63   10-00   32.34   1-20   30.63   10-00   32.34   1-20   30.63   10-00   32.34   1-20   30.63   10-00   32.34   1-20   30.63   10-00   32.34   1-20   30.63   10-00   32.34   1-20   30.63   10-00   30.63   10-00   30.63   10-00   30.63   10-00   30.63   10-00   30.63   10-00   30.63   10-00   30.63   10-00   30.63   10-00   30.63   10-00   30.65   10-00	1 1		14-32		1.21		1-16		ł	2-54		10-24		1.28
6         66,27         14-16         678,17         2-66         29,91         1-20         50         450,58         2-62         300,63         10-10         31,10         1-66         767,69         3-84         28,60         1-29         51         452,36         1-82         299,58         10-00         32,34         1-36         29,91         1-18         299,58         10-00         32,34         1-36         29,91         1-18         299,58         10-07         33,37         1-22         21,11         1-86         29,91         1-18         29,01         1-35         53         455,18         1-19         299,02         33,47         1-22         1-20         1-10         1-13,47         1-18         29,01         1-30         55         4456,22         1-60         260,017         1-84         4-64         22,33         1-10         56         457,64         4-66         20,013         1-84         4-64         22,33         1-10         57         455,04         4-60         20,013         3-64         4-71         3-84         3-84         458,19         4-61         4-60         3-83         465,11         3-60         4-84         3-84         41-11         4-61         4-61			14-26		1-65		1-18			2-29		10-17		1.27
10			14-18		2-06		1.20			2-02		10-11		1.26
7 94.35 18-96 672.60 9.89 27.45 1.94 52 453.89 1.92 229.80 9.89 33.57 1.22 29.80 1.91 131-11 131-16 665.82 8.89 24.92 1.27 54 456.22 1.06 269.00 9.89 33.57 1.22 114.88 4 18-87 657.27 4.06 22.363 1.32 56 457.64 1.06 269.01 114.85 47 18-87 657.27 4.06 22.363 1.32 56 457.64 1.06 269.01 114.85 47 18-87 657.27 4.06 22.363 1.32 56 457.64 1.06 269.01 114.85 1.12 162.03 18-19 652.42 4.88 21.01 1.32 57 458.02 1.01 1.02 1.02 1.02 1.02 1.02 1.02 1			14-10		2-48		1.22			1.78	8	10-05		1.24
8 108.20 13-80 660.51 3-29 26.19 1-37 54 456.22 1-06 260.72 35.99 36.99 34.92 1-37 54 456.22 1-06 260.72 35.99 1-39 35.99 1-39 35.99 1-39 1-39 1-39 1-39 1-39 1-39 1-39 1-					2-89		1.24		1	1.52		9.97		1.23
19			13-85		3-29		1-26		l	1-29		9-69		1.22
10			18-71		8-69		1.27			1-05		9-82	1	1.20
10	9	121.91		000.82		24.92		54	400.22		209.90		35.99	ا ا
11	10	1125.47	13-56	_661 73	4-09	_02 62	1.29	55	±457 04	0-82	_960 17	9-78	±37 17	1.18
12	1 1		+18-87		+ 4-46		+1-30			+0-60		+ 9-64		+1-17
13			18-19		4-85		1.32					9-55		1-16
14			12-98		5-23		1-33			+0-17		9-45		1-14
15	1 1		12-76		5-57		1-84			-0-08		9-35		1-18
16         212.60         13-39         629.42         6-37         15.63         1-88         61         457.53         0-41         203.79         9-14         43.97         1-06           18         236.45         11-80         615.94         -60         12.67         1-88         63         456.17         0-77         185.82         -8-8         45.05         1-08         456.17         0-77         185.82         -8-8         46.11         1-08         456.17         0-77         185.82         -8-8         46.11         1-04         -601.26         -601.26         -8-8         1-10.99         -601.26         -601.26         -7-8         1-10.09         +1-40         66         452.85         -1-17         159.72         +8-89         49.19         +1-10.09         448.12         -1-17         159.72         +8-89         49.19         +1-10.09         -601.26         445.14         66         4452.85         -1-17         159.72         +8-89         49.19         +1-10.09         -601.26         445.11         -10.09         +48.12         -1-17         159.72         +8-89         49.19         +1-10.09         -601.26         445.11         -10.09         +48.12         -1-18         66         445.14.2<	1 1		12-54		5-93		1-85			0.22		9-25		1-11
17	1 1	1	12-29		6-27		1.86			0-41		9-14		1.09
18			12-05		6-58		1-38	_		0-59		9-04		1-08
19 247.98 11-83 668.74 7-30 11.48 1-89 64 455.23 0-94 177.01 8-81 47.15 1-04 1-12 1-12 1-12 1-12 1-12 1-12 1-12 1-1	1 1		11-80		6-90		1.38		l .	0.77	B.	8-98	i e	1.06
20	1	1	11-58	_	7-20		1.89	-	l .	0-94	1	8-81		1-04
20	13	241.90	11.04	000.74	7.40	11.40	1.90	υ <u>ν</u>	400.60	1.11	177.01	9.70	47.10	1.09
21   270.19	20	+259,22	110-24	-601.26	l i	-10-09	1.08	65	+454.12	1.11	-168.31		+48.18	1.00
22   280.86   10-67   585.50   8-01   7.28   1-41   67   451.42   1-43   151.25   8-47   50.18   0-98   23   291.23   10-37   577.25   8-48   4.45   1-41   68   449.84   1-88   142.89   8-36   51.16   0-98   24   301.29   10-06   568.77   8-48   4.45   1-42   69   448.12   1-72   134.65   8-24   52.12   25   311.04   9-76   560.07   8-70   3.03   1-42   70   446.26   1-86   126.53   8-12   53.06   0-98   26   320.46   9-42   551.17   8-90   1.61   1-42   71   444.26   2-00   118.54   7-99   53.98   27   329.56   9-10   542.08   9-97   -0.19   1-42   72   442.13   2-13   110.66   7-88   54.89   28   338.32   8-76   532.81   9-27   +1.23   1-42   73   439.88   2-23   102.91   7-75   55.78   29   346.74   8-42   523.39   9-88   1-42   74   437.51   2-80   80.39   7-85   56.65   30   354.83   8-79   504.09   9-84   6.90   1-41   75   4435.02   2-80   80.39   7-27   59.15   31   +362.62   +7-79   504.09   9-84   6.90   1-41   76   432.42   2-80   65.98   7-14   59.94   32   370.07   7-45   494.25   9-95   8.31   1-41   78   426.92   2-80   65.98   7-14   59.94   33   377.21   7-14   484.30   9-95   8.31   1-41   78   426.92   2-80   65.98   7-12   59.94   34   334.01   6-80   474.25   10-31   11.11   1-40   80   421.02   3-00   52.07   6-89   61.48   36   396.63   6-16   453.91   10-24   13.81   10-31   12.51   1-40   81   417.93   3-89   45.29   6-78   62.23   37   402.45   8-82   443.65   10-36   13.89   13.89   390.47   3-84   4.66   6-84   67.51   466.92   40   +418.00   4-87   402.27   402.27   402.82   402.			+10-97		+ 7.75		+1.40			-1.27	1	+ 8-59	B .	+1-01
23			10-67		8-01		1-41			1-43		1		0.99
24         301.29         10-06         568.77         8-48         4.45         1-42         69         448.12         1-72         134.65         8-24         52.12         0-94           26         320.46         9-42         551.17         8-90         1.61         1-42         71         444.26         2-00         118.54         7-99         53.98         0-92           27         329.56         9-10         542.08         9-27         + 1.23         1-43         72         442.13         2-13         110.66         7-88         54.89         0-91           28         338.32         8-76         532.81         9-27         + 1.23         1-43         73         439.88         2-25         102.91         7-75         55.78         0-80           30         354.63         + 7.79         504.09         9-84         4.07         5.48         + 1-41         76         432.42         2-40         80.39         7-55.57.8         0-80           31         +362.62         7-45         494.25         9-84         6.90         1-42         77         443.02         2-70         73.12         7.77         55.56         56.33         1-68         59.51			10-87		8-25		1-41		i .	1.58		8-36		0-98
25         311.04         9-76         560.07         8-90         3.03         1-42         70         446.26         1.86         126.53         7-99         53.06         0-94           26         320.46         9-10         542.08         9-09         - 0.19         1-42         71         444.26         2-00         118.54         7-99         53.98         0-92           27         329.56         8-76         532.81         9-27         + 1.23         1-42         72         442.13         2-13         110.66         7-88         54.89         0-91           28         338.32         8-42         523.39         9-42         2.65         1-42         74         437.51         2-89         7-63         56.65         0-87           30         354.83         + 7-79         504.09         + 9-84         6.90         1-42         77         429.72         2-70         80.39         7-31         59.15         0-88           32         370.07         7-14         484.30         9-84         6.90         1-41         78         426.92         2-80         65.98         7-14         59.94         0-78           33         377.21         484.3		6	10-06		8-48		1-42				1	i		0-96
26         320.46         9-42         551.17         8-90         1.61         1-42         71         444.26         2-00         118.54         7-89         53.98         0-92           27         329.56         9-10         542.08         9-97         - 0.19         1-42         72         442.13         2-13         110.66         7-88         54.89         0-91           28         338.32         8-76         532.81         9-27         + 1.23         1-42         73         439.88         2-23         102.91         7-65         55.76         0-80           30         354.83         + 7-79         504.09         9-84         4.07         5.48         1-42         77         437.51         2-49         - 87.77         47.88         58.33         7.27         595.28         7-51         56.65         0-87           31         +362.62         + 7-79         504.09         + 9-72         5.48         1-42         77         429.72         2-70         73.12         7-27         59.15         0-89           32         370.07         7-14         484.30         9-84         6.90         1-42         77         429.72         2-70         73.12		ł	9.75		8-70		1.42		1	1.86		8-12		0-94
27         329.56         9-10         542.08         9-99         - 0.19         1-42         72         442.13         2-13         110.66         7-88         54.89         0-91           28         338.32         8-76         532.81         9-27         + 1.23         1-42         73         439.88         2-25         102.91         7-76         55.78         0-80           29         346.74         8-42         523.39         9-42         2-65         1-42         74         437.51         2-87         95.28         7-63         56.65         0-80           30         354.83         + 7.79         504.09         9-84         4.07         5.48         1-41         75         +435.02         -2-60         80.39         7-36         58.33         10-80         58.33         1-41         76         432.42         -2-60         80.39         7-73         59.15         0-89         58.33         10-95         58.31         1-41         76         442.02         2-80         65.98         7-14         59.94         59.96         6.90         1-41         77         429.72         2-70         73.12         7-27         59.15         0-89         58.33         10-39			9-42		8-90				1	1		1		0.92
28       338.32       8.76       532.81       9.27       + 1.23       1.42       73       439.88       2.25       102.91       7.76       55.76       0.88         29       346.74       8.42       523.39       9.42       2.65       1.42       74       437.51       2.87       95.28       7.63       56.65       0.67         30       354.83       + 7.79       504.09       + 9.72       5.48       + 1.41       76       432.42       -2.60       80.39       + 7.88       58.33       + 0.88         32       370.07       7.45       494.25       9.84       6.90       1.42       77       429.72       2.70       73.12       7.27       59.15       0.83         33       377.21       484.30       9.95       8.31       1.41       78       426.92       2.80       65.98       7.02       60.72       60.72         34       384.01       6.80       474.25       10.03       9.71       1.40       79       424.02       2.80       65.96       7.02       60.72       60.72         35       390.48       6.15       453.91       10.21       12.51       1.40       81       417.93       8.09			9-10	ľ	9-09		1.42			l .		1		0-91
29       346.74       8-42       523.39       9-42       2.65       1-42       74       437.51       2-87       95.28       7-63       56.65       0-67         30       354.83       + 7.79       504.09       + 9.72       5.48       1-42       75       + 435.02       - 2.60       80.39       + 7.81       + 57.50       0-88         32       370.07       7-45       494.25       9-84       6.90       1-42       77       429.72       2-70       73.12       7.97       59.15       59.71       142.02       2.90       58.96 <td< th=""><th>28</th><th></th><th>8-76</th><th></th><th>9-27</th><th></th><th>1.42</th><th>73</th><th>1</th><th>2.25</th><th></th><th></th><th></th><th>0-89</th></td<>	28		8-76		9-27		1.42	73	1	2.25				0-89
30         354.83         + 7.79         -513.81         + 9.72         5.48         + 1.41         75         + 435.02         -2.60         -87.77         + 7.51         + 57.50         + 6.83         + 6.93         -2.60         -2.60         -80.39         + 7.78         + 57.50         + 58.33         + 6.83         -2.60         -2.60         -80.39         + 7.21         59.15         -5.15         -8.31         -1.41         76         429.72         2.80         -6.90         73.12         7.14         59.91         -8.31         -1.41         78         426.92         2.80         65.98         7.14         59.91         -6.80         474.25         10.13         11.11         1.40         79         424.02         2.80         65.98         7.02         60.72         67.72         60.72         6.72         67.72         60.72         6.72         67.72         60.72         67.72         60.72         67.72         60.72         67.72         60.72         67.72         60.72         67.72         60.72         67.72         60.72         67.72         60.72         67.72         60.72         67.72         60.72         67.72         60.72         67.72         67.72         60.72         67.73	29		8-42		9-42		1-42	74		2.87		7-63		0.87
31         +362.62         +7.79         504.09         +9.72         5.48         +1.41         76         432.42         -2.60         80.39         +7.88         58.33         +0.88           32         370.07         7.45         494.25         9.84         6.90         1.41         78         426.92         2.80         65.98         7.14         59.94         0.79           33         377.21         7.14         484.30         9.95         8.31         1.41         78         426.92         2.80         65.98         7.14         59.94         0.79           34         384.01         6.80         474.25         10.05         9.71         1.40         79         424.02         2.80         65.98         7.02         60.72         0.73           35         390.48         6.47         464.12         10.13         11.11         1.40         80         421.02         3.00         52.07         6.89         61.48         0.76           36         396.63         6.16         453.91         10.21         12.51         1.40         81         417.93         3.99         45.29         6.78         62.23         0.75           38         407.9			8-09		9-58	. 2.00	1-42			2-49		7-51		0-85
31         +302.02         7.45         494.25         9.84         6.90         1.42         77         429.72         2.70         73.12         7.27         59.15         0.82           33         377.21         7.14         484.30         9.95         8.31         1.41         78         426.92         2.80         65.98         7.14         59.94         0.72           34         384.01         6.80         474.25         10.05         9.71         1.40         79         424.02         2.90         58.96         7.02         60.72         0.73           35         390.48         6.47         464.12         10.13         11.11         1.40         80         421.02         3.00         52.07         6.89         61.48         0.76           36         396.63         6.16         453.91         10.21         12.51         1.40         80         421.02         3.00         52.07         6.89         61.48         0.76           37         402.45         5.62         443.65         10.26         13.89         1.38         82         414.76         3.17         38.64         6.65         62.93         0.72           38         407.95 <th>30</th> <th>354.83</th> <th></th> <th>-513.81</th> <th></th> <th>+ 4.07</th> <th></th> <th>75</th> <th>+435.02</th> <th>١</th> <th>- 87.77</th> <th></th> <th>+57.50</th> <th>1 1</th>	30	354.83		-513.81		+ 4.07		75	+435.02	١	- 87.77		+57.50	1 1
32	31	+362.62		504.09	1 1	5.48	1	76	432.42		80.39		58.33	1
33 377.21 6.80 474.25 10.05 9.71 1.40 79 424.02 2.90 58.96 7.02 60.72 0.73 35 390.48 6.47 464.12 10.13 11.11 1.40 80 421.02 3.00 52.07 6.89 61.48 0.75 37 402.45 6.82 443.65 10.26 13.89 1.38 82 414.76 3.17 38.64 6.05 62.93 0.72 38 407.95 6.50 433.35 10.30 15.27 1.38 83 411.50 3.26 32.10 6.42 63.66 0.69 63.66 0.69 421.02 3.00 52.07 6.78 62.23 0.72 63.64 6.05 63.66 0.71 0.26 13.89 1.38 82 414.76 3.26 32.10 6.64 63.66 0.71 0.26 13.89 1.38 83 411.50 3.26 32.10 6.64 63.66 0.71 0.26 13.89 1.38 83 411.50 3.26 32.10 6.64 63.66 0.69 63.66 0.69 63.66 0.69 63.66 0.69 63.66 0.69 0.69 1.26 0.6	32	370.07	1	494.25	1	6.90		77	429.72		73.12	1	59.15	1
34 334.01 402.45 464.12 10-13 11.11 1-40 80 421.02 3.00 52.07 6-89 60.72 0.75 36 396.63 6-16 453.91 10-26 13.89 1.38 82 414.76 3.26 32.10 6.46 63.66 62.95 63.68 423.01 10-34 16.65 1.38 83 411.50 3.28 32.10 6.42 66.35 63.66	33	377.21		484.30	1 1	8.31	1	78	426.92	1	65.98	1	59.94	
36	34	384.01	1	474.25		9.71		79	424.02	1	58.96		60.72	1 4
36         396.0-3         402.45         5-82         443.65         10-26         13.89         1-38         82         414.76         3-17         38.64         6-65         62.23         0-72           38         407.95         5-50         433.35         10-30         15.27         1-38         83         411.50         3-26         32.10         6-64         63.66         0-71           39         413.13         5-18         423.01         10-34         16.65         1-38         84         408.17         3-38         25.68         6-42         63.66         64.35         0-69           40         +418.00         -4.87         -412.65         +18.01         +18.01         +1.36         86         401.29         -3-47         13.20         +6.18         65.67         6-63         65.67         66.30         6-63         66.30         66.30         66.30         66.30         66.30         66.30         66.30         66.30         66.30         66.30         66.30         66.30         66.30         66.30         66.30         66.30         66.30         66.92         66.30         66.30         66.30         66.92         66.30         66.92         66.30         66.92	35	390.48	1 1	464.12		11.11		80	421.02	1	52.07		61.48	1 I
37     402.45     5.82     443.65     10.26     13.89     1.38     82     414.76     3.17     38.64     6.65     62.95     0.72       38     407.95     5.50     433.35     10.30     15.27     1.38     83     411.50     3.26     32.10     6.64     63.66     63.66     63.66     64.35     64.35       39     413.13     5.18     423.01     10.34     16.65     1.88     84     408.17     3.41     5.66     64.25     64.35     64.35       40     +418.00     +4.57     402.27     +10.88     +18.01     +1.36     85     +404.76     -3.47     -19.38     +6.18     65.67       42     426.82     4.25     391.88     10.89     20.72     1.38     88     394.14     3.61     -1.18     5.96     66.92       43     430.78     3.96     381.49     10.89     20.72     1.38     88     394.14     3.61     -1.18     5.96     66.92       44     434.45     434.45     434.45     434.45     434.45     436.87     371.11     10.88     23.38     1.31     89     390.47     -2.72     4.66     5.84     67.51	36	396.63		453.91				81	417.93		45.29		62.23	
38	37	402.45		443.65	\$			82	414.76		38.64		62.95	1 1
39     413.13     5-18     423.01     10-34     16.65     1.38     84     408.17     3-33     25.68     6-42     64.35     0-69       40     +418.00     +4.57     -412.65     +10-88     +18.01     +1.36     85     +404.76     -3-47     -19.38     +6.18     65.67     +65.02       42     426.82     4.25     391.88     10-89     20.72     1-38     86     401.29     3-61     7.13     5-96     66.30     0-63       43     430.78     3-96     381.49     10-89     22.05     1-38     88     394.14     3-61     - 1.18     5-96     66.92     0-59       44     434.45     3-87     371.11     10-88     23.38     1-33     89     390.47     -2-72     4.66     4.66     4.57     67.51     4.57	38	407.95		433.35	1	15.27		83	411.50	1	32.10	1	63.66	1 1
40     +418.00     +4.57     -412.65     +10.88     +18.01     +1.36     85     +404.76     -3.47     -19.38     +6.18     +65.02     65.67       42     426.82     4.25     391.88     10.89     20.72     1.25     87     397.75     3.64     7.13     6-07     66.30     66.30       43     430.78     3.67     371.11     10.88     22.05     1.38     88     394.14     3.67     - 1.18     5.96     66.92       44     434.45     4.867     371.11     10.88     23.38     1.31     89     390.47     - 2.72     4.66     4.66     4.72     67.51	39	413.13	5-18	423.01	10.34		1.88	84	408.17	3-83		6-42		0-69
41 422.57 + 4.57 402.27 + 10.88 10.89 10.89 20.72 1.25 87 397.75 3.64 7.13 6.07 66.30 0.68 43 430.78 3.67 371.11 10.88 23.38 1.33 89 390.47 3.67 13.20 + 6.18 65.67 66.30 0.68 66.92 0.69 0.69 0.69 0.69 0.69 0.69 0.69 0.69		ĺ	4-87		10-36		1-36	ľ		3-41		6-30		0-67
41 422.57 4.25 391.88 10.89 20.72 1.85 86 401.29 3.65 66.30 0.68 43 430.78 3.67 371.11 10.88 23.38 1.81 29.39 390.47 5.73 3.67 3.67 371.11 10.88 23.38 1.81 89 390.47 5.73 5.73 6.67 67.51 5.87 5.73 67.51 5.73 6		1	+ 4.57		+10.80		+1.96		l	-9.47		+ 6-10	-	+0.65
42 420.52 3-96 381.49 10-38 22.05 1-33 88 394.14 3-61 - 1.18 5-95 66.92 66.92 66.92 44 434.45 + 3.87 371.11 + 10.86 23.38 + 1.31 89 390.47 - 2.73 + 4.66 + 5.73 67.51 + 0.86	11	I .			1 1			_	1	l		1		1
43 430.78 3.67 381.49 10.88 22.05 1.33 89 394.14 - 1.18 66.92 0.59 44 434.45 + 3.67 371.11 10.88 23.38 1.33 89 390.47 - 3.73 + 4.66 + 5.73 67.51 1.33 1.33 1.33 1.33 1.33 1.33 1.33 1					I					1				
$\begin{bmatrix} 44 & 434.45 \\ + 9.97 & 371.11 \\ + 10.96 & 23.38 \\ + 1.91 & 69 & 390.47 \\ - 9.79 & + 4.00 \\ + 5.79 & 07.51 \\ + 5.70 & 07.51 \\ + 5.70 & 07.5$	43			381.49	1						8	<u> </u>		
			+ 8.37		+10-86		+1.81	_		-8.72		+ 5.73		+0-56
45   +437.82   +3.51   -360.75   +10.56   +24.69   +1.51   90   +386.75   -3.12   + 10.39   +3.13   +68.09   +0.08	45	+437.82	. 3.31	-360.75	10.90	+24.69	. 1-01	90	+386.75	3-12	+ 10.39	. 3.13	+68.09	1 0.00

TABLE IV.—Continued.

# PERTURBATIONS OF THE CO-ORDINATES IN UNITS OF THE SIXTH DECIMAL.

				Ter	ms muitip	ned with	1 t. Aŋ	gument = .	04.			_	
Arg.	કૃ	Diff.	η <sub>1</sub>	Diff.	ζ1	Diff.	Arg.	ξ <sub>1</sub>	Diff.	$\eta_1$	Diff.	ζ <sub>1</sub>	Diff.
90°	+386.75		+ 10.39		+68.09		135	+192.61		+173.00		+76.34	
91	382.97	-8.78	16.00	+5-61	68.65	+0-56	136	188.14	-4-47	174.96	+1-96	76.16	-0-18
92	379.14	3-83	21.51	5-51	69.20	0-55	137	183.66	4-48	176.86	1-90	75.96	0-20
93	375.26	8-88	26.90	5-39	69.72	0-58	138	179.19	4-47	178.70	1-84	75.75	0-21
94	371.33	3-93	32.19	5-29	70.23	0-50	139	174.72	4-47	180.49	1-79	75.53	0-22
95	367.37	8-96	37.37	5-18	70.71	0-48	140	170.25	4-47	182.23	1.74	<b>75.2</b> 9	0-24
96	363.36	4-01	42.45	5-08	71.18	0-47	141	165.78	4-47	183.92	1-69	75.03	0-26
97	359.31	4-05	47.43	4-98	71.63	0-45	142	161.32	4-46	185.56	1-64	74.77	0-26
98	355.23	4-08	52.30	4-87	72.07	0-44	143	156.87	4-45	187.14	1-56	74.49	0-28
99	351.11	4-12	57.07	4-77	72.49	0-42	144	152.41	4-46	188.68	1-54	74.20	0-29
		4-15	0,,0,	4-67	12.30	0-40	744	106.41	4-45	100.00	1-49	14.20	0-31
100	+346.96		+ 61.74		+72.89	1	145	+147.96		+190.17		+73.69	
101	342.78	-4-18	66.32	+4-58	73.27	+0-38	146	143.52	-4-44	191.61	+1-44	73.57	-0.32
102	338.58	4-20	70.79	4-47	73.63	0-36	147	139.07	4-45	193.00	1-39	73.24	0-33
103	334.35	4-23	75.18	4-39	73.98	0-35	148	134.64	4-43	194.34	1-84	72.89	0.85
104	330.09	4-26	79.46	4.28	74.31	0.33	149	130.20	4-44	195.64	1-30	72.53	0-86
105	325.81	4-28	83.66	4-20	74.62	0-81	150	125.77	4-43	196.90	1-26	72.16	0.87
106	321.51	4-80	87.76	4-10	74.92	0.30	151	121.34	4-43	198.11	1.21	71.77	0-89
107	317.19	4.32	91.78	4-02	75.19	0.27	152	116.92	4-42	199.28	1-17	71.38	0-89
108	312.85	4-84	95.70	8-92	75.45	0-26	153	112.50	4-42	200.40	1-12	70.97	0.41
109	308.50	4-85	99.54	3-64	75.70	0-25	154	108.06	4.42	201.48	1-08	70.54	0.43
		4-87		3-76		0-22			4-41		1-04		0-48
110	+304.13		+103.30		+75.92		155	+103.67		+202.52		+70.11	
111	299.75	-4-38	106.97	+3-67	<b>76-1</b> 3	+0-21	156	99.26	-4-41	203.52	+1-00	69.66	-0-45
112	295.35	4-40	110.55	8-58	76.32	0-19	157	94.85	4-41	204.48	0-96	69.20	0-46
113	290.94	4-41	114.06	8.51	<b>76.5</b> 9	0-18	158	90.45	4-40	205.40	0-92	68.73	0.47
114	286.52	4-42	117.48	8-49	76.66	0-16	159	86.05	4-40	206.28	0-88	68.25	0-48
115	282.09	4-43	120.83	8-35	<b>76.</b> 80	0-14	160	81.65	4-40	207.12	0-84	67.75	0-50
116	277.66	4-48	124.10	8-27	76.93	0-18	161	77.25	4-40	207.92	0-80	67.24	0-51
117	273.21	4-45	127.29	3-19	77.04	0-11	162	72.86	4-39	208.68	0.76	66.72	0.52
118	<b>26</b> 9.76	4-45	130.41	3-12	77.13	0.09	163	68.47	4-89	209.40	0-72 0-69	66.19	0.68
119	264.30	4-46	133.45	8-04	77.21	0-08	164	64.08	4-89	210.09	0.09	65.65	0-54
		4-46		2-97		0-06			4-89		0-65		0-55
120	+259.84	-4-47	+136.42	+2.90	+77.27	+0-05	165	+ 59.69	-4-39	+210.74	+0-61	+65.10	-0.56
121	255.37	4-48	139.32	2-82	77.32	0-03	166	55.30	4-38	211.35	0-57	64.54	0.58
.122	250.89	4-47	142.14	2-76	77.35	+0.01	167	50.92	4-39	211.92	0-54	63.96	0-59
123	246.42	4-48	144.90	2-70	77.36	0.00	168	46.53	4-38	212.46	0-50	63.37	0.59
124	241.94	4.48	147.60	2-62	77.36	-0.03	169	42.15	4-38	212.96	0-46	62.78	0.61
125	237.46	4-49	150.22	2.56	77.34	0.03	170	37.77	4-39	213.42	0-48	62.17	0.62
126	232.97	4-48	152.78	2-49	77.31	0-05	171	33.38	4-38	213.85	0-39	61.55	0.63
127	228.49	4-49	155.27	2-48	77.26	0.06	172	29.00	4-88	214.24	C-35	60.92	0.63
128	224.00	4.49	157.70	2-87	77.20	0-08	173	24.62	4-89	214.59	0-82	60.29	0.65
129	219.51		160.07		77.12		174	20.23	<u>'</u>	214.91	1	59.64	
130	1015 00	4-48	+162.37	2-80	1 <del>77</del> 09	0-09	175	1 15 05	4-38	+215.20	0-29	+58.98	0-66
130	+215.03	-4-49	164.62	+2-25	+77.03 76.92	-0-11	175	+ 15.85 11.46	-4-89	215.44	+0-24	58.31	-0.67
131	210.54 206.06	4-48	164.62	2-18	76.92 76.80	9-12	176	7.08	4-88	215.44 215.65	0-21	57.63	0-68
133	201.58	4-48	168.92	2-12	76.66	0-14	177	+ 269	4-89	215.82	0-17	56.95	0-68
134	197.09	4-49	170.99	2-07	76.51	0-15	179	- 1.70	4-39	215.82	0.14	56.25	0-70
135	+192.61	-4-48	+173.00	+2+01	+76.34	-0-17	180	- 6.09	-4-39	+216.06	+0-10	+55.54	-0.71
130	T102.01	l	T14-3-(N)		T/U-34	<u> </u>	100	_ 0.09	<u> </u>	T&10-00	l	T00.04	<u> </u>

TABLE IV .- Continued.

## PERTURBATIONS OF THE CO-ORDINATES IN UNITS OF THE SIXTH DECIMAL.

I			<del></del>			<del></del>							
Arg.	ξ1	Diff.	$\eta_1$	Diff.	ζ,	Diff.	Arg.	ર્દા	Diff.	$\eta_1$	Diff.	ζ1	Diff.
180	- 6.09		+216.06		+55-54		225	-208.16		+178.25		+15.94	
181	10.48	-4-89	216.12	+0-06	54.82	-0.72	226	212.78	-4-63	176.30	-1.95	14.94	-1.00
182	14.88	4-40	216.15	+0-03	54.10	0-72	227		4-62		2.01		1.00
183	19.27	4-39	216.13	-0.02	53.36	0-74		217.40	4-69	174.29	2-06	13.94	1-01
184	23.67	4-40	216.13	0-04		0-74	228	222.02	4-62	172.23	2-12	12.93	1-01
, ,		4-40		0.09	52.62	0-76	229	226.64	4-68	170.11	2-19	11.92	1.01
185	28.07	4-41	216.00	0-12	51.86	0.76	230	231.27	4-63	167.92	2.24	10.91	1.01
186	32.48	4-40	215.88	0.16	51.10	0.77	231	235.90	4-68	165.68	2-81	9.90	1.02
187	36.88	4-41	215.72	0.20	50.33	0.78	232	240.53	4-68	163.37	2-38	8.88	1.02
188	41.29	4.42	215.52	0.23	49.55	0.78	233	245.16	4-68	160.99	2-46	7.86	1.02
189	45.71		215.29		48.77	1	234	249.79	]	158.55	i	6.64	1
190	50.10	4-49	.015.00	0-27		0-80	205	~	4-68	. 150.04	2.51		1.02
	- 50.13	-4-42	+215.02	-0.81	+47.97	-0.80	235	-254.42	-4-68	+156.04	-2-58	+ 5.82	-1.02
191	54.55	4.42	214.71	0-84	47.17	0.81	236	259.05	4-62	153.46	2.66	4.80	1 02
192	58.97	4-48	214.37	0.38	46.36	0-82	237	263.67	4-68	150.80	2.72	3.78	1.02
193	63.40	4-44	213.99	0-42	45.54	0.83	238	268.30	4-62	148.08	2-60	2.76	1-03
194	67.84	4-44	213.57	0-16	44.71	0 84	239	272.92	4-62	145.28	2-88	1.73	1.02
195	72.28	4-44	213.11	0-50	43.87	0.84	240	277.54	4-62	142.40	2.96	+ 0.71	1.02
196	76.72	4-45	212.61	0.54	43.03	0.85	241	282.16	4.61	139.44	8 04	- 0.31	1.03
197	81.17	4-46	212.07	0-58	42.18	0-86	242	286.77	4-60	136.40	8-12	1.34	1.02
198	85.63	4-46	211.49	0.62	41.32	0.86	243	291.37	4-59	133.28	3-20	2.36	1-03
199	90.09	4-10	210.87	0.02	40.46	0.00	244	295.96	4.09	130.08	3.20	<b>3.3</b> 9	1-00
		4-46		0-67		0-67			4-59		8-28		1-02
200	- 94.55	-4-47	+210.20	-0.70	+39.59	-0-88	245	-300.55	-4-58	+126.80	-3.36	- 4.41	-1 02
201	99.02	4-48	209.50	0-75	38.71	0-89	246	305.13	4-57	123.44	3.45	5.43	1.02
202	103.50	4-48	208.75	0.80	37.82	0-89	247	309.70	4-55	119.99	8-54	6.45	1-02
203	107.98	4-49	207.95	0.85	36.93	0-90	248	314.25	4-54	116.45	3 62	7.47	1.02
204	112.47	4.50	207.10	0-89	36.03	0.90	249	318.79	4-58	112.83	8.71	8.49	1 02
205	116.97	4-50	206.21	0-98	35.13	0.91	250	323.32	4.51	109.12		9.51	1-01
206	121.47	4.51	205.28	0.96	34.22	0.91	251	327.83	4-50	105.32	8 80 3-89	10.52	1.01
207	125.98	4.51	204.30		33.30	1	252	332.33		101.43	1	11.53	1.01
208	130.49	4-52	203.28	1.02 1.08	<b>32.3</b> 8	0.92	253	336.81	4.48	97.45	8.98	12.54	
209	135.01	4.02	202.20	1.08	31.45	0.98	254	341.27	4-46	93.38	4-07	13.55	1.01
		4-58		1.12		0-98			4-44		4-16		1-00
210	-139.54	-4.53	+201.08	-1.17	+30.52	-0-94	255	-345.71	-4-41	+ 89.22	-4-26	-14.55	-1-00
211	144.07	4-54	199.91	1.21	29.58	0-95	256	350.12	4-89	84.96	4-36	15.55	0-99
212	148.61	4-55	198.70	1.27	28.63	0.95	257	354.51	4.37	80.60	4-46	16.54	1.00
213	153.16	4-55	197.43	1.81	27.68	0.95	<b>25</b> 8	358.88	4-88	76.14	4-56	17.54	0-98
214	157.71	4-56	196.12	1.87	26.73	0.96	259	363.21	4.30	71.58	4-66	18.52	0.99
215	162.27	4-56	194.75	1.41	25.77	0.96	260	367.51	4.28	66.92	4.76	19.51	0.99
216	166.83	4-58	193.34	1.47	24.81	0.90	261	371.79		62.16		20.49	0.97
217	171.41	4.57	191.87	1.52	23.84	0.97	262	376.03	4.24	57.29	4-87	21.46	0.97
218	175.98	4-58	190.35	1.56	22.87	1 1	263	380.23	4-20	52.32	4-97	22.43	l 1
219	180.56		188.79	7.00	<b>21.8</b> 9	0.98	264	384.39	4-16	47.24	5-08	23.39	0-96
000	405	4-59		1-63		0.98			4-19		5-19		0-96
220	-185.15	-4-59	+187.16	-1.67	+20.91	-0-99	265	-388.51	-4+08	+ 42.05	-5-30	-24.35	-0.95
221	189.74	4-60	185.49	1.78	19.92	0.99	266	392.59	4.08	36.75	5.41	25.30	0-94
222	194.34	4.60	183.76	1.78	18.93	0.99	267	396.62	3-98	31.34	5.52	26.24	0.94
223	198.94	4-61	181.98	1.84	17.94	1.00	268	400.60	8-93	25.82	5-64	27.18	0.94
224	203.55	-4.61	180.14	-1.89	16.94	-1.00	269	404.53	-3.87	20.18	-5.75	28.11	-0.92
225	-208.16		+178.25	4-09	+15.94	1.00	270	-408.40	-9.91	+ 14.43	3.18	-29.03	0.92

TABLE IV .- Continued.

# PERTURBATIONS OF THE CO-ORDINATES IN UNITS OF THE SIXTH DECIMAL.

·													
Arg.	ξ1	Diff.	η1	Diff.	ζ1	Diff.	Arg.	ξı	Diff.	<b>7</b> 1	Diff.	ζι	Diff.
270°	-408.40		+ 14.43		-29.03		315	-457.24		-365.32		-56.92	
271	412.21	-3-81	8.56	- 5-87	29.95	-0.92		453.65	+ 3.59	375.78	-10-46		-0-17
272	415.97	8-76		5 <b>-9</b> 9	1	0.91	316		3-90		10-48	57.09	0-14
	3	3-68		6-11	30.86	0.90	317	449.75	4-18	386.26	10-49	57.23	0-12
273	419.65	8-62	- 3.54	6-28	31.76	0.89	318	445.57	4.50	396.75	10-47	57.35	0.09
274	423.27	8-55	9.77	6-84	32.65	0-88	319	441.07	4-81	407.22	10-45	57.44	0.06
275	426.82	8-47	16.11	6-47	33.53	0.87	320	436.26	5-11	417.67	10-42	57.50	0-04
276	430.29	8-30	22.58	6-60	34.40	0-86	321	431.15	5-44	428.09	10-89	57.54	-0.01
277	433.68	3.81	29.18	6-71	35.26	0.86	322	425.71	5-76	438.48	10-84	57.55	+0-02
278	<b>436.</b> 99	8.22	35.89	6-84	36.12	0.84	323	419.95	6-08	448.82	10-29	57.53	0-05
279	440.21	0.42	42.73	0.04	36.96	0.84	324	413.87	0.00	459.11	10.28	57.48	0.05
		3-18		6-96		0-83			6-41		10-28	l	0-06
280	-443.34	-3-04	<b>- 49.69</b>	- 7-09	-37.79	-0.82	325	-407.46	+ 6.74	-469.34	-10-14	-57.40	+0-11
281	446.38	2-94	<b>56.78</b>	7.21	38.61	0.80	326	400.72	7-06	479.48	10.05	57.29	0.14
282	449.32	2-83	63.99	7.34	39.41	1	327	393.66	7.40	489.53	9-95	57.15	0-17
283	452.15	2.72	71.33		40.21	0.80	<b>32</b> 8	386.26	i	499.48	9-82	56.98	) (
284	454.87		78.80	7-47	40.99	0.78	329	378.53	7.78	509.30	1	56.78	0-20
285	457.49	2-62	86.39	7-59	41.76	0.77	330	370.48	8-05	519.00	9-70	56.55	0.28
286	459.98	2-49	94.10	7-71	42.52	0.76	331	362.10	8-38	528.54	9-54	56.29	0.26
287	462.36	2.38	101.94	7-84	43.26	0.74	332	353.39	8-71	537.91	9-37	56.00	0-29
288	464.60	2.24	109.90	7-96	43.99	0-78	333	344.36	9.08	547.12	9-21	55.68	0-82
289	466.72	2.12	117.99	8-09	44.71	0.72	334	335.01	9-35	556.14	9-02	55.33	0-85
		1.98		8-21		0-70		000.02	9-67		8-61		0-38
290	-468.70		-126.20		-45.41		335	-325.34		-564.95	ł	-54.95	1 1
291	470.54	-1.84	134.53	- 8.33	46-10	-0.69	336	315.35	+ 9.99	5 <b>7</b> 3.56	- 8-61	54.54	+0-41
292	472.23	1.69	142.98	8-45	46.77	0-67	337	305.03	10-32	581.93	8 37	54.10	0-44
293	473.76	1-53	151.55	8-57	47.42	0-65	338	294.42	10-61	590.06	8-13	53.62	0-48
294	475.14	1.38	160.24	8-69	48.06	0.64	339	283.51	10-91	597.95	7.89	53.12	0-50
295	476.36	1.22	169.05	8-81	48.68	0.62	340	272.30	11-21	605.56	7-61	52.58	0-54
296	477.40	1-04	177.97	8-92	49.29	0-61	341	260.82	11-48	612.89	7-33	52.01	0.57
297	478.27	0-87	187.01	9-04	49.87	0-58	342	249.07	11-75	619.93	7-04	51.42	0-59
298	478.96	0-69	196.16	9-15	50.44	0-57	343	237.06	12-01	626.66	6.73	50.79	0-68
299	479.46	0-50	205.42	9-96	50.99	0-55	344	224.81	12-25	633.06	6-40	50.13	0-66
~~	413.40	0-82	200.42	9-36	00.00	0-58	717	&24.01	12-50	000.00	6-08	00.13	0-69
300	-479.78	0.02	-214.78	5-30	-51.52	0.00	345	-212.31	12.00	-639.14	. 0.00	-49.44	0.05
301	479.90	-0.13	224.25	- 9.47	52.03	-0-51	346	199.59	+12-72	644.88	- 5.74	48.72	+0.72
302	479.81	+0.09	233.82	9-57	52.52	0-49	347	186.65	12-94	650.26	5-36	47.97	0.75
303	479.52	0-29	243.48	9-66	52.99	0-47	348	173.50	13-15	655.28	5-02	47.19	0.78
304	479.00	0-52	253.24	9-76	53.44	0-45	349	160.15	13-35	659.91	4-63	46.39	0-80
305	478.27	0-78	263.09	9-85	53.87	0-48	350	146.64	13-51	664.16	4.25	45.55	0-84
306	477.30	0.97	273.09	9-98	54.28	0-41	351	132.95	13-69	668.02	8-86	45.55	0.86
		1.20		10-00		0-39		1	13-84		8-46		0.90
307 308	476.10	1-45	283.02	10-08	54.67	0-36	352	119.11	18-95	671.48	8-05	43.79	0.92
	474.65	1-69	293.10	10-16	55.03	0-84	353	105.16	14-08	674.53	2-65	42.87	0.94
309	472.96		303.26		55.37	1	354	91.08	1	677.18		41.93	
310	-471.01	1-95	_919 49	10-22	KE 60	0-82	355	75 01	14-17	670.40	2-24	-40.95	0-98
1 1	1	+2-22	-313.48	-10-27	-55.69	-0-80		- 76.91	+14-24	-679.42	- 1.82		+1.00
311	468.79	2-47	323.75	10-88	55.99	- 0-27	356	62.67	14-31	681.24	1.89	39.95	1-02
312	466.32	2.75	334.08	10-38	56.26	0.24	357	48.36	14-85	682.63	0.97	38.93	1-05
313	463.57	3-02	344.46	10-42	<b>56.</b> 50	0.22	358	34.01	14-38	683.60	0-52	37.88	1.07
314	460.55	+3-31	354.88	-10-44	56.72	-0.20	359	19.63	+18-39	684.12	- 0-10	36.81	+1.10
315	-457.24		-365.32		-56.92	0.20	360	- 5.24	1.25-08	-684.22		-35.71	

TABLE IV.—Continued.

PERTURBATIONS OF THE CO-ORDINATES IN UNITS OF THE SIXTH DECIMAL.

ARGUMENT I.

						III O DII	ENI I.						
Arg.	ξ1	Diff.	<b>7</b> 1	Diff.	ζ1	Diff.	Arg.	ξı	Diff.	7/1	Diff.	ζ1	Diff.
°	-577		+177		+21		45	+ 303		+928		+37	
1	570	+ 7	201	+24	21	0	46	339	+86	933	+ 5	38	+1
2	562	8	225	24	21	0	47	375	36	936	8	38	0
3	554	8	248	28	22	+1	48	412	87	938	2	39	1
4	545	9	271	23	22	0	49	450	38	940	+ 2	40	1 1
5	536	9	294	23	22	0	50	488	38	939	- 1	41	i
6	526	10	316	22	22	0	51	527	89	938	1	41	0
7	515	11	338	22	23	1 1	52	567	40	935	8	42	1 1
8	504	11	360	22	23	0	53	607	40	930	5	43	1
9	493	11	381	21	23	0	54	648	41	925	5	44	1
	400	12	301	21	~0	0	J 72	Vic	41		8		1
10	-481		+402		+23		55	+ 689		+917	1	+45	i l
11	468	+13	423	+21	24	+1	56	731	+42	908	- 9	46	+1
12	455	13	444	21	24	0	57	773	42	898	10	46	0
13	441	14	464	20	24	0	58	815	. 42	885	13	47	1
14	427	14	484	20	24	0	59	857	42	871	14	48	1
15	413	14	503	19	24	0	60	900	48	856	15	49	1
16	398	15	522	19	25	1	61	942	42	838	18	50	1
17	383	15	542	20	25	0	62	985	48	819	19	50	0
18	367	16	560	18	25	0	63	1027	42	798	21	51	1
19	350	17	579	19	25	0	64	1069	. 42	775	23	51	0
-	0.00	17		18		1			42		25		1
20	-333	+17	+597		+26	+0	65	+1111	+42	+750	-27	+52	+0
21	316		615	+18	26		66	1153	-	723		52	1
22	298	18	633	18	26	0	67	1194	41	695	28	53	0
23	279	19	650	17	26	0	<b>6</b> 8	1234	40	665	80	53	+1
24	260	19	667	17	27	1	69	1274	40	632	. 83	54	1 11
25	241	19	684	17	27	0	70 ´	1314	40	598	34	54	0
26	220	21	701	17	27	0	71	1352	38	563	85	54	0
27	200	20	717	16	<b>2</b> 8	1	72	1390	38	525	38	54	0
28	178	22	733	16	28	0	73	1427	87	485	40	54	0
29	156	33	749	16	28	0	74	1463	86	444	41	54	0
		23		15		1			85	l	48		-ı
30	-133	+24	+764	+15	+29	+0	<b>7</b> 5	+1498	+84	+401	-45	+53	-o
31	109	24	779	14	29	.0	76	1532	32	356	46	53	ŏ
32	85	25	793	14	29	1	77	1564	81	310	48	53	1
33	60	26	807	14	30	ô	<b>7</b> 8	1595	80	262	50	52	i
34	34	26	821	13	30	1	79	1625	28	212	51	51	0
35	- 8	28	834	13	31	Ô	80	1653	27	161	58	51	i
36	+ 20	28	847	13	31	1	81	1680	25	108	54	50	i
37	48	20	859	11	32	6	82	1705	24	+ 54	56	49	2
38	77	80	870	11	32	1	83	1729	22	- 2	57	47	i
39	107		881		33		84	1751		59		46	
ا مما	1100	30	1001	10	, 60	0	OF.	1 1 10001	20	110	59	+45	1
40	+137	+32	+891	+ 9	+33	+1	85 ec	+1771	+18	-118	-60	+45 43	-2
41	169	32	900	8	34	1	86	1789	16	178	61	43 41	2
42	201	83	908	8	35 25	0	87	1805	14	239	62	40	1
43	234	84	916	7:	35 36	1	88	1819	12	301	64	38	2
44	268	+35	923	+ 5	36	+1	89	1831	+10	365	-64		-2
45	+303		+928	<u> </u>	+37		90	+1841		<b>-42</b> 9		+36	

TABLE IV.—Continued.

PERTURBATIONS OF THE CO-ORDINATES IN UNITS OF THE SIXTH DECIMAL.

ARGUMENT I.

Arg.	કૃ	Diff.	$\eta_1$	Diff.	ζ,	Diff.	Arg.	ξ <sub>1</sub>	Diff.	$\eta_1$	Diff.	ζ <sub>1</sub>	Diff.
			400										
90	+1841	+7	- 429	-66	+ 36	-2	135	- 408	-96	-2839	- 1	-116	-8
91	1848	6	495	66	34	8	136	506	99	2840	+ 8	119	8
92	1854	+ 35	561	67	31	. 2	137	605	99	2837	6	122	8
93	1857	0	<b>62</b> 8	68	29	2	138	704	99	2631	11	125	2
94	1857	-1	696	69	27	8	139	803		2820	14	127	3
95	1856		765		24	_	140	902	99	<b>2</b> 80 <b>6</b>	l .	130	2
96	1851	5	834	69	21	8	141	1001	99	2788	18	132	1 1
97	1844	7	904	70	18	8	142	1100	99	2767	21	134	2
98	1835	9	975	71	15	8	143	1198	98	2741	96	136	2
99	1823	12	1045	70	12	8	144	1295	97	2712	29	138	2
		15		71		8	•		96	•	88	1	2
100	+1808	-17	-1116	-71	+ 9	-8	145	-1391		-2679	+ 37	-140	-1
101	1791		1187		6		146	1487	-96	2642	1	141	2
102	1771	20 23	1259	72	+ 3	8 8	147	1581	94	2602	40	143	1
103	1748		1330	71	0	•	148	1674	93	2558	44	144	1
104	1722	26	1401	71	4	4	149	1766	92	2510	48	145	1
105	1693	29	1471	70	7	8	150	1856	90	2459	51	146	1
106	1661	83	1542	71	11	4	151	1944	88	2405	54	147	1 1
107	1626	85	1612	70	14	8	152	2030	86	2347	58	148	1
108	1589	87	1681	69	18	4	153	2114	84	2286	61	148	0
109	1548	41	1749	68	22	4	154	2196	82	2221	65	149	-1
110		44	1018	68	~~	8		0000	80		67		0
110	+1504	-46	-1817	-66	- 25	-4 1	155	-2276	-78	-2154	+ 71	-149	0
111	1458	49	1883	66	29	4	156	2354	75	2083	74	149	0
112	1409	58	1949	64	33	4	157	2429	72	2009	76	149	+1
113	1356	55	2013	62	37	4	158	2501	70	1933	79	148	0
114	1301	58	2075	61	41	4	159	2571	66	1854	82	148	i
115	1243	61	2136	60	45	8	160	2637	64	1772	84	147	1
116	1182	61	2196	57	48	4	161	2701	1	1688	87	146	;
117	1118	66	2253	56	52	4	162	2762	61 57	1601	89	145	l i
118	1052	69	2309		56	1	163	2819	1	1512	92	144	;
119	983		2363	54	60.	4	164	2874	65	1420	1	143	]
120	+ 911	72	-2414	51		4	100	0005	51	1000	98		2
		-74		-49	- 64 60	-4	165	-2925	-48	-1327	+ 95	-141	+1
121	837	77	2463 9500	46	68	4	166	2973	44	1232	97	140	2
122 123	760 691	79	2509 0552	44	72 ~~	8	167	3017	41	1135	99	138	2
1	681 600	81	2553 9505	42	75	4	168	3058	87	1036	101	136	2
124	600	81	2595	38	79	4	169	3095	33	935	102	134	2
125	516	85	2633	35	83	3	170	3128	30	833	108	132	8
. 126	431	87	2668	33	86	4	171	3158	26	730	104	129	2
127	344	69	2701	29	90	4	172	3184	22	626	105	127	8
128	255	91	2730	26	94	3	173	3206	18	521	107	124	8
129	164	93	2756	22	97	3	174	3224	15	414	107	121	3
130	+ 71		<b>-277</b> 8		-100	•	175	-3239	19	- 307		-118	
131	- 22	93	2797	-19	104	-4	176	3249	, -10	200	+107	115	+8
132	117	95	2813	16	107	8	177	3255	6	- 92	108	112	8
133	213	96	2825	12	110	8	178	3258	- 8	+ 17	109	109	3
134	310	97	2834	9	113	3	179	3256	+ 2	125	108	105	4
135	<b>- 408</b>	-98	<b>-2839</b>	- 5	-116	-3	180	-3251	+ 5	+ 234	+109	-102	+8
		<del>' -</del>			<u> </u>	1	<u> </u>		1				<u>'</u>

TABLE IV.—Continued.

PERTURBATIONS OF THE CO-ORDINATES IN UNITS OF THE SIXTH DECIMAL.

ARGUMENT I.

ļ								<del></del>					
Arg.	ξ1	Diff.	η1	Diff.	ζ,	Diff.	Arg.	<b>દ</b> ા	Diff.	$\eta_1$	Diff.	ζ1	Diff.
180	-3251		+ 234		-102		225°	+ 122		+2878		+78	
181	3241	+ 10	342	+108	98	+4	226	220	+98	2857	-21	80	+2
182	3228	13	450	108	94	4	227	316	96	2832	25	82	2
183	3210	18	558	108	91	3	228	411	95	2804	28	84	2
184	3188	22	664	106	87	4	229	505	94	2773	81	86	2
185	3163	95	771	107	83	4	230	596	91	2738	85	88	2
186	3133	80	876	105	79	4	231	686	90	2700	38	90	2
187	3099	84	980	104	75	4	232	774	88	2659	41	92	2
188	3062	87	1083	108	70	5	233	859	85	2615	44	93	1
189	3020	42	1184	101	66	4	234	942	83	2568	47	94	1
103	00.00	45	1104	100	l ~	4	~~	02.0	81		50	"	1
190	-2975		+1284	j	- 62	1	235	+1023	1	+2518		+95	1 1
191	2926	+ 49	1382	+ 98	57	+5	236	1101	+78	2466	-52	96	+1
192	2874	52	1478	96	53	4	237	1177	76	2411	55	97	1
193	2817	57	1572	94	49	4	238	1250	78	2354	57	98	1
194	2758	59	1664	92	44	5	239	1320	70	2294	60	98	•
195	2695	63	1754	90	40	4	240	1388	68	2233	61	98	0
196	2628	67	1841	87	35	- 6	241	1453	65	2169	64	98	0
197	2558	70	1926	85	31	4	242	1514	61	2103	66	99	+1
198	2485	78	2008	82	26	5	243	1573	59	2036	67	98	-1
199	2410	75	2087	79	22	4	244	1629	56	1967	69	98	0
133	2110	79	2007	76		5	~~~	1020	58	1507	71	l ~	
200	-2331		+2163		- 17		245	+1682		+1896		+98	
201	2249	+ 82	2236	+ 78	13	+4	246	1732	+50	1824	-72	97	-1
202	2165	84	'2306	70	8	5	247	1778	46	1751	73	97	0
203	2079	86	2372	66	- 4	4	248	1822	44	1676	76	96	1
204	1990	89	2435	63	+ 1	5	249	1862	40	1601	75	95	1
205	1899	91	2495	60	5	4	250	1899	87	1524	77	94	1
206	1806	98	2551	56	10	5	<b>2</b> 51	1933	84	1447	77	93	1
207	1711	95	2603	52	14	4	252	1963	30	1369	78	92	1
208	1614	97	2651	48	18	4	253	1990	27	1291	78	90	3
209	1516	98	2696	45	23	5	254	2015	25	1212	79	89	1
		99		41		4		ļ	20		78		9
210	-1417	+101	+2737	+ 37	+ 27	+4	255	+2035	+18	+1134	-79	+87	-1
211	1316	102	2774		31		256	2053	14	1055	79	86	2
212	1214	102	2807	83 29	35	4	257	2067	12	976	79	84	2
213	1112	102	2836		39		258	2079	8	897	79	82	3
214	1008	104	2861	25	43	8	<b>25</b> 9	2087	6	818	1 '	80	2
215	905		2882	21	46		260	2093		740	78	78	2
216	801	104	2900	18	50	4	261	2095	+2	663	77	76	. 1
217	697	104	2913	18	54	4	262	2094	- 1	586	77	74	3
218	593	104	2922	9	57	8	263	2090	4	509	77	72	3
219	489	104	2927	5	60	8	264	2083	7	434	75	70	2
000		104	. 0000	+ 2		8			9		74		2
229	- 385	+103	+2929	- 8	+ 63	+4	265	+2074	-13	+ 360	-74	+68	9
221	282	102	2926	6	67	3	266	2061	15	286	72	66	8
222	180	102	2920	10	70	9	267	2046	17	214	71	63	2
223	- 78	100	2910	14	72	3	268	2029	21	143	69	61	9
224	+ 22	+100	2896	- 18	75	+3	269	2008	-23	74	-68	59	-3
225	+ 122		+2878		+ 78		270	+1985		+ 6	<u> </u>	+56	

TABLE IV.—Continued.

PERTURBATIONS OF THE CO-ORDINATES IN UNITS OF THE SIXTH DECIMAL.

ARGUMENT I.

Arg.	ξ1	Diff.	$\eta_1$	Diff.	ζ1	Diff.	Arg.	<b>દ્</b> ય	Diff.	$\eta_1$	Diff.	ζ1	Diff.
270°	+1985		+ 6		+56		315	- 20		-962		-10	
271	1960	-25	- 61	<del>-67</del>	54	-2	316	55	-35	944	+18	9	+1
272	1933	27	126	65	51	8	317	89	84	925	19	9	0
273	1903	30	189	68	49	2	318	122	33	905	20	8	1
274	1871	82	250	61	46	3	319	154	32	884	21	8	0
275	1837	84	309	59	44	2	320	185	31	863	21	7	1
276	1802	35	367	58	42	2	321	215	30	841	22	6	1
277	1764	38	422	55	39	8	322	243	28	818	23	6	0
278	1725	89	475	58	37	2	323	270	27	<b>7</b> 95	23	5	1 1
279	1684	41	527	52	34	8	324	296	26	771	24	4	1
l i		48		49		2			25		24		1
280	+1641	-44	- 576	-47	+32	2	325	-321	24	-747	+25	~ 3	+1
281	1597	45	623	45	30	8	326	345	23	722	25	2	1
282	1552	47	<b>66</b> 8	42	27	2	327	<b>36</b> 8	22	697	26	1	0
283	1505	47	710	40	25	2	328	390	20	671	26	- 1	1
284	1458	49	750	38	23	2	329	410	20 .	645	26	0	1
235	1409	49	788	36	21	8	330	430	18	619	26	+ 1	i
286	1360	50	824	88	18	2	331	448	17	593	27	2	1
287	1310	51	857	81	16	2	332	465	16	566	27	3	1
288	1259	51	888	28	14	2	333	481	16	539	27	4	1
289	1208		916		12		334	497		512		5	
290	+1156	52	- 942	26	+10	2	335	-511	14	-485	27	+ 6	1
291	1104	-52	966	-24	8	-2	336	524	-18	458	+27	7 7	+1
292	1052	52	988	22	7	1	337	536	12	431	27	8	1
293	999	58	1008	20	5	2	338	548	12	403	28	8	0
294	947	59	1025	17	3	. 2	339	558	10	376	27	9	1
295	895	52	1040	15	+ 2	1	340	567	9	348	28	10	1
296	843	52	1053	13	0	2	341	576	9	321	27	11	1
297	791	52	1064	11	- 1	1	342	583	7	293	28	12	1
298	740	51	1072	8	2	1	343	590	7	266	27	12	0
299	689	51	1079	7	4	2	344	595	5	239	27	13	1
		51		5		1			6		. 28		1
300	+ 638	-50	-1084	- a	- 5	-1	345	600	-4	-211	+27	+14	+0
301	588	49	1087	- 1	6	1	346	604	8	184	27	14	1
302	539	49	1088	+ 1	7		347	607	2	157	27	15	1
303	490	47	1087	3	7	1	348	609	- 2	130	27	16	0
304	443	47	1085	4	8	1	349	611	0	. 103	26	16	1
305	396	46	1081	6	9	ō	350	611	0	77	27	17	0
306	350	46	1075	7	9	-1	351	611	+1	50	26	17	1
307	304	44	1068	9	10	0	352	610	1	- 24	26	18	0
308	<b>26</b> 0	43	1059	10	10	0	353	609	8	+ 2	26	18	1
309	217	49	1049	12	10	0	354	606		28	25	19	0
310	+ 175	43	-1037		-10	"	355	-603	8	+ 53		+19	
311	134	-41	1024	+13	10	0	356	599	+ 4	79	+26	19	+0
312	94	40	1010	14	10	0	357	595	4	104	25	20	1
313	55	89	995	15	10	0	358	590	5	129	25	20	0
314	+ 17	88	979	16	10	0	<b>35</b> 9	584	6	153	24	20	0
315	- 20	-87	- 962	+17	-10	0	360	-577	+ 7	+177	+24	+21	+1

TABLE IV.—Continued.

PERTURBATIONS OF THE CO-ORDINATES IN UNITS OF THE SIXTH DECIMAL.

ARGUMENT II.

Arg.	ξ1	Diff.	$\eta_1$	Diff.	ζ,	Diff.	Arg.	ξ <sub>1</sub>	Diff.	7,1	Diff.	ζı	Diff
0			, 51		20		AE <sup>O</sup>	1110		1700	-	00	-
0	+551	- 1	+ 51	+14	-38	+1	45	+ 118	-26	+727	+12	-23	-0
1	550	2	65	13	37	0	46	92	26	739	11	23	0
2	548	1	78	13	37	1	47	66	27	750	10	23	1
3	547	1	91	14	36	1	48	39	27	760	9	24	0
4	546	2	105	13	35	i	49	+ 12	29	769	8	24	0
5	544	2	118	14	34		50	- 17	29	777	8	24	0
6	542	2	134	14	34	1	51	46	80	785	6	24	1
7	540	2	146	14	33	li	52	76	80	791	6	25	6
8	<b>53</b> 8	2	160	14	32	i	53	106	31	797	5	25	0
9	536	i -	174	1.4	31	ŀ	54	137		802	•	25	"
		. 2		14		0			82		8	١	1
10	+534	- 3	+188	+14	-31	+1	55	- 169	-82	+805	+ 8	-26	-0
11	531	8	202	15	30	1	56	201	82	808	+ 2	26	0
12	<b>528</b>	8	217	14	29	1	57	233	88	810	0	26	1
13	<b>525</b>	4	231	15	28	0	58	266	33	810	- 1	27	
14	521	4	246	15	28	1	59	299	34	809	1	27	0
15	517		261	1 1	27	1	60	333	1	807	2	27	1 -
16	513	4	276	15	27	0	61	367	84	804	8	27	0
17	508	5	292	16	26	1	62	401	34	799	5	27	0
18	503	5	307	15	25	1	63	435	84	793	6	28	-1
19	498	5	323	16	25	0	64	470	85	786	7	28	0
	400	6	0.00	16		1	-		84	1	8		0
20	+492	_	+339	ا ا	-24		65	- 504	1	+778		-28	l
21	485	- 7	355	+16	24	+0	66	538	-84	768	-10	28	0
22	478	7	371	16	24	0	67	573	35	756	12	28	0
23	470	8	387	16	23	1	<b>6</b> 8	607	84	744	12	28	0
24	462	8	404	17	23	0	69	641	84	730	14	28	0
25	453	9	420	16	22	1	70	674	88	714	16	28	0
26	444	9	437	17	22	0	71	708	34	697	17	28	0
27	434	10	453	16	22	0	72	740	32	679	18	28	0
28	423	11	470	17	22	0	73	773	88	660	19	27	+1
29	411	12	487	17	22	0	74	805	82	638	20	27	0
23	411	12	407	16	æ	+1	/4	005	31	030	92	21	0
30	+399		+503		-21		75	- 836	1	+616		-27	
31	386	<del>-</del> 13	520	+17	21	0	76	866	-80	592	-24	26	+1
32	372	14	536	16	21	0	77	896	80	567	25	26	0
33	358	14	553	17	21	0	78	925	29	540	27	26	0
34	342	16	569	16	21	0	79	953	28	512	28	25	1
35	326	16	585	16	21	0	80	980	27	483	29	24	1
36	309	17	601	16	21	0		1006	26	453	80	24 24	0
37		18	-	16		0	81		25		32	23	1
	291	18	617	15	21	0	82	1031	24	421	33		1
38	273	20	632	15	21	0	83	1055	22	<b>3</b> 88	84	22	0
39	253		647		21		84	1077		354		22	
40	+233	20	+661	14	-22	-1	85	-1098	21	+319	85	-21	1
41	211	-22	676	+15	-22 22	0	86	1118	20	282	-87	20	+1
41		22		18	22 22	0			19		37	20 19	1
	189	28	689	14		0	87	1137	17	245	39	- 1	1
43	166 142	94	70 <b>3</b> 715	12	. 22 22	0	88 89	1154 11 <b>7</b> 0	16	206 167	39	18 17	1

TABLE IV.—Continued.

PERTURBATIONS OF THE CO-ORDINATES IN UNITS OF THE SIXTH DECIMAL.

ARGUMENT II.

ļ				·					<u> </u>				
Arg.	ξ1	Diff.	<b>1</b> 1	Diff.	ζ1	Diff.	Arg.	ξ <sub>1</sub>	Diff.	ηι	Diff.	ζ1	Diff.
90	-1184		+ 127		-15		135	+ 5		-1420		+ 76	
91	1196	-12	86	-41	14	+1	136	61	+56	1424	-4	77	+1
92	1207	11	44	42	13	1	137	117	56	1425	- 1	79	2
93	1216	9	_	48	11	2	138	174	57	1424	+ 1	81	2
93	1223	7	+ 1 - 42	48	10	1	139	230	56	1424	8	83	2
	1	5		48		1		1	56		5	1	2
95	1228	4	85	45	9	. 2	140	286	56	1416	8	85	1
96	1232	- 2	130	44	7	- 2	141	342	56	1408	9	86	2
97	1234	0	174	45	5	1	142	398	55	1399	12	88	ī
98	1234	+ 2	219	46	4	2	143	453	56	1387	18	89	2
99	1232	. ~	265	1	- 2		144	509	1 :	1374	ł	91,	1 1
	1000	4	010	45	١ ,	2	4 45		54	***	16		1
100	-1228	+6	- 310	-46	0	+1	145	+ 563	+54	-1358	+18	+ 92	+1
101	1222	8	356	45	+ 1	2	146	617	68	1340	20	93	1
102	1214	10	401	46	3	2	147	670	53	1320	22	94	2
103	1204	11	447	45	5	2	148	723	61	1298	24	96	1
104	1193		492	46	7	2	149	774		1274	1	97	1 1
105	1179	14	538	45	9	2	150	825	51	1248	26	98	1
106	1163	16	583		11		151	875	50	1221	27	99	1
107	1146	17	627	44	13	2	152	923	48	1191	80	99	0
108	1126	20	671	44	15	2	153	971	48	1159	82	100	1 1
109	1104	22	715	44	17	2	154	1017	46	1126	38	101	1
		28		43		8			44		85		0
110	-1081		<b>- 75</b> 8	-42	+20		155	+1061	١ ا	-1091		+101	
111	1056	+25	800		22	+2	156	1105	+44	1054	+87	102	+1
112	1028	28	842	42	24	2	157	1147	42	1016	38	102	0
113	999	29	882	40	26	2	158	1187	40	976	40	102	0
114	968	81	922	40	29	8	159	1225	38	934	42	102	0
115	936	82	961	39	31	3	160	1262	87	891	48	103	+1
116	901	85	999	88	33	2	161	1297	85	847	44	103	0
117	865	36	1035	86	35	2	162	1330	88	801	46	102	-1
118	827	38	1070	35	38	8	163	1362	82	755	46	102	0
119	788	39	1104	34	40	2	164	1391	29	707	48	102	0
113	1	41	1101	33	1	2	103	1001	28		50	102	0
120	- 747		-1137		+42		165	+1419		- 657		+102	1 1
121	705	+42	1168	31	45	+8	166	1445	+26	607	+50	101	-1
122	661	44	1197	29	47	2	167	1468	28	556	51	101	0
123	616	45	1225	28	49	2	168	1489	21	504	52	100	1
124	569	47	1252	27	52	8	169	1509	20	452	52	99	1
125	522	47	1277	25	54	2	170	1526	17	398	54	99	0
126	473	49	1300	28	56	2	171	1541	15	344	54	98	1
127	423	50	1300 1321 ·	21	59	8	172	1554	18	290	54	97	1
	· ·	51	-	19	-	2		l	10		55		1
128	372	52	1340	17	61	2	173	1564	9	235	56	96	1
129	320	58	1357		63	9	174	1573	.	179	55	95	2
130	- 267	92	-1373	16	+65	3	175	+1579	"	- 124	90	+ 93	*
131	214	+58	1386	-18	67	+2	176	1582	+ 3	68	+56	92	-1
132	160	54	1398	12	69	9	177	1584	+ 2	- 12	56	91	1
		55		10		3			- 1		56		1
133	105	56	1408	7	72	2	178	1583	8	+ 44	56	90	2
134	- 50	+55	1415	+ 5	74	+2	179	1580	- 5	100	+66	88	-1
135	+ 5		-1420		+76		180	+1575		+ 156		+ 87	

TABLE IV.—Continued.

PERTURBATIONS OF THE CO-ORDINATES IN UNITS OF THE SIXTH DECIMAL.

ARGUMENT II.

Arg.	ξ1	Diff.	$\eta_1$	Diff.	ζ1	Diff.	Arg.	ξı	Diff.	η <sub>1</sub>	Diff.	ζι	Diff.
180	+1575		+ 156		+87		225	- 291		+1353		- 6	
181	1567	- 8	211	+55	85	-2	226	342	-51	1337	-16	8	2
182	1557	10	266	55	83	2	227	393	51	1318	19	10	2
183	1545	13	321	55	82	1	228	443	50	1298	20	11	1
184	1531	14	375	54	80	2	229	492	49	1276	22	12	1
185	1514	17	428	63	78	2	230	539	47	1252	24	14	2
186	1496	18	481	53	76	2	231	586	47	1226	26	15	1
187	1475	21	533	52	74	2	232	631	45	1199	27	17	2
188	1452	28	584	51	72	2	233	675	44	1170	29	18	1
189	. 1427	25	635	51	70	2	234	717	42	1140	80	19	1
	. 20.00	27	<b>V</b>	49		2		'-'	41		32		1
190	+1400		+ 684	1.0	+68		235	- 758		+1108		20	
191	1372	-28	732	+48	66	-2	236	798	-40	1075	-83	21	-1
192	1341	81	779	47	64	2	237	836	38	1040	85	22	1
193	1308	88	825	46	62	2	<b>23</b> 8	872	86	1004	36	23	1
194	1274	84	870	45	60	2	239	907	35	967	87	24	1
195	1238	36	913	43	5 <b>7</b>	3	240	940	38	929	38	25	1
196	1200	38	955	42	55	2	241	971	31	890	39	26	1
197	1160	40	995	40	53	2	242	1001	80	850	40	27	1
198	1119	41	1033	38	51	2	243	1028	27	809	41	27	0
199	1076	48	1071	38	48	8	244	1054	26	767	42	28	1
		44		85		2			. 24		43		1
200	+1032		+1106	ا معد ا	+46		245	-1078		+ 794	١	-29	
201	987	~45	1140	+84	44	-2	246	1100	-22	681	-48	29	-0
202	941	46	1172	82	41	8	247	1120	. 30	637	44	30	1
203	893	48	1202	80	<b>3</b> 9	2	<b>24</b> 8	1138	18	593	44	30	0
204	844	49	1230	28	37	2	249	1154	16	<b>54</b> 8	45	31	1
205	794	50	1256	26	34	3	250	1168	14	503	45	31	0
206	743	51	1281	25	32	2	251	1181	18	458	45	32	1
207	<b>6</b> 91	52	1303	22	30	2	252	1191	10	412	46	32	0
<b>20</b> 8	639	52	1324	21	28	2	253	1199	8	367	45	32	0
209	585	54	1342	18	25	8	254	1205	6	<b>3</b> 21	46	33	1
		54		16		2			5	ł	45		0
210	+ 531	-54	+1358	+15	+23	-2	255	-1210	- 2	+ 276	-46	-33	-o
211	477	55	1373	12	21	2	256	1212	- 1	230		33	0
212	422	55	1385	10	19	2	257	1213	+ 2	185	45	33	0
213	367	56	1395	8	17	2	258	1211	8	141	44	33	1
214	311	55	1403	6	15	8	259	1208	1	96	45	34	
215	256	56	1409	4	12	2	260	1203	5	52	44	34	0
216	200	56	1413	+ 1	10	2 2	261	1196	7	+ 9	48	34	0
217	144	55	1414		8	_	262	1187	9	- 34	48	34	
218	89		1414	0	6	2	263	1177	10	76	42	34	0
219	+ 33	56	1412	- 2	4	2	264	1165	12	118	42	34	0
000		55		5	١	1			14		40		0
220	- 22	55	+1407	-7	+ 3	-2	265	-1151	+15	- 158	-40	-34	<b>−</b> 0
221	77	54	1400		+ 1	2	266	1136	17	198	39	34	0
222	131	54	1391	10	- 1	2	267	1119	18	237	87	34	0
223	185	53	1381	18	3	2	<b>26</b> 8	1101	20	274	1	34	
224	238	-58	1368	-15	5	-1	<b>2</b> 69	1081	+21	311	37 -36	34	-0
225	- 291		+1353	10	- 6	1 *	270	-1060	T21	- 347	-80	-34	"

TABLE IV.—Continued.

PERTURBATIONS OF THE CO-ORDINATES IN UNITS OF THE SIXTH DECIMAL.

ARGUMENT II.

Arg.	કૃ	Diff,	<b>7</b> 1	Diff.	ζ1	Diff.	Arg.	ξ <sub>1</sub>	Diff.	<b>1</b> / <sub>1</sub>	Diff.	ζ1	Diff.
270°	-1060		-347		-34		315	+385		-647		-46	
	1037	+23	382	-85		<b>−</b> 0			+20	-	+16		-0
271 272	1013	24	302 415	88	34	0	316 31 <b>7</b>	305 324	19	631 615	16	46	0
		25		32	34	0 1			18		16	46	1
273	988 '	26	447	81	34	0	318	342	17	599	16	47	0
274	962	27	478	30	34	١٠	319	359	16	583	17	47	1
275	935	28	508	29	34	0	320	375	16	566	17	48	0
276	907	29	536	28	34	ō	321	391	14	549	17	48	0
277	878	80	564	96	34	o	322	405	14	532	17	48	ı
278	848	80	590	24	34	0	323	419	13	575	17	49	0
279	818		614		34	l 1	324	432	1 1	498	l :	49	•
280	- 786	33	637	23	-34	0	325	+444	19	-481	17	<b>-4</b> 9	0
281	754	+39	658	-21	34	-0	326	455	+11	463	+18	49	<b>−</b> 0
282	722	82	678	20	34	0	327	466	11	446	17	50	-1
283	689	83	697	19	34	0	328	476	10	429	17	50	0
263 284	655	84	714	17	34	0	329	485	9	412	17	50 50	0
285 285	621	84	714	16	34 35	1	330	480 493	8	394	18	50 50	0
286	587	84	744	14	35	0	331	501	8	377	17	50	0
287	552	85	744 757	18		0	332		7	-	17	50 50	0
		85		12	35	0		508	6	360	17	50 50	0
288	517	84	769	10	35		333	514	6	343	16		0
289	483	85	779	. 9	35	1	334	520		327		50	0
290	- 448	85	-788		-36	1	335	+525	5	-310	17	-50	"
291	413	+35	795	- 7	36	-0	336	530	+ 5	294	+16	50	0
292	378	85	801	6	36	0	337	534	4	277	17	50	0
293	344	84	806	5	36	0	338	538	4	261	16	50	0
294	309	85	810	4	37	1	339	541	8	245	16	50	0
295	275	34	812	2	37	0	340	544	8	230	15	49	+1
296	241	34	813	- 1	37	0	341	547	8	214	16	49	0
297	208	83	813	0	38	1	342	549	2	199	15	49	0
298	175	33	811	+ 2	38	0	343	551	2	184	15	49	0
299	143	82	809	2	38	0	344	552	1	169	15	48	1
200	140	82	000	4	30	1	922	002	1	105	15	•	
300	- 111		-805		-39		345	+553		-154		<b>-4</b> 8	*
301	79	+82	800	+ 5	39	⊸	346	554	+ 1	140	+14	47	+1
302	48	81	795	5	40	1	347	555	1	125	15	47	0
303	- 18	80	788	7	40	0	348	556	+ 1	111	14	46	1
304	+ 12	80	780	8	40	0	349	556	0	97	14	46	0
305	41	29	772	8	41	1	350	556	0	83	14	45	1
306	69	28	762	10	41	0.	351	556	0	69	14	45	0
307	96	27	752	10	42	1	352	556	0	56	18	44	1
308	123	27	741	11	42	0	353	556	0	42	14	43	1
309	148	25	729	12	43	1	354	555	- 1	29	18	43	0
-		25	.~~	12	70	0	[ ~~		0	· ~~	14	~	1
310	+ 173		-717		<b>-43</b>		355	+555	ł	- 15		-42	
311	197	+24	704	+13	44	-1	356	554	- 1	- 2	+18	41	+1
312	221	24	690	14	44	0	357	553	1	+ 11	18	40	1
313	243	22	676	14	45	1	358	553	0	25	14	40	0
314	265	22	662	14	45	0	359	552	1	38	18	39	1
315	+ 285	+20	-647	+15	-46	-1	360	+551	- 1	+ 51	+13	-38	+1

TABLE IV.—Continued.

PERTURBATIONS OF THE CO-ORDINATES IN UNITS OF THE SIXTH DECIMAL.

ARGUMENT III.

Arg.	ક્	Diff.	7/1	Diff.	ζ <sub>1</sub>	Diff.	Arg.	ξ1	Diff.	η,	Diff.	ζ,	Diff.
°	+977		-196		+15		45°	+537		-829		- 7	
1	973	-4	213	-17			46	522	-15	<b>83</b> 8	-9	İ	
2	969	4	230	17		-2	47	506	16	847	9		-2
3	965	4	247	17	13		48	491	15	856	9 .	9	
. 4	960	5	264	17			49	475	16	865	9		
5	955	5	281	17		1.	50	460	15	873	8	i	1
6	950	5	298	17	12		51	444	16	881	8	10	
7	945	5	314	16			52	428	16	889	8		
8	939	6	331	17		1	53	412	16	896	7	1	2
9	933	6	347	16	11		54	395	17	903	7	12	1.
		6		17					16		7		
10	+927	_	-364			_ 1	55	+379		-910	١ ـ	}	1 _
11	920	- 7	380	-16		2	56	<b>36</b> 3	-16	917	-7	ŀ	1
12	913	7	396	16	9		57	346	17	923	6	13	1
13	906	7	412	16		_	58	329	17	929	6	1	_
14	898	8	428	16		1	59	312	17	935	6	ł	1
15	890	8	444	16	8		60	296	16	941	6	14	}
16	882	8	459	15			61	279	17	946	5		1
17	874	8	475	16		2	62	261	18	951	5	Į	2
18	865	9	490	15	6		63	244	17	955	4	16	}
19	856 .	9	505	15			64	227	17	960	5	i	l
		9		15		1			17	· -	4 .	ļ	1
20	+847	- 9	-520	_,,			65	+210		-964	3	j	
21	838		535	-15	5		66	192	-18	967	-	17	j
22	828	10	550	15		2	67	175	17	971	4	1	١.
23	818	10	564	14		*	68	158	17	974	3	1	1
24	808	10	<b>57</b> 8	14	3		69	140	18	977	8	18	1
25	797	11	592	14		_	70	123	17	979	3		
26	786	11	606	14		1	71	105	18	981	2	ł	1
27	775	11	620	14	+ 2		72	87	18	983	2	19	
28	764	11	633	13		_	73	70	17	985	2		
29	752	12	647	14		3	74	52	18	986	1		1
		12		18					17		1		
30	+740	-12	660	-13	0		75	+ 35	-18	-987	-1	20	
31	728	12	673	12		1	76	+ 17	18	988	-1		1
32	716	13	685	12		•	77	- 1	*17	989			
33	703	12	698	12	- 1		78	18	18	989	0	21	
34	691	13	710			,	79	36		989	+1		1
35	<b>67</b> 8	18	722	12		2	80	53	17	988	1		'
36	665	18	734	12	3		81	71	18	987		22	[
37	651		745	11		, ,	82	<b>8</b> 8	17	986	1		
38	638	13	756	11		1	83	106	18	985	1		1
39	624	14	768	13	4		84	123	17	983	2	23	
		14		11					18		2		
40 .	+610	-18	<b>-779</b>	-10		2	85	-141	-17	-981	+2	•	1
41	595	14	789	11	_	1	86	158	17	979	2		
42	581	14	800	10	6		87	175	17	977	8	24	
43	567	15	810	10		- <u>ı</u>	88	192	17	974	8		-1
44	552	-15	820	- g		•	89	209	-17	971	+4		•
45	+537		-829		- 7		90	-226		-967		-25	

TABLE IV.—Continued.

PERTURBATIONS OF THE CO-ORDINATES IN UNITS OF THE SIXTH DECIMAL.

ARGUMENT III.

Arg.	ξ <sub>1</sub>	Diff.	η1	Diff.	ξ1	Diff.	Arg.	<u></u> ξ	Diff.	7,	Diff.	ζ,	Diff.
				<del></del>	ļ	-	135				-	<b></b>	
90	-226	-17	-967	+ 8	-25			-834	-8	548	+14	-27	1
91	243	17	964	4	l	-1	136	842	8	534	15	Ι .	+0
92	260	17	960	4	<u>~</u>		137	850	8	519	14	l	
93	277	17	956	5	26		138	858	8	505	15	27	
94	294	16	951	5		0	139	866	8	490	16	1	1
95	310	17	946	5	-00		140	874	7	475	15		
96	327	16	941	5	26		141	881	7	460	15	26	
97	343	16	936	6		1 1	142	888	6	445	15	ł	0
98	359	16	930	6		_	143	894	7	430	15		
99	375		924		27		144	901	l	415		26	
100	-391	16	<b>-9</b> 18	6			145	-907	6	-399	16	l	
101	407	-16	911	+7		0	146	913	-6	384	+15	l	1
102	423	16	905	6	27		147	918	5	368	16	25	1
103	438	15	898	7	~"		148	924	6	352	16	[ ~	
103	454	16	890	8		-1	149	924	5	336	16	l	0
105	469	15	883	7	28		150	933	4	320	16	25	1
106	484	15	8 <b>7</b> 5	8	20		151	938	5	304	16	~	
107	499	15	767	8		0	152	942	4	288	16	l	1 1
108	513	14	859	8	28		153	942	4	272	16	24	1
109	528	15	850	9	20		154	950.	4	255	17	<i>~</i>	1 .
109	020	14	000	ا و ا		0	104	950.	3	200	16	i	1
110	-542		-841			•	155	-953		-239	1	l	•
111	557	-15	832	+9	28		156	956	8	222	+17	23	1
112	571	14	823	9			157	959	8	206	16	l	
113	584	13	813	10		0	158	961	2	189	17	Į.	1
114	598	14	803	10	28		159	963	2	172	17	22	
115	611	13	793	10			160	965	2	155	17	}	
116	625	14	783	10		0	161	967	2	139	16		1
117	638	13	772	11	28		162	968	1	122	17	21	1 1
118	651	13	762	10			163	969	1	105	17		
119	663	19	751	11		0	164	970	-1	88	17		1
		18		11					0		17		
120	-676	-12	-740	<b>+12</b>	28		165	-970	0	- 71	+17	20	
121	688	12	<b>72</b> 8	11		٥	166	970	0	54	17		1
122	700	13	717	1		۷	167	970	-	37	17		'
123	711	11	705	12 12	28		168	970	0 +1	20	17	19	
124	723	11	693	1			169	969		- 3	17		,
125	734	11	681	12		0	170	968	1	+ 14			1
126	745	_ 1	668	18	28		171	967	1	31	17	18	
127	756	11	655	18			172	965	2	48	47		
128	767	11	643	12		0	173	964	1	65	17		1
129	777	10	630	13	28		174	962	3	82	17	17	
,,,		10	0-0	14					8		17		ļ
130	-787	-10	-616	+13			175	-959	+2	+ 99	+17		2
131	797	9	603	13			176	957	8	116	17		-
132	806	10	590	14	28		177	954	4	133	17	15	1
133	816	9	576	14		+1	178	950	8	150	16		+1
134	825	<b>– 9</b>	. 562	+14			179	947	+4	166	+17		-
135	-834		-548		-27		180	-943		+183		-14	

TABLE IV.—Continued.

PERTURBATIONS OF THE CO-ORDINATES IN UNITS OF THE SIXTH DECIMAL.

ARGUMENT III.

Arg.	ξı	Diff.	η1	Diff.	ζ1	Diff.	Arg.	ξį	Diff.	η1	Diff.	ζι	Diff.
180	-943		+183		-14	i	225	-524		+816		+ 7	
181	. 939	+ 4	200	+17	-14		226	510	+14	826	+10	T .	i i
182	935	4	217	17		+1	227	496	14	835	9		+1
183	930	5	233	16	13	l	228	482	14	844	9	8	
184	925	5	250 250	17	10		229	467	15	853	9		
185	920	5	266	16		1	230	453	14	862	9		2
		5	283	17	10				15		9	٠,	
186	915	6		16	12		231	<b>43</b> 8	15	871	8	10	
187	909	6	299	16		2	232	. 423	14	879	8		1
188	903	6	315	16			233	409	15	887	8		-
189	897		331	_	10		234	394	1 1	895		11	
190	-891	6	+347	16			235	-378	16	+902	7	ł	
190	-031 884	+ 7	363	+16	ı	1 1	236	-376 363	+15	909	+7		1
	877	7	379	16	9		237	348	15	916	7	12	
192		7		16	9				16		7	12	
193	870	7	395 411	16		1	238 239	332	15	923	6	ľ	2
194	863	8		15				317	16	929	6		
195	855	8	426	16	. 8	l i	240	301	16	935	6	14	
196	847	8	442	15		2	241	265	16	941	6	ı	1 1
197	839	8	457	15	_		242	269	16	947	5		1
198	831	9	472	15	6		243	253	16	952	5	15	
199	822		487				244	237		957		}	
200	019	9	+502	15		1	245	-221	16	1001	4	1	1
200	-813	+ 9		+15	_	i i			+16	+961	+ 5	1.0	1
201	804	9	517	14	5	i	246	205	16	966	4	16	
202	795	10	531	15		9	247	189	16	970	4		1
203	785	9	546	14	_	[	248	173	17	974	8		-
204	776	10	560	14	3		249	156	16	977	3	17	
205	766	11	574	14		1	250	140	17	980	8	l	2
206	755	10	588	14		_	251	123	. 16	983	3		-
207	745	11	602	13	- 2		252	107	17	986	2	19	1
208	734	10	615	14		9	253	90	16	988	2		1
209	724		629			*	254	74		990	1	1	•
010	~10	11	1640	13	_	1	OFF	-~	17		2		
210	-713 701	+12	+642 655	+13	0		255 256	- 57	+17	+992	+ 1	20	
211		11		18		1		40	16	993	1	1	1
212	690	19	668	13			257	24	17	994	1		
213	678	12	681	12	+ 1		258 250	- 7	17	995	0	21	
214	666	12	693	12		2	259	+ 10	16	995	0	Í	1
215	654	12	705	12		"	260	26	17	995			
216	642	12	717	12	3		261	43	17	995		22	
217	630	13	729	12		1	262	60	17	995	- 1	Ì	1
218	617	13	741	11	Ī	•	263	77	16	994	i		•
219	604	: !	752		4		264	93		993	i -	23	
220	-591	13	+763	11			265	+110	17	+991	9	l	
		+18		+11		1			+17		- 1	l	1
221	578	13	774	11			266	127	16	990	2		
222	565	14	785	11	5		267	143	17	968	8	24	
223	551	18	796	10		+2	268	160	17	985	9	l	+0
224	538	+14	806	+10			269	177	+16	983	- 8		
225	-524		+816		+ 7		270	+193		+980		+24	

TABLE IV.—Continued.

PERTURBATIONS OF THE CO-ORDINATES IN UNITS OF THE SIXTH DECIMAL.

ARGUMENT III.

Arg.	<b>ξ</b> 1	Diff.	<b>7</b> 1	Diff.	ζ,	Diff.	Arg.	₹1	Diff.	7/1	Diff.	ζ <sub>1</sub>	Diff.
270°	+193		+980		+24		315	+821		+561		+28	
271	210	+17	977	- 8	744		316	830	+ 9	547	-14	.~~	1
272	226	16	973	4		+1	317	840	10	533	14		⊸
273	242	16	969	4	25		318	849	9	518	15	28	
274	259	17	965	4	20		319	858	9	502	16	<b> </b> ~	
275	275	16	961	4		1	320	867	9	486	16	1	1 1
276	291	16	956	6	26		321	875	8	471	15	27	
277	307	16	951	5	20		322	883	8	455	16	~	
278	324	17	946	5		0	323	891	8	439	16	ł	0
279	340	16	940	6	26		324	899	8	423	16	27	
213	510	15	540	6	20		0.52	000	7	1 420	16	~'	
280	+355		+934				325	+906		+407		1	
281	371	+16	928	-6		1	326	913	+ 7	391	-16		1 1
282	387	16	921	7	27		327	920	7	375	16	26	
283	403	16	915	6			328	927	7	359	16		
284	418	15	908	7		0	329	933	6	342	17		1 1
285	433	15	900	8	27		330	939	6	325	17	25	
286	449	16	893	7			331	945	6	309	16	l	l i
287	464	15	885	8		3	332	950	5	292	17	1	1
288	479	15	876	9	28		333	955	5	275	17	24	1
289	494	15	868	8			334	960	5	258	17	l	1
		15		9		0			4		17		0
290	+509	+14	+859	- 9			335	+964	+ 5	+241	-17		
291	523		850	9	28		336	969	1	224	l .	24	}
292	<b>53</b> 8	5	841	10		0	337	973	4	206	18		١.,
293	552	14 14	831	9	•	"	338	976	3	189	17	i	1
294	566	14	822	10	28		339	979	3	172	17	23	1
295	580		812	11		+1	340	982	3	154	18		١, ١
296	594	14 14	801	10		**	341	985	8 2	137	17		1
297	608	13	791	11	29		342	987	2	120	18	22	
298	621	14	780	11		0	343	989	2	102			1 1
299	635		<b>76</b> 9			ľ	344	991	1	84	18		1
000	. C40	18		12			045		2	. ~	17		
300	+648	+18	+757	-11	29	1	345	+993	+ 1	+ 67	-18	21	1
301	661	12	746	12		0	346	994	+ 1	49 32	17		1
302	673	13	734	12	600		347	995	0		18		
303	686	12	722	12	29		348	995	0	+ 14	18	20	
304 305	698	18	710 697	13		0	349 350	995 995	0	21	17	l	1
	711	12		12	60				0		18	10	
306	723	11	685	18	29		351	995	- 1	39	17	19	
307	734	12	672	18		-1	352	994	1	56	18		2
308	746	11	659	14	۰		353	993	1	74	17	1 ,,,	1 1
309	757	11	645	13	28		354	992	i	91	1	17	1 1
310	+768		+632		l		355	+990	2	-109	18		1 1
311	779	+11	618	-14	l	0	356	988	- 2	126	-17		1
312	790	11	604	14	28		357	985	3	144	18	16	1
313	801	11	590	14	l ~		358	983	2	161	17	l ~	[ ]
314	811	10	576	14		0	359	980	3	178	17	I	-1
315	+821	+10	+561	-15	+28		360	+977	- s	-196	-18	+15	
010	T061	<u> </u>	וטטד ו		T20	<u> </u>	JOU	Till	<u></u>	-190	<u> </u>	I TIU	

TABLE IV.—Continued.

PERTURBATIONS OF THE CO-ORDINATES IN UNITS OF THE SIXTH DECIMAL.

ARGUMENT IV.

 	· · · · · · · · · · · · · · · · · · ·	ABGUMENT IV.										. <del></del>	
Arg.	ξ1	Diff.	71	Diff.	ζ1	Diff.	Arg.	<b>ક</b> ા	Diff.	71	Diff.	ζ,	Diff.
°	-775		+ 75		+38		45°	-502		+691		+ 6	
1	773	+ 2	90	+15		i	46	492	+10	702	+11		ł
2	772	1	106	16		-2	47	482	10	713	11	i	-4
3	770	2	121	15	36		48	471	11	723	10	+ 2	1
4	768	2	137	16			49	460	11	734	11	`~	1
5	765	8	152	15		1 1	50	450	10	744	10		4
6		2		15	35			i e	11	1	10	- 2	
7	763	3	167	15	30		51	439	12	754	9	- z	
	760	8	182	15		1	52	427	11	763	10		4
8	757	8	197	16	0.4		53	416	11	773			
9	754		213	ا ا	34		54	405	İ	782		6	ĺ
10	-750	4	+228	15			55	-393	12	+791	9		
1		+ 3	243	+15		2			+11	800	+ 9	ŀ	4
. 11	747	4		14	20		56	382	12		9	۱ ,,	
12	743	4	257	15	32		57	370	12	809	8	10	
13	739	4	272	15		2	58	358	12	817	8		
14	<b>73</b> 5	5	287	15	•	_	59	346	12	825	8		, -
15	730	5	302	14	30		60	334	12	833	8	15	l
16	725	5	316	15		, ,	61	322		841	i		١
17	720	1	331			1	62	310	12	848	7		5
18	715	5	345	14	29		63	<b>2</b> 98	12	856	8	20	1
19	710	5	359	14			64	285	18	863	7		1
		6		15		2			12		6 -		5
20	-704	+ 5	+374	٠., ا			65	-273	+13	+869	1		
21	699		388	+14	27		66	260		876	+ 7	25	
22	693	6	402	14			67	248	12	882	6		
23	687	6	416	14		2	<b>6</b> 8	235	13	888	6		5
24	680	7	430	14	25	1	69	222	13	894	6	30	ł
25	674	6	443	13			70	209	13	899	5		Ī
26	667	7	457	14		2	71	196	13	904	5		5
27	660	7	470	13	23		72	183	13	909	5	35	ĺ
28	653	7	484	14			73	170	18	914	5		
29	645	8	497	13		2	74	157	13	918	4		6
~~	040	7	101	13			' '	10.	18	310	4		
30	-638		+510		21		75	-144		+922		41	Į
31	630	+ 8	523	+13			76	130	+14	926	+ 4		
32	622	8	536	13		3	77	117	18	929	3		5
33	614	8	549	13	18		78	103	14	932	8	46	
34	605	9	562	13			79	90	13	935	3		
35	597	8	574	12		8	80	<b>7</b> 6	14	937	2		6
36	588	9	587	13	15		81	63	13	940	8	52	
		9		12	10		82	49	14		2	22	
37	579	9	599	12		8		_	14	942	1		5
38	570	9	611	12			83	35	14	943	1		
39	561		623		12		84	21		944		57	
40	-552	9	+635	12			85	- 8	13	+945	1		
- 1		+10	646	+11		8	86		+14	+945 946	+ 1		6
41	542	10		12	ا م				14		0	co	
42	532	9	658	11	9		8 <b>7</b>	20	14	946	0	63	
43	523	10	669	11		-3	88	34	14	946	ŏ		5
44	513	+11	680	+11		•	89	48	+14	946	- 1		_
45	-502		_+691_		_+6_		90	+ 62		+945		<b>-6</b> 8	

TABLE IV.—Continued.

PERTURBATIONS OF THE CO-ORDINATES IN UNITS OF THE SIXTH DECIMAL.

ARGUMENT IV.

H.		And Calabia 11.												
	Arg.	ξ1	Diff.	η1	Diff.	ζ1	Diff.	`Arg.	ξı	Diff.	η1	Diff.	ζ,	Diff.
	90°	+ 62		+945		<b>- 6</b> 8		135	+678		+605		-114	
ı	91	77	+15	944	-1			136	690	+12	591	-14	<b>l</b> .	
Į	92	91	14	943	1		-5	137	701	11	578	18	l	0
ı	93	105	14	941	2	73		138	712	11	564	14	114	
l	94	119	14	939	2		1	139	723	11	550	14		
ı	95	133	14	937	9		5	140	734	11	536	14	1	+1
H	96	147	14	935	2	78	1	141	745	11	522	14	113	ļ
l	97	162	15	932	8	.		142	755	10	507	15	]	
l	98	176	14	929	3		5	143	765	10	493	14	1	1
l	99	190	14	925	4	83		144	775	10	478	15	112	
I	"	100	14	0.20	4	, w	1			9	2.0	15	1	
	100	+204		+921	1			145	+784	1	+463			
ı	101	219	+15	917	- 4		4	146	794	+10	448	-15		2
ı	102	233	14	912	5	87		147	803	9	433	15	110	
	103	247	14	. 908	4	•		148	812	9	418	16		
	104	262	15	903	5		6	149	820	8	403	15	ł	2
ı	105	276	14	897	6	92		150	828	8	388	15	108	
l	106	290	14	891	6	J.		151	836	8	372	16		1
ı	107	305	15	885	6		4	152	844	8	357	15	l	8
	108	319	14	879	6	96		153	851	7	341	16	105	}
	109	333	14	872	7	50	1	154		7	325	16	100	}
	109	333	14	012	7		8	10-2	858	7	320	16		8
I	110	+347		4865				155	+865		+309	10		•
ı	111	362	+15	858	- 7	99		156	872	+ 7	293	-16	102	
ı	112	376	14	851	7	55		157	878	6	277	16	100	
ı	113	390	14	843	8		4	158	884	6	261	16		3
I	114	404	14	835	8	103		159	889	5	245	16	99	
	115	418	14	826	9	103		160	894	5	229	16	33	1
	116	432	14	817	9		3	161	899	5	213	16		4
	117	446	14	808	9	106		162	904	5	197	16	95	1
		459	13	799	9	100		163		4	181	16	1 80	1
l	118		14	î .	9		2		908	4		17		4
ı	119	473	14	790	10		ŀ	164	912	8	164		I	
ı	120	+487	14	+780	10	108		165	+915		+148	16	91	l
ı	121	500	+13	770	-10	100		166	918	+ 3	132	-16	"	<u> </u>
I	122	514	14	760	10		2	167	921	8	115	17		5
	123	527	13	749	11	110		1 <b>6</b> 8	923	2	99	16	86	1
ı	124	541	14	738	11	110		169	925	3	83	16	∞	Ī
		554	18	727	11		2	170		2		16	l	5
ı	125		18		11	110			927	1	67	17	.,	
H	126	567	13	716	12	112		171	928	+ 1	50	16	81	
H	127	580	13	704	11		1	172	929	0	34	16	l	5
ı	128	593	12	693	12		_	173	929	0	18	17		-
	129	605	_	681		113		174	929		+ 1	ł	76	
	130	+618	13	+669	12		i	175	+929	0	- 15	16	1	
	131	630	+12	656	-18		-1	176	928	- 1		-16	l	6
	132	643	13	644	12	114	1			1	31	16	70	1
۱		-	12		13	114		177	927	1	47	16	70	1
	133	655	12	631	18	l	0	178	926	2	63	16	1	+6
I	134	667	+11	618	-13			179	924	- 2	79	-16	۱	
II.	135	+678	<u> </u>	+605	<u> </u>	-114		180	+922	<u> </u>	<b>–</b> 95	<u> </u>	- 64	

TABLE IV.—Continued.

PERTURBATIONS OF THE CO-ORDINATES IN UNITS OF THE SIXTH DECIMAL.

ARGUMENT IV.

												•	
Arg.	<b>ξ</b> 1	Diff.	. <b>7</b> 1	Diff.	ζ1	Diff.	Arg.	<b>ξ</b> 1	Diff.	71	Diff.	ζ1	Diff
180°	+922		- 95		64		225°	+481		700		+38	
181	919	- 8	111	-16			226	465	-16	710	-10		1
182	916	8	127	16		+6	227	450	15	719	9		+6
183	913	3	143	16	58	i i	228	434	16	729	0	44	1
184	909	4	158	15			229	419	15	738	9		l
185	905	4	174	16		6	230	403	16	747	9	٠.	6
186	901	4	190	16	52		231	387	16	756	9	50	
187	896	5	205	15	- O.		232	371	16	764	8	~	1
188	891	5	221	16		7	233	355	16	773	9	l	6
189	885	6	236	15	45		234	339	16	781	8	56	
109	600	6	200	15	40		204	339	16	701	8	1	
190	+879		~251	"			235	+323	10	<b>-7</b> 89		1	
191	873	- 6	266	-15		7	236	307	-16	797	- 6		
192	866	7	281	15	38		237	291	16	805	8	61	1
193	859	7	296	15	30		238	274	17	812	7	l "	
194	852	7	311	15		7	239	258	16	819	7	}	
195	844	8	326	15	31		240	l	16	826	7	66	
196	836	8	340	14	91	•	l i	242 226	16	833	7	I <sup>™</sup>	
		8		15		7	241		16		6		5
197	828	9	355 960	14	64		242	210	17	839	7	<b>.</b>	
198	819	9	<b>36</b> 9	14	24		243	193	16	846	6	71	
199	810		383	١,, ١		_	244	177	1	852		}	1 . 1
200	+801	9	~397	14		7	245	+161	16	<del>~8</del> 57	•	}	•
201	791	-10	411	-14	17		246	145	-16	863	- 6	75	
201	781	10	425	14	17		247	129	16	8 <b>6</b> 8	5	l "	
203	771	10	438	13		7	248	113	16	873	5	l	4
203	760	11	452	14	10		249	97	16	878	5	79	
205	749	11		14	10		249 250	81	16	883	5	19	
	1	11	466	18		7			16		4	1	
206	738	11	479	13			251	65	16	887	4	-00	
207	727	12	492	18	- 3		252	49	15	891	4	82	
208	715	12	505	18		7	253	34	16	895	4		8
209	703		518	12	1		254	18		899	8		
210	+691	12	-530	12	+4		255	+ 3	15	<b>~9</b> 02	•	85	
211	678	-18	543	-18			256	- 13	-16	905	- 8	•	
212	665	13	555	12		7	257	28	15	908	8		8
213	652	18	567	12	11		258	43	15	911	8	88	
213	639	18	579	12	**		259	40 58	15	913	2	3.0	
215	626	13	591	12	,	7	260	73	15	915 915	2		2
		14		12	40				15		2	90	
216	612 598	14	603	11	18		261	88 100	14	917	2	<i>3</i> 0	
217		14	614	12		. 7	262	102	15	919	1		2
218	584	14	626	11		, i	263	117	14	920	1		ľ
219	570	1	637		25	•	264	131		921		92	ļ
220	+555	15	-648	11			265	-145	14	<b>~92</b> 2	<b>-</b> 1		ļ
221	541	-14	658	-10		6	266	160	-15	922	0		1
222	526	15	669	11	31		267	174	14	922	0	93	1
223	1	15		10	OI.				18	922 922	0	90	1
223 224	511	15	679 690	11		+7	268	187	14	922 922	0		+1
	496	-15		-10	1.00		269	201	-18	922 -921	+ 1	+94	
225	+481	<u> </u>	<b>-700</b>	1	+38		270	-214		-H21		194	

TABLE IV.—Continued.

PERTURBATIONS OF THE CO-ORDINATES IN UNITS OF THE SIXTH DECIMAL.

ARGUMENT IV.

Arg.	ξ <sub>1</sub>	Diff.	71	Diff.	ζ1	Diff.	Arg.	ξ <sub>1</sub>	Diff.	$\eta_1$	Diff.	ζ <sub>1</sub>	Diff.
270°	-214		-921		+94		315	-652		-600		+71	
271	<b>22</b> 8	-14	920	+ 1	İ		316	658	-6	587	+13	ł	
272	241	13	919	1	ľ	+1	317	664	6	574	18	1	8
273	254	18	917	2	95		318	670	6	561	13	68	
274	267	13	915	2	l	ļ	319	676	6	548	13	İ	
275	279	12	913	2	l	0	320	681	5	535	18	ł	3
276	292	13	911	2	95	l	321	687	6	521	14	65	1
277	304	12	908	8			322	692	5	507	14		
278	316	12	905	8		-1	323	697	5	493	14		3
279	328	12	902	8	94		324	702	5	479	14	62	
		12		4					5		14		1
280	-340	-12	898	+4		1 .	325	-707		<b>-46</b> 5	1,,		2
281	352	_	894	1 1		0	326	712	-5	450	+15		1 2
282	363	11	890	4	94		327	716	4	436	14	60	1
283	375	12	886	4		1 .	<b>32</b> 8	721	5	421	15	į	
284	386	11	881	5		1	329	725	4	406	15	Į	3
285	397	11	876	5	93		330	729	4	392	14	57	1
286	408	11	871	5			331	733	4	377	• 15	1	1
287	418	10	865	6		1	332	737	4	362	15	Į.	2
288	429	11	859	6	92		333	741	4	347	15	55	1
289	439	10	853	6			334	744	8	332	15	ł	
		10		6		2			4		16		3
290	<b>-44</b> 9	-10	-847	+7			335	-748	-3	-316	+15	ł	1
291	459	10	840		90	<u> </u>	336	751	8	301		52	1
292	469	10	833	7 8		2	337	754	8	286	15 16		2
293	<b>47</b> 9	9	825	_		*	338	757	8	270		l	*
294	488	9	818	7	88		339	760	,	255	15	50	
295	497	10	810	8		و ا	340	762	8	239	16		2
296	507		802			*	341	765	1	223	16		2
297	516	9	793	9	86		342	767	2	208	15	48	1
298	524	8	785	8		2	343	769	2	192	16		١.
299	533	9	776	9		"	344	771	2	177	15		2
000				9			ا		2		16		1
300	-542	- 8	-767	+10	84		345	<b>-77</b> 3	-1	-161	+16	46	
301	550	8	757	10		8	. 346	774	1	145	16		2
302	558	8	747	10			347	775	1	129	15		1
303	566	8	737	10	81		348	776	1	114	16	44	1
304	574	8	727	10		2	349	777	i	98	16	Į	1
305	582	š	717	11			350	778	1	82	16		-
306	590	7	706	11	79		351	<b>7</b> 79	_ <del>_</del>	66	15	43	ł
307	597	7	695	11		3	352	779	0	51	16		2
308	604	8	684	11			353	779	0	35	16		1
309	612		673		76		354	779		19		41	1
910	610	7	CC1	12			255	pre-c	0		16	Ì	1
310	-619	- 7	-661	+19		3	355	- <b>77</b> 9	0	- 3	+15	[	2
311	626	6	649	12	<b></b>		356	779	+1	+ 12	16	39	l
312	632	7	637	12	73		357	778	1	28	16	39	1
313	639	6	625	12		<b>,</b>	358	777	1	44	15	l	-1
314	645	- 7	613	+18			359	776	+1	59	+16		
315	-652		-600		+71	li	<b>36</b> 9	<b>-77</b> 5		+ 75	1 -	+38	l

Arg.	<i>ξ</i> <sub>1</sub>	Diff.	<b>7</b> 1	Diff.	ζ1	Diff.	Arg.	ξ <sub>1</sub>	Diff.	η1	Diff.	ζ1	Diff.
°	-507		+ 52		- 84		135°	+358		-188		+150	
3	507	0	39	-13	77	+7	138	376	+18	181	+ 7	148	-2
6	505	+ 2	26	13	70	7	141	392	16	174	7	146	2
9	502	3	+ 13	13	63	7	144	408	16	166	8	144	2
12	497	5	0	13	56	7	147	422	14	158	8	141	8
15	491	6	- 13	18	49	7	150	436	14	150	8	137	4
18	484	7	26	13	41	8	153	448	12	141	9	133	4
1		9	39	18		8		ľ	11		9		4
21	475	10	l .	13	33	8	156	459	10	132	10	129	4
24	465	11	52	19	25	7	159	469	8	122	9	125	5
27	454		64		18		162	477	1	113		120	
30	-441	13	- 77	13	10	8	165	1.404	7	-103	10		5
		+14		-12	- 10	+8	165	+484	+ 6		+11	+115	-6
33	427	15	89	11	- 2	8	168	490	4	92	10	109	6
36	412	16	100	12	+ 6	8	171	494	3	82	11	103	6
39	396	17	112	11	14	8	174	497	+ 2	71	10	97	6
42	379	19	123	10	22	1	177	499	0	61	11	91	7
45	<b>36</b> 0		133	l i	30	8	180	499	1	50		84	1
48	340	20	143	10	38	8	183	498	- 1	39	11	78	6
51	320	20	153	10	45	7	186	496	9	28	11	71	7
54	299	21	163	10	53	8	189	493	8	16	12	63	8
57	277	22	171	8	60	7	192	488	5	- 5	11	56	7
60	-254	23	-179	8	. 60	8	195	+482	6	+ 6	11	. 40	8
		+24		- 8	+ 68	+7	198		<b>– 8</b>		+12	+ 48	-7
63	<b>23</b> 0	24	187	7	75	7	_	474	9	18	11	41	8
66	206	25	194	7	82	6	201	465	10	29	11	33	8
69	181	25	201	6	88	7	204	455	11	40	11	25	8
72	156	26	207	5	95	6	207	444	12	. 51	12	17	8
75	130	26	212	4	101	6	210	432	14	63	11	9	8
78	104	26	216	;	107	5	213	418	14	74	10	+ 1	8
81	78		220	i .	112	1	216	404	E	84	1	- 7	1
84	51	27	224	4	118	6	<b>2</b> 19	388	16	95	11	15	8
87	- 25	26	226	2	123	5	222	371	17	106	11	23	8
1		27		2	l .	4	İ		17		10		8
90	+ 2	+27	-228	- 2	+127	+4	225	+354	-19	+116	+10	- 31	-8
93	29	26	230	-1	131	1	228	335	19	126	i	39	1
96	55	! !	231	1	135		231	316	1	136	10	47	8
99	81	26	231	0	139	4	234	295	21	145	9	54	7
102	107	96	230	+ 1	142	8	237	274	21	154	9	61	7
105	133	26	229	1	145	8	240	252	22	163	9	69	8
108	159	26	228	1	147	2	243	230	22	172	9	76	7
111	184	25	226	9	149	2	246	207	28	180	8	83	7
114	208	24	223	8	151	2	249	183	24	187	7	89	6
117	232	24	219	4	152	1	252	158	95	194	7	£6	7
***		28	213	4	1.52	+1	202	100	25	154	7	"	6
120	+255	ممدا	-215	١	+153	_	<b>25</b> 5	+133		+201	1 .	-102	
123	277	+22	211	+4.	153	0	<b>2</b> 58	108	-25	207	+ 6	107	-5
126	<b>2</b> 98	21	206	5	153	0	261	83	25	213	6	113	6
129	319	91	200	6	152	-1	264	57	26	218	5	118	5
132	339	20	194	6	151	1	267	31	26	222	4	123	6
135	+359	+19	-188	+ 6	+150	-1	270	+ 5	-26	+226	+ 4	-127	-4
1.7.7	て・メノフ	1	-100	<u> </u>	1 7100	<u> </u>	- 21U	1 T U		1 7440	1	-121	1

TABLE IV.—Continued.

PERTURBATIONS OF THE CO-ORDINATES IN UNITS OF THE SIXTH DECIMAL.

ARGUMENT V.

Arg.	ξ <sub>1</sub>	Diff.	71	Diff.	ζ1	Diff.	Arg.	<b>ট</b> া	Diff.	71	Diff.	ζ1	Diff.
270 273 276 279 282 285 288 291 294 297 300 303 306 309 312	+ 5 - 21 47 72 98 124 149 174 198 222 -245 268 290 311 332	-26 26 26 26 26 25 26 24 24 23 23 -28 29 21 -19	+226 229 232 234 235 236 236 235 234 232 +229 226 222 217 211	+8 8 9 1 +1 0 -1 1 2 8 -8 4 6 -6	-127 132 135 139 142 145 147 149 150 151 -152 152 151 150		315 318 321 324 327 330 333 336 339 342 345 348 351 354 357	-351 370 387 404 420 434 447 459 470 479 -487 494 499 503 506	-19 17 17 16 14 18 19 11 9 8 -7 8 4 8	+205 199 191 183 175 166 156 146 136 125 +113 102 90 77 65	- 6 8 8 9 10 10 10 11 12 -11 12 13 13 -13	-149 147 145 142 139 136 132 128 124 119 -114 109 103 97 91	+2 2 3 3 4 4 4 5 +5 6 6 6 6 7
315	-351		+205		-149		360	-507	1	+ 52		<b>– 84</b>	

### ARGUMENT VI.

Arg.	કૃ	Diff.	$\eta_1$	Diff.	ζ1	Arg.	<b>ઠા</b>	Diff.	$\eta_1$	Diff.	ζ1
0 3 6 9 12 15 18 21 24 27	+492 488 483 477 470 461 451 440 428 414	- 4 5 6 7 9 10 11 12 14 14	+ 54 79 104 129 153 177 200 223 245 267 +288	+25 25 25 24 24 23 28 29 91	0 0 -1 1 2	69 72 75 78 81 84 87 90 93 96	+127 102 77 51 + 25 - 1 27 53 78 104 -129	-25 26 26 26 26 26 26 26 26 26 26	+471 477 482 485 487 488 487 485 482 477	+6 6 8 9 +1 -1 2 8 6	-4 4 4 5
33	384	-16 17	308	†20 19	2	102	154	-25 25	464	- 7 9	5
36 39 42	367 349 330	18 19	327 346 363	19 17	2 3	105 108 111	179 203 226	24 28	455 446 435	9 11	4
45 48	311 290	19 21	379 395	16 16	3	114 117	249 271	28 22	422 409	18 13	4
51 54	269 247	21 22	409 423	14 14	3	120 123	293 314	29 21	394 379	15 15	4
57	224	28	435	19 11		126	333	19 19	362	17 18	4
60 63 66	+201 177 152	94 95	+446 455 464	+ 9	4 -4	129 132 135	-352 370 387	-18 17	-344 326 306	-18 20	4
69	+127	-25	+471	+ 7		138	-403	-16	-286	30	-3

TABLE IV.—Continued. . PERTURBATIONS OF THE CO-ORDINATES IN UNITS OF THE SIXTH DECIMAL. . ARGUMENT VI.

Arg.	<b>દ</b> ા	Diff.	η,	Diff.	ζ,	Arg.	ક્ષ	Diff.	71	Diff.	ζ1
138	-403		+286		-3	<b>249</b> °	-125	\	-473		
141	418	-15	265	21	Ī	252	100	+25	479	- 6	+4
145	431	13	243	22	3	255	74	96	483	4	
147	444	18	220	28		<b>25</b> 8	48	26	486	3	4
150	455	11	197	23	3	<b>2</b> 61	- 22	96	488	3	
153	465	10	173	94		264	+ 4	96	488	0	5
156	474	9	149	94	2	267	30	26	487	+1	
159	481	7	124	25		270	56	96	485	2	5
162	487	6	99	25	2	273	81	25	481	4	
165	492	6	74	25		276	107	26	476	5	5
		3		26				25		6	
168	-495	- 2	+ 48	25	1	279	+132	+25	-470	+8	
171	497	-1	+ 23	26		282	157	24	462	9	5
174	498	+ 1	- 3	26	<b>-1</b>	285	181	94	453	10	
177	497	2	29	25		288	205	23	443	11	5
180	495	4	54	26	0	291	228	23	432	19	
183	491	6	80	25		294	251	22	420	14	4
186	486	6	105	25	0	297	273	21	406	15	
189	480	8	130	25		300	294	20	391	15	4
192	472	8	155	24	+1	303	314	20	376	17	
195	464	· -	179			306	334		<b>3</b> 59		4
100	454	10	000	23		309	+353	19	041	18	
198	-454	+12	-202	-23	1		1	+17	-341	+18	
201	442	12	225	28	•	312	370	17	323	20	4
204	430	14	248	22	2	315	387	15	303	20	
207	416	16	270	21	٠,	318	402	15	283	21	3
210	401	16	291	20	·2	321	417	18	262	22	
213	385	17	311	19		324	430	12	240	23	3
216	368	19	330	19	2	327	442	11	217	28	_
219	349	19	349	17	_	330	453	10	194	28	3
222	330	20	366	17	3	333	463	9	171	24	
225	310	1	383			336	472	1	147		2
<b>22</b> 8	-290	20	-398	15	3	339	+479	7	-132	25	
231	268	+22	412	-14	ا	342	485	+ 6	-132 98	+24	2
231 234	246	22	426	14	4	345	489	4	73	25	~
237	223	28	438	12	*	348	492	3	47	26	1
237 240	199	24	448	10	4	351	492	2	- 22	25	1
	175	24	446 458	10	7	351 354	494 495	+ 1		25	, 1
243	175 150	25	456 466	8	+4	354 357	495 494	- 1		96	+1
246 940	-125	+25	400 -473	- 7	T*3	360	+492	- 2	29 + 54	+25	0
249	1 -120	<u> </u>	4/3	1		300	1492	<u> </u>	+ 04	<u> </u>	<u> </u>
							· · · · · · · · · · · · · · · · · · ·				

TABLE IV.—Continued.

PERTURBATIONS OF THE CO-ORDINATES IN UNITS OF THE SIXTH DECIMAL.

ARGUMENT VIL

A		Diff.	<u> </u>	Diff.	,	l	કૃ	Diff.		Diff.	,
Arg.	<u>ξ</u>		η1	- Діп.	ζι	Arg.		ДШ.	η1	——	<u></u>
°	<b>-23</b> 1		- 4		-20	135	+292		-400		
3	232	- 1	8	-4		138	322	+30	383	+17	+8
6	233	1	13	5	21	141	350	28	364	19	
9	234	1	18	6		144	377	27	342	22	10
12	236	2	23	5 6	22	147	403	96 23	319	28 96	
15	<b>23</b> 8	2 2	29	6		150	426	23	293	270 277	13
18	240	3	35	7	23	153	448	20	266	30	
21	243	2	42	8		156	<b>46</b> 8	17	236	81	15
24	245	3	50	8	24	159	485	16	205	32	
27	<b>24</b> 8		58			162	500	1	173		16
30	-250	2	- 67	9	24	165	+513	18	-140	23	
33	253	8	77	-10	~1	168	522	+9	106	+84	18
36	255	2	88	11	24	171	529	7	70	36	10
39	256	1	99	11	~-	174	533	4	- 35	85	19
42	<b>258</b>	- 2	112	18	23	177	534	+1	+ 1	86	
45	<b>25</b> 8	0	126	14		180	533	-1	37	86	20
48	258	0	140	14	23	183	<b>528</b>	5	72	28	
51	<b>25</b> 8	. 0	155	15		186	521	7	107	85	21
54	256	+ 2	171	16	22	189	511	10	142	85	
57	253	3	187	16		192	498	13	175	83	22
		4		17	_ 1			16		82	
60	-249	+ 5	-204	-18	21	195	+482	-18	+207	+31	
63	244	7	222	17		198	464	20	238	29	22
66	237	8	239	18	19	201	444	22	267	27	
69	229	9	257	18		. 204	422	24	294	96	23
72	220 209	11	275	18	18	207	398	96	320	23	
75 78	209 196	13	293 311	19	10	210	372 345	27	343	21	23
81	182	14	328	17	16	213 216	316	29	364 383	19	22
84	166	16	325 345	17	14	216 219	286	30	400	17	22
87	149	17	362	17	14	222	256	30	414	14	22
0,	113	90	302	15		222	200	81	313	11	22
90	-129		-377		12	225	+225		+425		
93	109	+20	391	-14		228	194	-81	434	+ 9	21
96	86	23	404	18	9	231	162	32	441	7	
99	62	24 25	416	19		234	131	31 31	445	+ 2	20
102	37	27	426	10 8	7	237	100	31	447	0	
105	- 10	28	434	7		240	69	29	447	- <b>s</b>	19
108	+ 18	29	441	4	4	243	40	29	444	4	
111	47	29	445	- 8		246	+ 11	28	440	7	18
114	76	81	448	0	- 2	249	- 17	27	433	9	
117	107		448		1	252	44	ł	424		17
120	+138	81	-446	+ 9	+ 1	255	- 69	25	+414	10	Į.
123	169	+31	442	+ 4	1	258	93	-24	402	-12	15
126	200	31	435	7	3	261	115	22	389	18	I
129	231	81	426	9	ľ	264	136	21	375	14	13
132	262	81	414	12	+6	267	155	19	360	15	l
135	+292	+30	-400	+14	1	270	-172	-17	+344	-16	+11
!				<del></del>	<u> </u>	<del> </del>		<del>'                                    </del>	-		

TABLE IV.—Continued.

PERTURBATIONS OF THE CO-ORDINATES IN UNITS OF THE SIXTH DECIMAL.

ARGUMENT VII.

Arg.	ξı	Diff.	7/1	Diff.	ζι	Arg.	\$ <sub>1</sub>	Diff.	η1	Diff.	ζ1
270 273 276 279 282 285 288 291 294	-172 188 202 214 225 234 242 248 253 257	-16 14 12 11 9 8 . 6 5	+344 327 309 202 274 256 238 220 203 186	-17 18 17 18 18 18 18 18 17 17	+11 9 7 5 + 3	315 318 321 324 327 330 333 336 339 342	-259 257 255 252 249 247 244 241 239 237	+2 2 3 3 2 2 3 2 2 2	+100 88 78 68 59 51 43 36 30	-12 10 10 9 8 8 7 6	- 7 9 11 13
300 303 306 309 312 315	-260 261 262 262 261 -259	- 1 - 1 - 0 + 1 + 2	+170 155 140 126 112 +100	16 -15 15 14 14 -12	0 - 2 - 4	345 348 351 354 357 360	-235 233 232 231 231 -231	+2 1 +1 0	+ 19 14 9 5 + 1 - 4	5 - 5 5 4 - 4	17 19 -20

## ARGUMENT VIII.

Arg.	ક્ષ	Diff.	$\eta_1$	Diff.	ζ1	Arg.	ξı	Diff.	$\eta_1$	Diff.	ζ1
0 3 6 9 12 15 18	-352 350 347 344 339 334 328 320	+ 2 3 3 5 6 8	+ 22 40 58 76 94 112 129 146	+18 - 18 18 18 18 17	-7 6 5	69 72 75 78 81 84 87 90	-106 88 70 52 34 - 15 + 3	+18 18 18 18 19 18	+335 340 344 347 349 350 351 350	+ 5 4 3 2 1 + 1 - 1	+ 6 7 8
24 24 27 30	312 303 -294	9	163 179 +194	17 16 15	3	93 96 99	40 58 + 76	18 18 18	348 346 +342	9 9 4	9
33 36 39 42	283 272 260 247	+11 11 12 13	209 224 238 251	+15 16 14 13	-1 0	102 105 108 111	94 112 129 146	+18 18 17 17	338 332 326 319	- 4 6 6 7	10 10
45 48 51 54	233 219 204 189	14 14 16 15	263 275 286 296	12 12 11 10	+2	114 117 120 123	162 178 194 209	16 16 16 16	311 302 292 281	8 9 10 11	11 11
57 · 60 63	173 -157 140	16 16 +17	306 +314 322	10 8 + 8 7	4	126 - 129 132	224 +238 251	15 14 +18 12	270 +258 245	. 11 12 -18	11 11
66 69	123 -106	+17	329 +335	+ 6	+5	135 138	263 +275	+12	232 +218	-14	+11

TABLE IV.—Continued.

PERTURBATIONS OF THE CO-ORDINATES IN UNITS OF THE SIXTH DECIMAL.

ARGUMENT VIII.

Arg.	ξ1	Diff.	71	Diff.	ζ1	Arg.	ξ <sub>1</sub>	Diff.	71	Diff.	ζ1
138	+275		+218		+11	<b>249</b> °	+106		-335		- 6
141	286	+11	203	-15		252	89	-17	340	_ •	
144	297	11	188	15	11	255	71	18	344	4	7
147	306	9	172	16		<b>2</b> 58	53	18	347	8	
150	315	9	156	16	11	261	34	19	349	2	8
153	322	7	139	17	]	264	+ 16	18	350	1	
156	329	7	122	17	10	267	- 3	19	351	- 1	9
159	335	6	105	17		270	21	18	350	+ 1	
162	340	5	87	18	9	273	39	18	349		9
165	344	4	69	18		276	58	19	346	8	
		4		18	_			18		4	
168	+348	+ 2	+ 51	-18	9	279	- 76	18	-342	+4	10
171	350	1 1	33	18		282	94	17	338	5	
174	351	+ 1	+ 15	18	8	285	111	18	333	7	10
177	352	-1	- 3	19		288	129	17	326	7	
180	351	2	22	18	7	291	146	16	319	8	11
183	349	2	40	18		294	162	16	311	9	
186	347	1	58	18	6	297	178	16	302	10	11
189	343		76	18		300	194	15	292	10	
192	339	5	94	18	5	303	209	15	282	11	11
195	334		112			306	· <b>224</b>		271		
		7	100	17		000	200	14	050	12	
198	+327	- 7	-129	-17	4	309	-238	-13	-259	+18	11
201	320	8	146	16		312	251	18	246	- 14	
204	312	9	162	16	3	315	264	12	232	14	11
207	303	9.	178	16		318	276	11	218	15	
210	294	11	194	15	2	321	287	10	203	15	11
213	283	11	209	14		324	297	9	188	15	•
216	272	12	223	14	+ 1	327	306	9	173	17	11
219	260	18	237	18		330	315	8	156	16	
222	247	14	250	13	0	333	323	7	140	17	10
225	233		263			336	330	-	123		
228	+219	14	-275	12	- 2	339	-336	6	-105	18	9
231	205	-14	296	-11	~ ~	342	-336 341	- 5	-105 87	+18	9
234	189	16	296	10	3	342 345	341 345	4	70	17	9
237	173	16	305	9	٥	348	348	8	70 51	19	9
240	157	16	305 314	9	4	348 351	346 351	8	33	18	8
	141	16	322	8	*	351	351 352	- 1		18	•
243		17	-	7	- 5	1		. 0	- 15	19	
246	124	18	329 -335	-6	- 0	357 360	352	0	+ 4	+18	+ 7
249	+106	[	-330			300	-352		+ 22		

TABLE IV.—Continued.

PERTURBATIONS OF THE CO-ORDINATES IN UNITS OF THE SIXTH DECIMAL.

ARGUMENT IX.

											<del></del> '
Arg.	ξ1	Diff.	71	Diff.	ζ1	Arg.	ξ1	Diff.	71	Diff.	<b>ζ</b> 1
°	+150		- 3		+22	180	-305		+ 11		-24
5	150	0	11	- 8	20	185	302	+ 8	45	+84	21
10	150	0	18	7	18	190	294	8	78	83	19
15	151	+ 1	26	8	16	195	282	12	110	82	16
20	152	1	34	8	13	200	267	15	140	30	13
25	153	+ 1	43	9	11	205	247	20	167	97	10
30	153	0	53	10	8	210	225	23	192	25	7
.35	, 153	0	63	10	6	215	200	25	212	20	4
40	153	0	75	12	+ 3	220	172	28	230	18	-1
45	152	- 1	87	12	0	225	144	28	243	13	+2
		8		18				29		9	
50	+149		-100		- 2	230	-115	Lan	+252	١	+ 5
55	146	8	114	-14	5	235	86	+29	257	+ 6	8
60	141	5	128	14	8	240	57	29	<b>2</b> 59	+ 2	11
65	134	7	143	15	10	245	29	98	257	- 9	13
70	126	8	158	15	13	250	- 3	26	252	8	16
75	116	10	173	15	16	255	+ 22	25	244	8	18
80	104	12	188	15	18	260	45	28	234	10	21
85	89	15	202	14	20	265	65	20	222	12	23
90	72	17	216	14	23	270	83	18	209	18	25
95	53	. 19	228	12	25	275	99	16	194	15	26
		22		10				14		16	1
100	+ 31	-24	<b>-23</b> 8	- 8	-27	280	+113	+11	+178	-15	+28
105	+ 7	25	246	6	2/8	285	124	8	163	16	29
110	- 18	27	252	- 8	30	290	132	. 7	147	16	30
115	45	28	255		31	295	139		131	15	31
120	73	28	255	+4	32	300	144	4	116	14	31
-125	101	29	251	8	33	305	148	9	102	18	32
130	130	29	243	11	34	310	150	+ 2	89	13	32
135	159	27	232	15	34	315	152	0	76	13	32
140	186	21 26	217	19	34	320	152	0	64	10	31
145	212		198		34	325	152		54		31
150	000	94	180	23		900	.150	. 0		10	
150	-236	-21	-176	+26	-33	330	+152	- 1	+ 44	<b>–</b> 9	+30
155	257	17	150	29	32	335	151	1	35	8	29
160	274	14	121	81	31	340	150	ō	27	8	28
165	288	10	90	82	29	345	150		19	8	27
170	298	6	58	84	28 °°	350	150	- i	11	7	25
175	304	-1	- 24	+35	26	355	149	+ 1	+ 4	- 7	24
180	-305		+ 11		-24	360	+150		- 3		+22

TABLE IV.—Continued.

PERTURBATIONS OF THE CO-ORDINATES IN UNITS OF THE SIXTH DECIMAL.

ARGUMENT X.

<u> </u>					<u>,</u>			<del>,</del>			
Arg.	<b>১</b>	Diff.	<b>7</b> 1	Diff.	ζ1	Arg.	ર્દા	Diff.	η1	Diff.	ζ1
o°	+187		- 10		+ 6	180°	-178		+ 17		- 6
5	186	- 1	26	<del>-</del> 16	5	185	175	+ 8	33	+16	5
10	183	8	43	17	4	190	171	4	48	15	4
15	178	5	60	17	3	195	166	5	62	14	
20	172	6	76	16	3	200	159	7	76	14	2
25	164	8	91	15	2	205	152	7	90	14	3 2 2
30	155	9	106	15	+ 1	210	143	9	103	13	- 1
35	145	10	120	14	0	215	134	9	115	12	0
40	133	12	133	18	- 1	220	123	11	126	11	+ 1
45	121 .	. 12	145	12	2	225	112	11	136	10	2
		14		11				12		10	
50	+107		-156		- 3	230	-100		+146		+ 3
55	92	-15	165	- 9	4	235	87	+13	154	+ 8	4
60	77	15	173	8	5	240	74	13	162	8	5
65	61	16	180	7	6	245	60	14	168	6	6
70	45	16	185	5	7	250	46	14	173	5	6 6 7
<b>7</b> 5	28	17	188	8	7	255	32	14	177	4	7
80	+ 11	17	190	2	8 '	<b>26</b> 0	17	15	180	8	8
85	- 6	17	191	-1	9	265	- 2	15	181	1	8
90	23	17	189	+ 2	9	270	+ 14	16	182	+ 1	9 9
95	39	16	187	2	10	275	29	15	180	- 2	9
		16		4				15		2	ì
100	- 55	-16	-183	+ 6	-10	280	+ 44	+15	+178		+10
105	71	1	177	1	10	285	59	14	174	- •	10
110	86	15	170	8	11	290	73		169	5	11
115	100	14	162		11	295	87	14	163	6	11
120	113	18	152	10	11	300	101	14	156	7	11
125	125	12	141	11	11	305	114	18	147	9	11
130	136	11	130	11	11	310	126	19	137	10	11
135	146	10	117	18	11	315	138	. 12	126	11	11
140	155	9	104	18	10	320	148	10	114	12	11
145	163	8	90	14	10	325	158	10	101	13	10
		6		15				8		14	
150	-169	- 5	<b>– 75</b>	+15	-10	330	+166	+ 7	+ 87	-15	+10
155	174	8	60	15	9	335	173	6	72	15	9 9
160	177	2	45	16	9	340	179	4	57	16	
165	179	-1	29	15	8	345	183	8	41	17	8
170	180	- 1	- 14	16	7	350	186	+ 1	24	17	8
175	180	+ 2	+ 2	+15	7	355	187	0	+ 7	-17	7
180	-178	1 7 2	+ 17	- 10	- 6	360	+187		- 10	-11	+6
	<del></del>										

TABLE IV.—Continued.

PERTURBATIONS OF THE CO-ORDINATES IN UNITS OF THE SIXTH DECIMAL.

ARGUMENT XI.

·											
Arg.	ξ1	Diff.	<b>7</b> 1	Diff.	ζ <sub>1</sub>	Arg.	ξį	Diff.	71	Diff.	្រ
°	+101		+ 11		- 3	180°	-144		+ 10	,	-30
. 5	98	- 8	30	+19	- 1	185	144	0	8	- 2	31
10	92	6	48	18	+1	190	144	0	6	2	31 31
15	83	9	65	17	2	195	145	- 1	+ 3	8	32
20	72	11	79	14	3	200	145	0	0	8	32
25	58	14	92	18	4	. 205	145	0	- 3	8	33
30	43	15	102	10	4	210	146	- 1	6	3	34
35	27	16	110	8	4	215	146	0	10	4	34
40	+ 11	16	116	6	4	220	146	0	14	. 4	35
45	- 5	16	119	8	3	225	146	0	18 "	4	· 36
		16		+ 1				+ 1		5	i i
50	- 21	-15	+120	- 1	+ 2	230	-145	+ 1	- 23	- 6	-36
55	36	1	119	9	+ 1	235	144	2	<b>2</b> 8	6	37
60	51	15	117	8	0	240	142	2	34	7	37
65	64	18	114	4	- 2	245	140		41	6	37
70	76	12	110	_	3	250	137	8	47		′ <b>38</b>
75	87	11	105	5	5	<b>25</b> 5	133	4	54	7	38
80	97	10	99	6	7	260	128	5	61	8	38
85	106	9	93	6	9	265	122	6	69		<b>3</b> 8
90	113	7	86	7	10	270	115	7	76	7	38
95	120	7	80	6	12	275	106	9	83	7	37
		5		7				9		7	
100	-125	- 6	+ 73	- 6	-14	280	- 97	+11	- 90	- 6	-37
105	130	8	67	6	15	285	86	19	96	5	36
110	133	8	61	6	17	290	74	14	101	8	35
115	136		55	6	18	295	60	14	106	8	34
120	139	i	49	5	19	300	46	16	109	- 2	32
125	140	i	44	4	21	305	30		111	0	30
130	141	1	40	4	22	310	- 13	•17 17	111	+ 3	28
135	142	1	36	4	23	315	+ 4	17	108	5	26
140	143	0	32	8	24	320	21	17	103	7	24
145	143	"	29		25	325	38		96		21
	440	0		8		200		16	~	9	
150	-143	-0	+ 26	8	-26	330	+ 54	+14	- 87	+12	-19
155	143	اة	23	8	<b>2</b> 6	335	68	12	75	15	16
160	143	اةا	20	2	27	340	80	10	60	16	13
165	143		18	8	28	345	90	7	44	18	10
170	143	-1	15	9	29	350	97	+4	26	19	8
175	144	ō	13	<b>– 3</b>	29	355	101	0	- 7	+18	5
180	-144		+ 10		30	360	+101		+ 11		- 3

TABLE IV.—Continued.

PERTURBATIONS OF THE CO-ORDINATES IN UNITS OF THE SIXTH DECIMAL.

ARGUMENT XIL

Arg.	, &	Diff.	<b>7</b> 1	Diff.	ζ <sub>1</sub>	Arg.	ξ1	Diff.	71	Diff.	<b>ն</b> 1
0	- 97	+ 1	- 6	- 7	-2	180	+122	- 9	+ 8	+12	+2
5	96	1 1	13	8		185	120	8	20	11	
10	95	i	21	7	2	190	117	8	31	11	2
15	94	2	28	7		195	114	5	42	10	
20	92	8	35	8	3	200	109	6	52	10	3
25	89	8	43	7	•	205	103	7	62		
30	86	4	50	7	3	210	96	8	71	8	3
35	82	_	57	-		215	88	-	79	· ·	
40	78	4	64	7	2	220	80	8	86	7	2
45	74	4	70 -	6		225	71	9	93	7	
	i	6	1	7				10		5	i
50	<b>- 6</b> 8	+ 6	- 77		2	230	+ 61	-10	+ 98	+ 5	2
55	62		83			235	51	1	103		
60	56	6	88	5	2	240	41	10	106	8	2
65	49	7	93	5		245	31	10	109	8	
70	41	8	98	5	2	250	20	11	110	1	2
75	33	8	102	4		255	+ 10	10	111	+ 1	]
80	24	9	105	8	1	260	0	10	110	- 1	1 1
85	15	9	108	8		265	- 10	10	109	1	
90	- 5	10	109	1	1	270	19	9	107	2	1
95	+ 5	10	110	- 1		275	29	10	104	3	_
	' '	10		0				8		4	
100	+ 15		-110		-1	280	- 37		+100	_	+1
105	25	+10	109	+1		285	45	<b>– 8</b>	96	- 4	i i
110	36	11	107	2	0	290	53	8	91	5	0
115	46	10	105	2		295	60	7	86	5	i i
120	56	10	101	4	0	300	66	6	80	6	0
125	66	10	96	5		305	72	6	74	6	
130	75	9	90	6	+1	310	77	5	67	7	-1
135	84	9	83	7		315	81	4	60	7	-
140	92	8	75	8	1	320	85	4	53	7	1
145	99	7	66	9		325	88	8	46	7	
1	"	7	l ~~	9	'			8	-~	7	
150	+106		- 57		1	330	- 91		+ 39		1
155	111	+ 5	47	+10		335	93	- 2	32	- 7	
160	115	4	37	10	2	340	95	2	24	8	2
165	119	4	26	11		345	96	1	17	7	
170	121	2	15	11	2	350	97	- 1	9	8	2
175	122	+1	- 3	12	1	355	97	0	+ 2	7	· ·
180	+122	0	+ 8	+11	+2	360	- 97	0	- 6	- 8	-2

TABLE IV.—Continued.

PERTURBATIONS OF THE CO-ORDINATES IN UNITS OF THE SIXTH DECIMAL.

ARGUMENT XIII.

Arg.	š <sub>1</sub>	Diff.	η <sub>1</sub>	Diff.	ζ1	Arg.	₹ <sub>1</sub>	Diff.	71	Diff.	S <sub>1</sub>
							<u> </u>				
0	-83	+1	0	-4	- 6	180	+83	-1	+ 0	+8	+ 6
5	82	2	- 4	3		185	82	9	3	4	
10	80	2	7	4	4	190	80	2	7	8	4
15	<b>7</b> 8	8	11	8		195	78	3	10	4	_
20	75	3	14	8	- 2	200	75	4	14	3	+ 2
25	72	4	17	4		205	71	4	. 17	8	
30	<b>6</b> 8		21	3	0	210	67	5	20	8	0
35	63	5	24	2		215	62	5	23	8	
40	<b>5</b> 8	6	26	8	+ 1	220	57	5	26	2	- 1
45	52	1	29			225	52		28		
50	40	6	01	2		230	.40	6	. 21	8	
50	<b>-46</b>	+6	-31	-9	3	235 235	+46	-7	+31 33	+2	3
55 60	40	7	33	2			39	6		2	
60	33	7	35	2	5	240	33	7	35	1	5
65 70	26	7	37	1	_	245	26	7	36	2	_
70	19	7	38	1	7	<b>25</b> 0	19	7	38	1	7
<b>7</b> 5	12	7	39	-1		255	12	7	39	+1	
80	- 5	8	40	0	8	260	+ 5	8	40	0	8
85	+ 3	7	40	0		265	- 3	7	40	0	
90	10	7	40	o	9	270	10	7	40	0	9
95	17		40	4.		275	17	l	40		
100	+24	7	-39	+1	10	280	-24	7	+40	0	10
105	31	+7	39	+0 '	10	285	31	-7	39	-1	10
110	38	7	38	1	10	290	38	7	38	1	10
115	44	6	<b>36</b>	2	10	295	44	6	37	1	10
120	50	6	34	2	11	300	50	6	35	2	11
125	56	6	32	2		305	56	6	33	2	11
130	61	6	30	2	11	<b>31</b> 0	61	5	31	2	11
135	66	5	28	2	**	315	66	5	29	2	11
140	70	4	25 25	8	10	320	70	4	26 26	8	10
145	74	4	23	2	1	325	74	4	23	8	10
1720	17	8	~~	8			, ,	8	~~	8	
150	+77		-20		9	<b>33</b> 0	-77		+20		9
155	80	+8	17	+8		335	80	-8	17	8	
160	82	2	13	4	8	340	82	2	14	8	8
165	83	1	10	8		345	83	1	10	4	
170	. 84	+1	7	8	7	350	84	-1	7	8	7
175	84	0	- 3	4		355	84	0	+ 3	4	
180	+83	-1	0	+8	+ 6	<b>36</b> 0	-83	+1	0	-8	- 6
			-								

TABLE IV.—Continued.

PERTURBATIONS OF THE CO-ORDINATES IN UNITS OF THE SIXTH DECIMAL.

ARGUMENT XIV.

Arg.	<b>δ</b> 1	Diff.	71	Diff.	ζ1	Arg.	ક્ષ	Diff.	η1	Diff.	દા
°	+44		+ 3		+2	180	54		- 2		-2
5	45	+1	- 1	-4		185	54	0	+ 3	+5	
10	45	0	4	8	2	190	- 54	0	8	5	2
15	44	-1	7	3		195	53	+1	13	5	
20	44	0	11	4	1	200	51	2	18	5	1
25	43	1	14	8	_	205	49	2	23	5	1
30	42	1	18	4	`+1	210	47	2	27	4	-1
35	• 41	1	21	8	'-	215	44	8	31	4	•
40 -	39	2	24	8	0	220	40	4 -	35	4	0
45	37	2	28	4	•	225	37	8	38	8	, v
-	•	2	~				0.	4		3	
- 50	+35		-31	Ĭ	-1	<b>9</b> 30	-33	-	+41		+1
55	32	8	34	8		235	29	+4	44	+8	
60	30	2	-37	8	1	240	24	5	46	2	1
65	27	8	40	8	_	245	20	4	47	1	_
70	23	4	42	2	2	250	15	5	48	1	2
75	20	•	44	2	~	255	11	4	49	1	
80	16	4	46	2	2	960	6	5	50	+1	2
85	12	4	48	2	~	265	- 2	4	49	-1	~
90	8	4	49	1	3	270	+ 2	4	49	0	3
95	+ 3	5	50	1	ا	275	7	5	48	1	"
30	T 3	4	50	-1		210	•	4	40	1	
100	- 1	•	-51	-	3	200	+11		+47	_	3
105	6	-5	51	0	_	285	14	+8	45	2	_
110	11	5	51	0	3	290	18	4	44	1	3
115	15	4	50	+1		295	22	4	42	3	•
120	20	5	49	1	3	300	25	8	39	8	3
125	25	5	47	2		305	28	8	37	2	•
130	29	4	45	2	4	<b>3</b> 10	30	2	34	8	4
135	33	4	42	3	•	315	33	8	31	8	•
140	37	4	39	3	3	<b>320</b>	35	2	28	8 .	3
145	41	4	35	4		325	37	2	25	8	•
140		8	30	4		960	01	2	20	8	
150	-44		-31	_	3	330	+39		+22	_	3
155	47	-3	27	+4		335	40	+1	19	-8	
160	50	8	23	4	3	340	42	2	16	8	3
165	52	2	18	5		345	43	'n	13.	8	
170	53	1	13	5	3	350	43	0	10	8	3
175	54	-1	8	5		355	44	+1	6	4	
		lol	<b>- 2</b>	+6	-2	360	+44	0	+ 3	-8	_
180	-54		- 2		×				+ 4		+2

TABLE IV.—Continued.

PERTURBATIONS OF THE CO-ORDINATES IN UNITS OF THE SIXTH DECIMAL.

ARGUMENT XV.

ļ											
Arg.	ξ <sub>1</sub>	Diff.	<b>7</b> 1	Diff.	ζ1	Arg.	<b>ξ</b> 1	Diff.	7/1	Diff.	ζ,
°	-29		- 2		0	180°	+31		+ 2		0
5	29	0	4	-2	0	185	31	0	5	+3	0
10	29	0	7	8	0	190	30	-1	7	2	0
15	28	+1	9	2	0	195	29	1	10	8	0
20	27	1	12	8	0	200	28	1	13	3	0
25	26	1	14	2	0	205	27	1	15	2	0
30	25	1	16	2	0	210	25	2	17	2	0
35	23	2	18	3	0	215	24	1	20	8	0
40	22	1	20	2	0	220	22	2	22	2	0
45	20	2	22	2	0	225	20	2	23	1	0
	ł	2		2				2		2	ļ
50	-18	+2	-24	-1	0	230	+18	8	+25	+1	0
55	16	2	25	1	0	235	15	2	26	9	0
60	14	8	26	1	0	<b>24</b> 0	13	3	28	1	0
<b>6</b> 5	11	9	27	i	0	245	10	9	29	0	0
70	9	2	28	i	0	250	8	8	29	+1	0
75	7	3	29	-1	0	255	5	8	30	0	0
80	4		30	0	0	260	+ 2		30		0
85	- 1	8	30	ı i	0	265	0	2	30	0	0
90	+ 1	2	30		0	270	- 3	8	30	0	0
95	4	8	30	0	0	275	5	2	30	0	0
	_	2		0				3		-1	_
100	+ 6	_ +8	-30	+1	0	280	- 8	-2	+29	-1	0
105	9	8	29	1	0	285	10	3	28	i	0
110	12	2	28	il	0	290	13	2	27	1	0
115	14	2	27	i	0	295	15	2	26	2	0
120	16	8	26	9	0	300	17	2	24	i	0
125	19	2	24	ī	0	305	19	2	23	2	0
130	21	2	23	2	0	310	21	2	21	2	0
135	23	2	21	2	0	315	23	1	19	2	0
140	25	î	19	<b>1</b>	0	320	24	1	17	2	0
145	26		16		0	325	25		15		0
150		2	,,	2		330		2	.,,	2	
150	+28	+1	-14	+8	0		-27	-1	+13	8	0
155	29	1	11	2	0	335	28	0	10	2	0
160	30	0	9	3	0	340	28	-1	8	2	0
165	30	+1	6	8	0	345	29	ō	6	8	0
170	31	0	3	2	0	350	29	ò	3	2	0
175	31	0	- 1	+8	0	355	29	Ö	+ 1	-8	0
180	+31		+ 2		0	360	-29		- 2		0

TABLE IV.—Continued.

PERTURBATIONS OF THE CO-ORDINATES IN UNITS OF THE SIXTH DECIMAL.

	A	RGUME	NT XVI.				A	RGUME	NT XVII	,	
Arg.	ξı	Diff.	71	Diff.	ζ,	Arg.	ξį	Diff.	<b>1</b> /1	Diff.	Š1
0	+113		+ 4	-10	+2	°°	-103	+1	- 16	-8	-2
5	113	- 1	- 6	9		5	102	8	24	9	
10	112	2	15	10	2	10	99	3	33	9	2
15	110	2	25	9		15	96	4	42	8	
20	108	4	34	9	1	20	92	5	50 57	7	1
25 30	104	• 4	43	9	.,	25 30	87	5		7	,
	100	5	52	9	+1		82	6	64	7	1
35 40	95	6	61	8		35 40	76	7	71 78	7	_
45	89	6	69 70	7	0		69	7	78 83	5	0
40	83	7	76	7		45	62	8	53	5	
50	+ 76	•	- 83	•	0	50	- 54	_	- 88	"	0
55	68	- 8	89	- 6	ľ	55	46	+8	93	-5	
60	60	8	95	6	-1	60	38	8	96	8	+1
65	52	8	100	5	1 -	65	29	. 9	99	8	'-
70	43	9	104	4	1	70	20	9	101	2	1
75	34	9	107	8	•	75	11	9	103	9	•
80	24	10	110	8	2	80	- 2	9	103	0	1
85	14	10	111	1	-	85	+ 7	9	103	0	-
90	+ 5	9	112	- 1	2	90	16	9	102	+1	2
95	- 5	10	112	0		95	25	9	101	1	
		10		+ 1				9		8	
100	- 15		-111		3	100	+ 34	ا . ا	- 98		2
105	25	-10	109	+ 2		105	42	+8	95	+8	
110	34	9	107	3	3	110	50	8	91	4	2
115 ·	43	9	103	4		115	58	8	86	5	
120	52	9	99	4	3	120	66	8	81	5	2
125	61	9	94	5		125	73	7	<b>7</b> 5	6	
130	69	8	88	6	3	130	79	6	<b>6</b> 8	7	2
135	77	8	82	6		135	85	6	61	7	
140	84	7	75	7	3	140	90	5	54	7	3
145	90	. 6	<b>6</b> 8	7		145	94	4	46	8	
		5	-00	8		150		4		8	ا ۾ ا
150	- 95	- 5	- 60	+ 9	3	150	+ 98	+8	- 38	+9	2
155	100	5	51	9		155	101	2	29	9	
160	105	3	42	9	3	160	103	1	20	9	2
165	108	2	33	9		165	104	+1	11	9	
170	110	9	24	10	2	170	105	-1	- 2	9	2
175	112	~ i	14	+10		175	104	-1	+ 7	+9	
180	-113	•	- 4		-2	180	+103	-	+ 16		+2

TABLE IV.—Continued.

PERTURBATIONS OF THE CO-ORDINATES IN UNITS OF THE SIXTH DECIMAL.

1											
	A	RGUME	NT XVII	τ.				ARGUME	NT XIX.		
Arg.	ક્	Diff.	η,	Diff.	ζ1	Arg.	ર્દા	Diff.	71	Diff.	Š.
°	+43		+ 5		0	ő	+29	_	+14		-1
10	41	-2	12	+7	0	10	26	-8	18	+4	-1
20	39	2	19	7	0	20	22	4	22	4	0
30	35	.4	26	7	0	30	17	5	26	4	0
40	30	5	31	5	0	40	12	5	28	2	0
50	24	6	36	5	0	50	7	5	30	+2	+1
60	17	7	40	4 9	0	60	+ 1	6	30	0	1
70	10	7	42	+1	0	70	- 5	6	30	-1	1
80	+ 3	8	43	1 1	0	80	10	-	29	· -	2
90	- 5		43		0	90	15	5	27	2	2
100	10	7	+42	-1	•	100		5	. 04	8	
100	-12	-7		<b> </b> −8	0	100	-20	-4	+24	-3	+2
110	19	7	39	4	0	110	24	4	21	4	2
120	26	5	35	5	0	120	28	2	17	5	2
130	31 36	8	30 24	6	0	130	30	9	12 7	5	2 2
140 150	39	8	17 •	7	0	140 150	32 33	-1	+ 2	5	1
160	39 42	8	17.	7	0	160	33	0	+ 2 - 4	6	1
170	42 43	-1	+ 3	7	٠ ١			+2	-	5	1
180	-43	0	+ 3 - 5	0 170 31 4 9 4							+1
100	-40			<u> </u>	<u> </u>	100	-23		-14	!	71
	ARGUME	NT XX.			ARGUME	NT XXI.		1	RGUME	NT XXII	•
Arg.	<b>ξ</b> 1	<b>7</b> 1	ζ,	Arg.	<b>ક</b> 1	71	<b>ζ</b> ι	Arg.	ξı	7/1	ζ,
°	-27	- 4	0	o°	+25	+1	0	o°	-24	+10	_ <del>8</del>
10	26	9	0	10	24	- 3	0	10	21	14	8
20	24	13	0	20	24	8	0	20	17	18	8
30	21	17	0	30	22	12	0	30	13	21	7
40	18	21	0	40	20	16	0	40	9	23	7
50	14	23	0	50	17	19	0	50	- 4	25	6
60	10	25	0	60	13	22	0	60	+ 1	26	5
70	- 5	27	0	70	10	24	0	70	6	26	3
80	0	27	0	' 80	6	26	0	80	10	25	2
90	+ 4	27	0	90	+1	26	0	90	15	23	-1
100	+ 9	-26	0	100	- 3	<b>26</b>	0	100	+19	+21	+1
110	13	24	0	110	7	25	0	110	22	19	2
120	17	21	0	120	11	24	0	120	25	15	4
130	21	18	0	130	15	21	0	130	26	11	5
140	23	14	0	140	18	18	0	140	28	7	6
150	25	10	0	150	21	14	0	150	28	+ 3	7
160	27	- 5	0	160	23	10	0	160	27	- 2	8
170	27	0	0	170	24	6	0	170	26	6	8.
180	+27	+ 4	0	180	-25	-1	0	180	+24	<del>-</del> 10	+8
						<u></u>					

TABLE IV.—Continued.

PERTURBATIONS OF THE CO-ORDINATES IN UNITS OF THE SIXTH DECIMAL.

A	RGUME	NT XXIII	ī.	ARGUMENT XXIV.				ARGUMENT XXV.				
Arg.	δ <sub>1</sub>	η1	ζ1	Arg.	₽.	71	ζı	Arg.	ξ1	<b>7</b> 1	ζ1	
°°	-22	- 2	-1	°	+20	-4	+2	°	· -19	+ 1	0	
10	22	+ 2	1	10	20	4	1	10	19	4	0	
20	21	6	-1	20	18	4	+1	20	18	7	0	
30	20	10	0	30	16	3	0	30	16	10	0	
40	18	13	0	40	14	3	-1	40	14	13	0	
50	15	16	0	50	11	2	2	50	12	15	0	
60	12	18	0	60	8	1	2	60	9	17	0	
70	9	20	+1	70	+ 4	-1	3	70	6	18	0	
80	5	21	1	80	0	0	4	80	- 3	19	0	
90	- 1	22	1	90	- 3	+1	4	90	+ 1	19	0	
100	+ 3	+22	+1	100	- 7	+1	-4	100	+ 4	+19	0	
110	6	21	1	110	10	2	4	110	7	18	0	
120	10	20	2	120	13	3	4	120	10	16	0	
130	13	18	2	130	16	3	4	130	13	14	0	
140	16	15	2	140	18	4	4	140	15	12	0	
150	18	12	2	150	19	4	4	150	17	9	0	
160	20	9	1	160	20	4	8	160	18	6	0	
170	22	5	1	170	21	4	3	170	19	+ 3	0	
180	+22	+ 2	+1	180	-20	+4	-2	180	+19	-1	0	
A	RGUME	ıt xxvı		ARGUMENT XXVII.				AI	RGUMEN	T XXVII	I.	
Arg.	ξı	71	ζı	Arg.	ક્ષ	71	ζ1	Arg.	ξı	71	ζ,	
°	+19	+13	0	°	+16	+11	+3	°	-15	+ 5	+1	
10	21	9	ő	10	14	7	3	10	14	8	1	
20	23	6	ŏ	20	12	+ 2	3	20	13	11	î	
30	24	+ 2	ŏ	30	10	- 2	2	30	12	14	+1	
	i	- 2	ŏ	40	7	7	2	40	10	16	0	
40	24	1 <b>–</b> 2	י ט י	40								
40 50	24 23	- z 6	0	50	4	11	2	50	8	18	. 0	
			-						8 6	18 19	0	
50	23	6	0	50	4	11	2	50	-		-	
50 <b>6</b> 0	23 22	6 10	0	50 60	4 + 1	11 15	2 1	50 60	6	19	0	
50 60 70	23 22 20	6 10 13	0 0 0	50 60 70	4 + 1 - 3	11 15 19	2 1 +1	50 60 70	6 - 3	19 20	0	
50 60 70 80	23 22 20 17	6 10 13 16	0 0 0	50 60 70 80	4 + 1 - 3 6	11 15 19 22	2 1 +1 0	50 60 70 80	6 - 3 0	19 20 19	0 0 -1	
50 60 70 80 90	23 22 20 17 14	6 10 13 16 19	0 0 0 0	50 60 70 80 90	4 + 1 - 3 6 9	11 15 19 22 24	2 1 +1 0 0	50 60 70 80 90	6 - 3 0 + 2	19 20 19 19	0 0 -1 1	
50 60 70 80 90	23 22 20 17 14 +11	6 10 13 16 19	0 0 0 0	50 60 70 80 90	4 + 1 - 3 6 9	11 15 19 22 24 25	2 1 +1 0 0	50 60 70 80 90	6 - 3 0 + 2 + 5	19 20 19 19	0 0 -1 1	
50 60 70 80 90 100 110	23 22 20 17 14 +11 7	6 10 13 16 19 -21	0 0 0 0 0 0	50 60 70 80 90 100	4 + 1 - 3 6 9 -11	11 15 19 22 24 -25 26	2 1 +1 0 0	50 60 70 80 90 100	6 - 3 0 + 2 + 5 7	19 20 19 19 +18	0 0 -1 1	
50 60 70 80 90 100 110 120	23 22 20 17 14 +11 7 + 3	6 10 13 16 19 -21 22 23	0 0 0 0 0 0 0 0	50 60 70 80 90 100 110	4 + 1 - 3 6 9 -11 14	11 15 19 22 24 -25 26 26	2 1 +1 0 0	50 60 70 80 90 100 110 120	6 - 3 0 + 2 + 5 7	19 20 19 19 +18 16	0 0 -1 1 -1 1 2	
50 60 70 80 90 100 110 120 130	23 22 20 17 14 +11 7 + 3 - 1	6 10 13 16 19 -21 22 23 23	0 0 0 0 0 0 0 0 0	50 60 70 80 90 100 110 120	4 + 1 - 3 6 9 -11 14 16 17	11 15 19 22 24 -25 26 26 25	2 1 +1 0 0 -1 1 2	50 60 70 80 90 100 110 120	6 - 3 0 + 2 + 5 7 9	19 20 19 19 +18 16 14	0 0 -1 1 -1 1 2 2	
50 60 70 80 90 100 110 120 130 140	23 22 20 17 14 +11 7 + 3 - 1 6	6 10 13 16 19 -21 22 23 23 22	0 0 0 0 0 0 0 0 0 0	50 60 70 80 90 100 110 120 130 140 150	4 + 1 - 3 6 9 -11 14 16 17 18 18	11 15 19 22 24 -25 26 26 25 24	2 1 +1 0 0 0 -1 1 2 2	50 60 70 80 90 100 110 120 130	6 - 3 0 + 2 + 5 7 9 11	19 20 19 19 19 +18 16 14 11 8	0 0 -1 1 -1 1 2 2 2	
50 60 70 80 90 100 110 120 130 140 150	23 22 20 17 14 +11 7 + 3 - 1 6	6 10 13 16 19 -21 22 23 23 22 20	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	50 60 70 80 90 100 110 120 130 140	4 + 1 - 3 6 9 -11 14 16 17 18 18	11 15 19 22 24 -25 26 26 25 24 21	2 1 +1 0 0 0 -1 1 2 2 3 3	50 60 70 80 90 100 110 120 130 140	6 - 3 0 + 2 + 5 7 9 11 13	19 20 19 19 +18 16 14 11 8 5	0 0 -1 1 -1 1 2 2	

TABLE IV.—Continued.

PERTURBATIONS OF THE CO-ORDINATES IN UNITS OF THE SIXTH DECIMAL.

A	RGUME	XXX TO	•	ARGUMENT XXX.				ARGUMENT XXXL			
Arg.	ξ <sub>1</sub>	η1	ζ,	Arg.	ξı	η1	Ğı	Arg.	ક્	$\eta_1$	ζ,
°	+12	+ 1	0	°	-8	-1	0	°	-7	-1	0
10	12	-1	0	10	8	2	0	10	7	2	0
20	12	3	Ô	20	7	3	0 0	20	6	3	0
30	11	5	ŏ	30	7	5	0	30	6		
40	10	7	-	40	6	6	0	40	5	4 5	0
		9	0	50	5	7			-		0
50	9	-	0		_	1	0	50	. 4	6	0
60	7	10	0	60	4	8	0	60	3	6	0
70	5	11	0	70	2	8	0	70	-2	7	0
80	3	12	0	80	-1	8	0	80	0	7	0
90	+ 1	12	0	90	+1	8	0	.90	+1	7	0
100	- 1	-12	-1	100	+2	-8	0	100	+2	-6	0
110	3	· 12	1	110	3	8	0	110	3	6	0
120	5	11	1	120	4	7	0	120	4	5	0
130	7	10	1	130	5	6	0	130	5	5	0
140	9	9	1	140	6	5	0	140	6	4	Ö
150	10	7	1	150	7	4	0	150	7	3	0
160	11	5	-1	169	8	2	0	160	7	-2	Ö
170	12	3	ō	170	8	-1	o l	170	7	ō	Ŏ
180	-12	-1	0	180	+8	+1	0	180	+7	+1	Ŏ

AF	RGUMEN'	т хххи		ARGUMENT XXXIII.				ARGUMENT XXXIV.			
Arg.	ξ <sub>1</sub>	η <sub>1</sub>	ζ1	Arg.	ξ,	71	ζ <sub>1</sub>	Arg.	<b>દે</b> 1	η1	ζ <sub>1</sub>
°				0		0		0			
0	+4	-5	0	0	+3	1 1	0	0	+3	0	. 0
10	5	4	0	10	3	0	0	10	3	+1	0
20	6	3	0	20	3	-1	0	20	3	1	0
30	6	. 2	0	30	3	1	0	30	2	2	0
40	7	-1	0	40	3	2	0	40	2	2	0
50	7	0	0	50	2	2	0	50	2	2	0
60	7	+1	0	60	2	3	0	60	1	3	0
70	6	2	0	70	1	3	0	70	+1	3	0
80	6	3	0	80	+1	3	0	80	0	3	0
90	5	4	0	90	0	3	0	90	0,	3	0
100	+4	+5	0	100	. 0	-3	0	100	-1	+3	0
110	. 3	5	0	110	-1	3	0	110	1	3	0
120	2	6	0	120	1	3	0	120	2	2	0
130	+1	6	0	· 130	2	3	0	130	2	2	0
140	0	6	0	140	2	2	0	140	3	2	0
150	-1	6	0	150	3	2	0	150	3	1	0
160	2	6	0	160	3	1	0	160	3	+1	0
170	3	5	0	170	3	-1	0	170	3	0	0
180	-4	+5	0	180	-3	0	0	180	-3	0	0

TABLE IV.—Continued.

PERTURBATIONS OF THE CO-ORDINATES IN UNITS OF THE SIXTH DECIMAL.

				II				II				
A	RGUMEN	T XXX	7.	AB	GUMEN	T XXXV	Ί.	AI	GUMEN'	r xxxv	Ή.	
Arg.	<u>ξ</u>	η1	ζ1	Arg.	ξ <sub>1</sub>	71	ζ,	Arg.	\$1	η <sub>1</sub>	ζ,	
°	-3	+1	0	o°	-2	0	0	o°	+2	+ 2	-1	
10	3	1	0	10	2	0	0	10	2	4	0	
20	3	1	0	20	2	-1	0	20	2	6	0	
30	2	1	0	30	2	1	0	30	2	7	0	
40	2	1	0	40	2	1	0	40	2	9	0	
50	2	+1	0	50	1	2	oʻ	50	. 2	. 10	0	
60	2	. 0	0	60	1	2	0	60	2	11	0	
70	. 1	0	0	70	-1	2	0	70	1	11	+1	
80	-1	0	0	80	0	2	0	80	1	12	1	
90	0	0	0	90	0	2	0	90	+1	11	1	
100	0	0	0	100	+1	-2	0	100	0	+11	+1	
110	+1	-1	0	110	1	2	0	110	0	10	1	
120	1	1	0	120	1	2	0	120	-1	9	1	
130	1	1	0	130	,2	2	0	130	1	7	1	
140	2	1	0	140	2	1	0	140	1	6	1	
150	2	1	0	150	2	1	0	150	2	4	1	
160	2	1	0	160	2	-1	0	160	2	+ 2	1	
170	2	• 1	0	170	2	0	0	170	2	0	1	
180	+3	-1	9	180	+2	0	0	180	-2	- 2	+1	
AR	GUMENT	xxxvi	П.	AR	ARGUMENT XXXIX.				ARGUMENT XL.			
Arg.	ર્દા	71	Š1	Arg.	કૃ	71	ζι	Arg.	<b>\$</b> 1	η1	ζ1	
°	-2	+4	0	0	-2	-2	+2	°	-2	0	0	
20	3	4	0	20	2	-1	ī	20	2	-1	. 0	
40	4	3	ő	40	3	ō	î	40	ĩ	i	o	
60	4	2	ŏ	60	3	+1	+1	60	-1	2	ő	
80	3	+1	ŏ	80	2	1	0	80	ō	2	Ŏ	
100	3	-1	+1	100	2	2	0	100	+1	2	Ŏ	
120	-2	2	1	120	-1	3	-1	120	1	1	0	
140	Õ	3	+1	140	0	3	1	140	2	-1	0	
160	+1	4	0	160	+1	3	1	160	2	0	0	
180	+2	-4	0	180	+2	+2	-2	180	+2	0	0	

TABLE IV.—Concluded.

PERTURBATIONS OF THE CO-ORDINATES IN UNITS OF THE SIXTH DECIMAL.

A	ARGUME	NT XLI.		ARGUMENT XLII.				ARGUMENT XLIII.			
Arg.	ţ <sub>1</sub>	$\eta_1$	51	Arg.	ξ1	η1	ζ1	Arg.	\$ <sub>1</sub>	η1	ζ1΄
· 0°	-1	0	0	° °	-1	+2	0	° °	-1	0	0
‡ <b>2</b> 0	1	+1	0	20	0	2	0	20	1	0	. 0
40	-1	1	0	40	0	2	0	40	-1	+1	0
60	0	1	0	60	+1	2	0	60	: 0	1	0
80	0	1	0	80	1	1	0	80	0	1	0
100	0.	1	0	`100	2	+1	0	100	0	1 -	0
120	+1	1	0	120	2	0	0	120	+1	1 .	0
140	1	+1	0	140	2	-1	0	140	1	+1	0
160	1	0	0	160	1	1	0	160	1	0	0
180	+1	0	0	180	+1	-2	0	180	+1	0	0

	ARGUMEN	T XLIV.		ARGUMENT XLV.					
Arg.	ξ <sub>1</sub>	$\eta_1$	ζ <sub>1</sub>	Arg.	ξ,	η <sub>1</sub>	ζι		
°	-1	+1	0	°	0	0	0		
20	1	0	0	20	-1	0	0		
40	1	0	0	40	1	• -1	. 0		
60	-1	0	0	60	1	1	0.		
80	0	0	0	80	1	2	0		
100	0	0	0	100	1	2	0		
120	0	0	0	120	1	2	0		
149	0	<b>-1</b>	0	140	-1	1	. 0		
160	+1	1	0	160	0	-1	0		
180	+1	-1	0	180	0	0	0		

<sup>• 180°</sup> are to be subtracted from the Arguments > 180°, and  $\xi_1$ ,  $\eta_1$ , and  $\zeta_1$  to be taken with the reversed sign.

Mean Equinox of the beginning of the Year.

cos (z<sub>1</sub> z) Years.  $\cos(x_1 x)$  $\cos(y_1 x)$  $\cos(z_1 x)$ cos (y1 y)  $\cos(z_1 y)$  $\cos(x_1z)$ cos (y<sub>1</sub> z)  $\cos(x_1 y)$ 9.983980 1852 B 9.982316 9.423945n8.944771 9.966907 9.4009262 8.169765n 9.425327 9.446013 1853 9.982289 9.424326n 9.400892n 8.167022n 9,425285 9.983984 8.944586 9,446346 9,966880 9.425243 9,983988 1854 9.400858% 8.16426578 9.982261 9.424707n 8,944400 9.966852 9.446679 9.982234 9.400824n 8.1614887 9.425201 9.983992 1855 9.4250887 8.944215 9.447012 9.966824 9.983996 1856 B 9.425468n 9.495159 9,982206 9.4007912 8.158674n 8,944029 9.447345 9.966796 1857 9.982179 9.425848n 8.943844 9.966768 9.400757n 8.155832n 9,425117 9.984000 9,447677 9.425075 9.984004 1858 9.982151 9.426227n8.943658 9.448009 9.966740 9.400723n 8.152991n 1859 8.150142n 9.425033 9.984008 9.982123 9.4266062 8.943472 9.448341 9.4006892 9.966712 9.984011 1860 B 9.982095 9.426984n 8.943286 9.448673 9.066684 9.4006567 8.147263n 9.424990 9.424948 9.984015 1961 9.982068 9.4273627 9,4006227 8.144356n 8.943100 9.449004 9.966656 1862 9.982040 9.427740n 8.942914 9.449335 9.966628 9.4005888 8.1414187 9.424905 9.984019 9.984023 8.1384727 9.424863 1863 9.982012 9.428117n 8.942728 9.449666 9.966600 9.400554n 9.424820 9.984027 1864 B 9.981984 9.428494n 8.942541 9.449996 9.966572 9.400521n 8.135514n 9.424778 9.984031 1865 9.981956 9.428871n 8.942355 9.450326 9.966544 9.4004872 8.132548n 1866 9.981928 9.966516 9.400454n 8.129549n 9.424735 9.984035 9.429247n8,942168 9.450656 1867 9.981900 9.429623n 8.941981 9,966488 9.400420n 8.126521n 9.424693 9.984039 9.450986 8.123466n 9,424650 9.984042 9.400387n 1868 B 9.981872 9.429999n8.941794 9.966459 9.451315 9.400353n8.120409n 9.424608 9.984046 1869 9.981844 9.430374n 8.941607 9.451644 9.966431 8.117338n 9.984050 9,424565 1870 9.981816 9.430749n8.941420 9.451972 9.966403 9.400320n1871 9.981788 9.431124n 8.941233 9.452301 9.966375 9.400286n 8.114244n 9.424522 9.984054 1872 B 9.981760 9.431498n 8.941045 9.452629 9.966346 9.400253n8.111114n 9,424479 0.984058 9.400219n 8.107956n 9.424437 9.984062 1873 9.981732 9.431872n8,940858 9.966318 9,452357 9.981704 9.432245n8,940670 9.966290 9.400186n 8.104794n 9.424394 9.984066 1874 9,453284 9.432618n 9.424351 9.984070 9.400152n8.1016102 1875 9.981676 8.940483 9.453612 9.966262 9.400119n 8.098387n9.424308 9.984073 1876 E 9.981647 9.432991n8.940295 9.453939 9.966233 9.424265 9.984077 1877 9.981619 9.433364n 8.940107 9.454266 9.966205 9.4000852 8.095134n 9.424222 9.984081 1878 9.981591 9.433736n 8.939919 9.454592 9.966177 9.4000527 8.091878n 9,424179 9.984085 1879 9.981563 9.434108n 8.939731 9.454918 9.966149 9.400019n 8.088597n 9.399986n 8.085275n 9.424136 9.984088 1880 E 9.981534 9.434479n 8.939543 9.455244 9.966120 1881 9.981506 9.434850n 8.939355 9.399952n8.081923n9,424093 9.984092 9,455570 9.966092 9.399919n 9.424050 9.984096 1882 9.981478 9.435221n9.455895 8.0785292 8,939167 9.966063 9.399886n 8.075119n 9.424007 9.984100 1883 9.981450 9.435591n 8.938979 9.456220 9.966035 9.3998537 9,423964 9.984103 1884 B 9.981421 9.435961n 8.938790 9.456545 9.966906 8.071711n 9.423921 9.984107 1885 9.981393 9.436331n 8.938602 9.456869 9.965978 9.399819n 8.068265n 9.984111 9.423878 1886 9.981364 9.436700% 8.938413 9.457193 9.965949 9.399786n8.064795n 1887 9.981336 9.437069n 8,938224 9.457517 9.965921 9.3997537 8.061302n 9.423835 9.984115 9.984119 1888 B 9.981307 9.437438n 8.938035 9.3997202 8.057762n 9,423791 9,457841 9.965892 1889 9.423748 9.984123 8.0541922 9.981279 9.437807n 8.937846 9.458164 9.965864 9.399687n1890 9.981250 9.438175n 8.937657 9.458487 9.965835 9.399654n 8.050612n9.423704 9.984127 9.423661 9.984131 1891 9.981222 9.438543n 8.937468 9.458810 9.965806 9.399621n 8.0469827 9.423617 9.084134 1892 B 9.981193 9.438910n 8.937278 9.459133 9.965777 9.399588n 8.043323n 9.423573 9.984138 1893 9.981165 9.439277n 8.937089 9.459455 9.965749 9.399555n8.039652n1894 9.981136 9.4396442 9.3995922 8.0359502 9.423529 9.984142 8,936899 9,459777 9.965720 1895 9.981108 9.440011n 8.936709 9.399489n 8.032216n 9.423485 9,984146 9.460099 9.965691 1896 B 9.981079 9.423442 9.984149 9.440377n8.0284497 8.936519 9.460420 9.965662 9.3994562 9.423398 9.984153 1897 9.981051 9.440743n 8.936329 9.460741 9.965634 9.399423n 8.024650n 9.984157 9.423355 1898 9.981022 9.4411087 8.936139 9.461061 9.965605 9.3993907 8.020817# 1899 9.980993 9.441474n 8.935949 9.461382 9.399357n 8.016950n 9,423311 9.984161 9.965576 9.423268 9.984164 1900 B 9.980964 9.441839n 8.935758 9.461702 9.965547 9.399325n8.013048n

TABLE VI.

CONSTANTS FOR THE EQUATOR.

Equator and mean Equinox at the beginning of the Year.

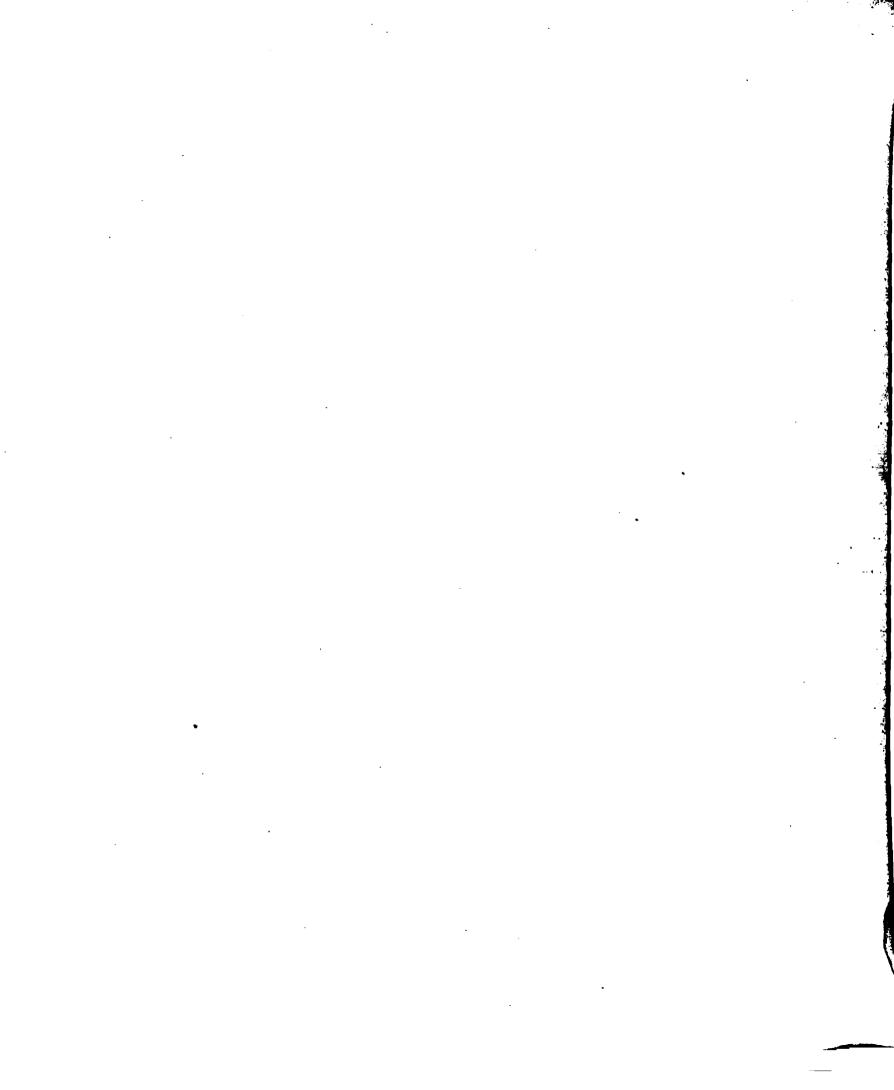
		Isquator and mean	Equitox at all begin			
Years.	A'	В′	C'	log sin a.	log sin b.	log sin c.
1852 B	105 27 14.0	16 46 17.2	356 49 20.7	9.398310	9.985785	9.425995
1853	105 28 3.8	16 47 4.6	356 50 31.7	9.998311	9.985787	9.425945
1854	105 28 53.6	16 47 52.0	356 51 42.7	9.998313	9.985790	9.425895
1855	105 29 43.5	16 48 39.2	356 52 53.8	9.998314	9.985792	9.425844
1856 B	105 30 33,4	16 49 26.8	356 54 5.0	9.998316	9.965794	9.425794
1857	105 31 23,2	16 50 14.2	356 55 16.1	9.998317	9.985797	9.425744
1858	105 32 13,0	16 51 1.6	356 56 27.1	9.998319	9,985799	9.425694
1859	105 33 2.9	16 51 49.0	356 57 38.2	9.998320	9,985801	9.425644
1860 B	105 33 52,8	16 52 36.5	356 58 49.5	9,998321	9.385804	9.425593
1961	105 34 42.6	16 53 23.8	357 0 0.6	9.998323	9,985806	9.425543
1862	105 35 32.4	16 54 11.2	357 1 11.7	9.996324	9,985808	9.425493
1863	105 '36 22.2	16 54 58.6	357 2 22.9	9.998326	9.985811	9.425443
1864 B	105 37 12.2	16 55 46.1	357 3 34.2	9.998327	9,985813	9.425392
1865	105 38 2.0	16, 56 33.5	357 4 45.4	9.998329	9,985815	9.425342
1866	105 38 51.8	16 57 20.9	357 5 56.5	9.996330	9,985818	9.425292
1867	105 39 41.6	16 58 8.2	357 7 7.7	9.998331	9,985820	9.425242
1868 B	105 40 31.6	16 58 55.8	357 8 19.1	9,998333	9,965822	9.425192
1869	105 41 21.4	16 59 43.1	357 9 30,3	9,998334	9,985825	9.425142
1870	105 42 11.2	17 0 30.5	357 10 41.5	9,998336	9.965827	9.425092
1871	105 43 1.0	17 1 17.9	357 11 52.7	9,998337	9,985829	9,425042
1872 B	105 43 50.9	17 2 5.4	357 13 4.1	9.996339	9.965831	9,424991
1873	105 44 40.7	17 2 52.8	357 14 15.4	9.996340	9,965634	9,424941
1874	105 45 30,5	17 3 40.2	357 15 26.6	9.998342	9,965836	9,424891
1875	105 46 20.3	17 4 27.6	357 16 37.9	9.998343	9,985838	9,424841
1876 B	105 47 10.3	17 5 15.1	357 17 49.3	9.998344	9.985840	9.424791
1877	105 48 0.1	17 6 2.5	357 19 0.6	9.998346	9,985843	9.424741
1878	105 48 49.9	17 6 49.8	357 20 11.9	9.996347	9,985845	9.424691
1879	105 49 39.7	17 7 37,2	357 21 23.2	9.998349	9,985847	9.424641
1880 B	105 50 29.7	17 8 24.7	357 22 34.7	9.998350	9,985849	9.424591
1881	105 51 19.5	17 9 12.1	357 23 46.0	9.998352	9.985852	9,424541
1882	105 52 9.3	17 9 59.5	357 24 57.3	9.998353	9,985854	9.424491
1883	105 52 59.1	17 10 46.9	357 26 8.7	9.998354	9.985856	9.424441
1884 B	105 53 49.0	17 11 34.4	357 27 20.2	9.998356	9.985858	9.424391
1885	105 54 38.8	17 12 21.8	357 28 31.6	9.998357	9.985860	9.424341
1886	105 55 28.6	17 13 9.1	357 29 42.9	9.998359	9.985863	9.424291
1887	105 56 18.4	17 13 56.5	357 30 54.3	9.998360	9.985865	9.424241
1888 B	105 57 8.4	17 14 44.0	357 32 5.9	9.998361	9.965867	9.424191
1889	105 57 58.2	17 15 31.4	357 33 17.3	9.998363	9.985869	9.424141
1890	105 58 48.0	17 16 18.8	357 34 28.7	9.996364	9.985871	9.424091
1891	105 59 37.8	17 17 6.2	357 35 40.2	9.998366	9.985874	9.424041
1892 B	106 0 27.7	17 17 53.7	357 36 51.8	9.998367	9.985876	9.423991
1893	106 1 17.5	17 18 41.1	357 38 3.2	9.998369	9.985878	9.423941
1894	106 2 7.3	17 19 28.5	357 39 14.7	9.998370	9.985880	9.423891
1895	106 2 57.2	17 20 15.9	357 40 26.2	9.998371	9.965882	9.423841
1896 B	106 3 47.1	17 21 3.4	357 41 37.8	9.998373	9.985884	9.423792
1897	106 4 36.9	17 21 50.8	357 42 49.4	9.998374	9.985886	9.423742
1898	106 5 26.7	17 22 38.1	357 44 0.9	9.998376	9.985888	9.423692
1899	106 6 16.5	17 23 25.5	357 45 12.4	9.998377	9.985890	9.423642
1900 B	106 7 6.5	17 24 13.0	357 46 24.1	9.998379	9.985893	9.423592
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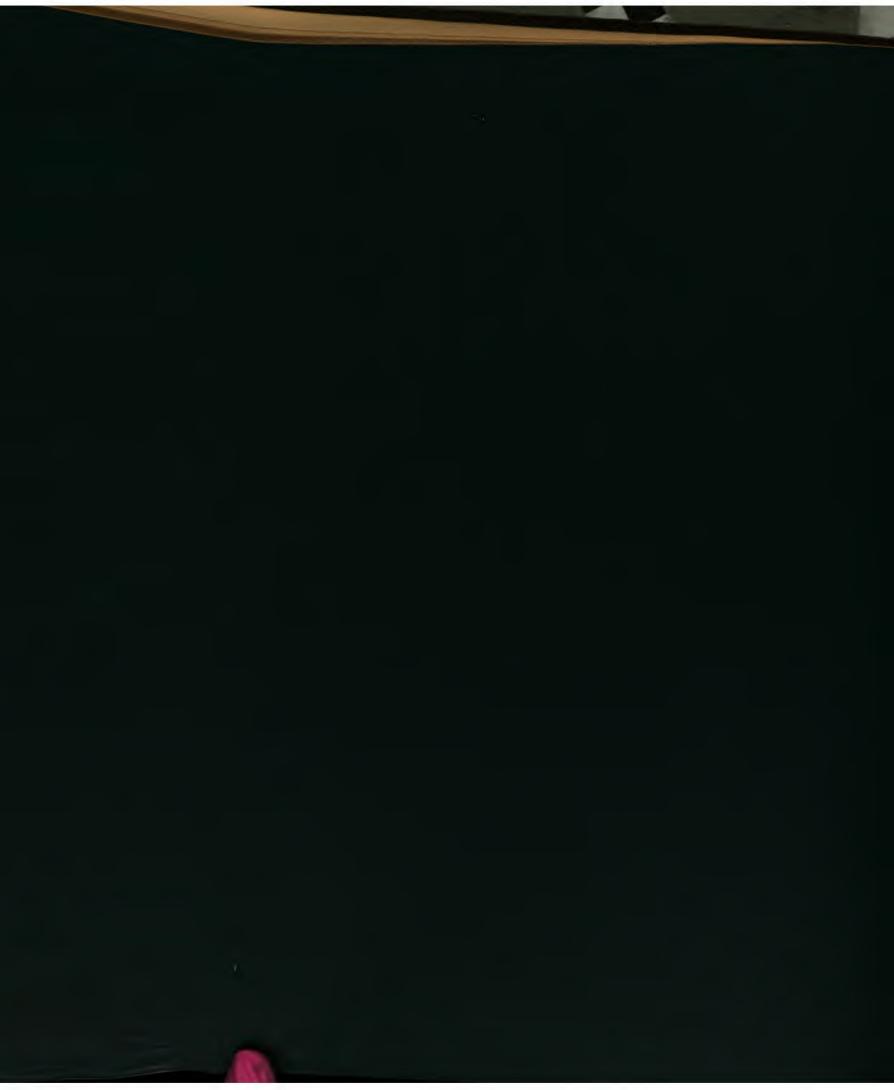
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